Investigation of Novel Ferroelectrics and their Electrical and Optical Applications

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About the Author

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Abstract

Ferroelectric materials are considered essential components in a wide spectrum of electrical and optical applications, including but not limited to ferroelectric random access memory (FeRAM), piezoelectric transducers, and optical waveguides and modulators, owing to their remarkable ferroelectric, piezoelectric, and electro-optic properties. Since the first report of ferroelectrics in the 1920s, extensive research has been invested and substantial achievements have been made in the ferroelectric domain. The research presented in this thesis provides a comprehensive investigation, including theoretical principles, fabrication technology, performance optimization, and electrical/optical applications, of two innovative ferroelectric materials, namely, Nd-doped bismuth titanate (BNdT) and bismuth ferrite (BFO).

We start by describing the material fabrication procedure, and then study the dependence of ferroelectric properties on various fabrication parameters. By varying the post annealing temperature and tuning the elemental constituents, ferroelectrics with optimized performance parameters, such as large remnant polarization (39.6 μ C/cm²), little fatigue degradation (<1.5%), low leakage density (5×10⁻⁷ A/cm² at 5 V DC), and so forth, are demonstrated in our work. Then, we further our study into the optical characterization of the BNdT material, and provide a systematic investigation of BNdT optical properties for the first time. Optical parameters including the optical transmittance, refractive index, extinction coefficient, and optical band gap energy, are examined and their correlation with different fabrication variables and microstructure properties is studied both experimentally and theoretically. In the third part of this thesis, by introducing the optimized BNdT ferroelectric thin film as a seeding layer for the BFO material, we report the first room temperature (RT) ferroelectric measurement of pure BFO material. A ferroelectric inducing effect in the BFO/BNdT multilayer structure is identified as the reason behind this phenomenon of ferroelectric enhancement.

We further advance our study by investigating the photovoltaic nature of multiferroic BFO, and report enhanced photovoltaic performance of the BFO material

in a graphene/polycrystalline BFO/Pt heterojunction structure for the first time. The unique properties of the graphene electrode lead to a short circuit current density of 61 μ A/cm² and an open circuit voltage of 0.52 V in the heterojunction. These values are much higher than the results previously reported in the literature. A theoretical model that takes into consideration the ferroelectric polarization, interface states, and energy band bending effect, is constructed to describe the ferroelectric photovoltaic effect and carrier transport behaviour for the first time. Key photovoltaic parameters, such as conversion efficiency, illumination intensity response, ON/OFF characteristics, minority carrier lifetime, and external quantum efficiency (EQE), are investigated through both theory and measurements. Finally, to improve the existing photovoltaic performance of the graphene/polycrystalline BFO/Pt heterojunction, HNO₃ treatment and CdSe quantum dots (QDs) filling/sensitizing, as two independent chemical and physical routines, are processed and compared. It can be seen that the photocurrent density exhibits a significant improvement from 61 μ A/cm² to 8.67 mA/cm² (~150 fold) after HNO₃ treatment, while a considerable enhancement of ~5 fold is seen with QDs filling/sensitizing. An optical application of a photosensitive detector and an electrical application of a tunable switch are also demonstrated as two interesting applications of the BFO photovoltaic effect.

Research in the field of novel BNdT and BFO ferroelectric materials continues to thrive, and a number of interesting theoretical and application studies are currently underway. The results achieved in this thesis may provide a useful understanding of the principles and properties of two such ferroelectrics, and can serve as assistance in future research perspectives.

Sommaire

Les matériaux ferroélectriques sont des composantes essentielles pour plusieurs applications en électriques et en optique comme les mémoires vives ferroélectriques (FeRAM), les transducteurs piézoélectriques et les guides d'onde et modulateurs optique, dues à leur propriétés ferroélectrique, piézoélectrique et électo-optique remarquables. Depuis le premier rapport de ferroélectricité dans les années 1920, l'intérêt de recherche et les réalisations massives dans le domaine de la ferroélectricité n'ont cessé de croître. La recherche présentée dans cette thèse fournie une étude compréhensive de deux nouveaux matériaux ferroélectriques, soit le bismuth de titane dopé au néodyme (BNdT) et la ferrite de bismuth (BFO). Cette étude inclue les principes théoriques, les technologies de fabrication, l'optimisation des performances et les applications électriques et optiques.

Nous débutons avec la fabrication des matériaux, et nous étudions la dépendance des propriétés ferroélectriques sur différents paramètres de fabrications. En modulant différemment la température de post-hybridation et en accordant le constituant élémentaire, nous démontrons des matériaux ferroélectriques ayant des paramètres de performance optimisés, tel une large polarisation rémanente (39.6 μ C/cm²), une faible fatigue de dégradation (<1.5%), une faible fuite de densité (5×10^{-7} A/cm² at 5 V DC), etc. Ensuite nous approfondissons notre recherche dans la caractérisation du BNdT et fournissons une étude systématique, en première, des propriétés optique du BNd. Nous examinons les paramètres optiques tels la transmittance optique, l'index de réfraction, les coefficients d'extinction et l'énergie de gap de bande et nous étudions expérimentalement et théoriquement leur corrélation avec différents paramètres de fabrication et de microstructure. Dans la troisième partie de cette thèse, en introduisant le film mince optimisé de BNdT ferroélectrique comme couche nourrissante du matériel BFO, nous rapportons la première mesure ferroélectrique à la température pièce du matériel BFO pure. Un champ ferroélectrique induit dans la structure multicouche BFO/BNdT est adressé pour expliquer une telle amélioration du phénomène ferroélectrique.

Nous faisons progresser notre étude en examinant la nature photovoltaïque de la BFO multiferroïque et signalons pour la première fois une performance améliorée photovoltaïque du matériel BFO dans une hétérojonction de graphène / BFO polycristalline / Pt. Les propriétés uniques de l'électrode de graphène mènent à un courant de court-circuit de la densité de 61µA/cm² et un circuit ouvert du voltage de 0,52 V à l'hétérojonction. Ces valeurs sont beaucoup plus élevées que les résultats précédemment rapportés dans la littérature. Un modèle théorique qui prend en considération la polarisation ferroélectrique, les états d'interface et l'effet de flexion de la bande d'énergie est, pour la première fois, construit pour décrire l'effet photovoltaïque ferroélectrique et le comportement de transport des porteurs. Les principaux paramètres photovoltaïques, tels que l'efficacité de conversion, la réponse de l'intensité de l'éclairage, les caractéristiques d'ON / OFF, la durée de vie des porteurs minoritaires et le rendement quantique externe (EQE), sont étudiés à la fois par la théorie et par les mesures. Enfin, le traitement avec HNO₃ et le remplissage / la sensibilisation des points quantiques (PQ) de CdSe, comme deux routines indépendantes chimiques et physiques, sont traités et comparés pour améliorer la performance photovoltaïque existante de l'hétérojonction de graphène / BFO polycristalline / Pt. Il peut être observé que la densité du photocourant montre un accroissement significatif à partir de 61 μ A/cm² à 8,67 mA/cm² (~ 150 fois) après le traitement avec HNO3, tandis qu'un accroissement considérable de la ~5 fois est observé avec le remplissage / la sensibilisation des points quantiques. Une application optique d'un détecteur photosensible et une application électrique d'un interrupteur accordable se également démontrent comme deux utilisations intéressantes de l'effet photovoltaïque BFO.

La recherche continue à prospérer dans le domaine des nouveaux matériaux ferroélectriques de BNDT et de BFO; un certain nombre d'études théoriques et sur l'application intéressantes sont actuellement en cours. Les résultats obtenus dans cette thèse-ci peuvent fournir une compréhension utile des principes et des propriétés des deux matériaux ferroélectriques et peuvent aider à la recherche en perspective à l'avenir.

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Yongyuan Zang July, 2012

Publications

All first-author peer-reviewed publications relating to Mr. Zang's novel ferroelectric research and its electrical and optical applications are listed below.

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[1] Y. Y. Zang, D. Xie, Y. Chen, X. Wu, T. L. Ren, H. W. Zhu, J. L. Cao, and D. V. Plant, "Investigation of the Improved Performance in a Graphene/polycrystalline BiFeO3/Pt Photovoltaic Heterojunction: Experiment, Modeling, and Application," *J. Appl. Phys.*, vol. 112, no. 5, pp. 054103 (10 pages), 2012.

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[2] **Y. Y. Zang**, D. Xie, M. H. Li, and D. V. Plant, "Temperature Dependence of Optical Properties of Nd-doped Bismuth Titanate Thin Film for Optical Application" *International Symposium on Integrated Functionalities*, 2011.

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List of Acronyms

Atomic force microscopy
Bismuth ferrite
Bipolar junction transistor
Bite line
La-doped bismuth titanate
Nd-doped bismuth titanate
Barium strontium titanate
Barium titanate
Bismuth titanate
Conductive atomic force microscopy
Complementary metal oxide semiconductor
Carbon nanotube
Chemical solution deposition
Chemical vapor deposition
Dynamic random access memory
Erasable programmable read only memory
External quantum efficiency
Ferroelectric dynamic random access memory
Ferroelectric field effect transistor
Ferroelectric random access memory
Full width at half maximum
Grain boundary limited conduction
High resolution transmission electron microscopy
Indium tin oxide
Molecular beam epitaxy
Multiple exciton generation
Micro electromechanical systems
Metal ferroelectric insulator silicon
Metal ferroelectric metal
Metal ferroelectric metal insulator silicon
Metal ferroelectric semiconductor
Metal organic chemical vapor deposition
Metal oxide semiconductor field effect transistor
Normal pressure and temperature
Photo conductivity decay
Polarization electric filed
Pulsed laser deposition
Pulsed common plate
Lead lanthanum zirconate titanate
Polymethyl methacrylate
Lead titanate

PV	Polarization voltage
PZT	Lead zirconate titanate
QDs	Quantum dots
RTA	Rapid thermal annealing
SA	Sensitive amplifier
SAW	Surface acoustic wave
SBT	Strontium bismuth tantalite
SEM	Scanning electron microscope
Sol-Gel	Solution-gelatin
SRAM	Static random access memory
TEM	Transmission electron microscopy
ТМ	Tapping mode
VOA	Variable optical attenuator
WDM	Wavelength division multiplexers
WDMA	Wavelength division multiple access
WL	Word line
XRD	X-ray diffraction
YIG	Yttrium iron garnet

Chapter 1

Introduction

erroelectric materials have attracted much research interest since their discovery in 1921 [1]. From the first ferroelectric phenomena reported in $NaKC_4H_4O_6 \cdot 4H_2O$ by Valasek [2] to the recently discovered room temperature ferroelectric BiFeO₃ (BFO) [3], research on ferroelectrics has continued ceaselessly over the past several decades. Initially, ferroelectric research focused mainly on the physical understanding of the ferroelectric mechanism and established a complete set of ferroelectric theories and models. Since the early 1960s, effort has been increasingly devoted to applying ferroelectric materials to various electrical and optical applications, because of their remarkable and unique electrical, dielectric, piezoelectric, and optical properties [4-6]. Many technically demanding applications, such as Ferroelectric Random Access Memory (FeRAM), ferroelectric piezoelectric microsensors and microactuators, ferroelectric microwave varactors, ferroelectric optical Microelectromechanical systems (MEMS), and ferroelectric solar cells, etc., have been actively investigated. Ferroelectric-based application devices all exhibit significant performance enhancements over those designed with traditional materials, indicating that ferroelectric materials hold promise for use in the next generation of electrical and optical applications [7-9].

1.1 Motivation

1.1.1 Ferroelectric random access memory

Memory technology is a fast growing field within modern electronics. With the development of chip technology predicted by Moore's Law [10], memory devices also have the potential to undergo a rapid and dynamic development. Large memory space, small device size, fast read/write speed, and good reliability, are the key concerns in modern memory device development. From the first integration with silicon CMOS in 1987 [11], Ferroelectric Random Access Memory (FeRAM) has been extensively investigated over the past two decades. Based on a simple one transistor, one ferroelectric capacitor (1T1C) structure, and on the ferroelectric polarization reversal by an external applied voltage, FeRAM has proven to exhibit superior performance than most existing non-volatile memory devices. Fig. 1.1 and 1.2 show a schematic illustration and a scanning electron microscope (SEM) image, respectively, of a 1T1C FeRAM unit [12]. It can be seen from Table 1.1 that FeRAM exhibits several attractive application features such as non-volatility, good radiation resistance, long fatigue endurance, fast write/read cycle time, and low power consumption. A great degree of industrial support from Ramtron, Infineon, Texas Instruments, Toshiba, etc., has been invested in FeRAM research since the late 1990s, and many commercial products of FeRAM have been released on the market. As the functional material in FeRAM, ferroelectric materials are of great interest to both academic and industry researchers. The investigation of ferroelectric materials, including basic electrical properties and the optimization of fabrication processes, can be valuable and directly impacts FeRAM development in the modern memory technology field.



Fig.1.1 Schematic illustration of 1T1C and 2T2C FeRAM cell structures [12].



Fig.1.2 Scanning electron microscope (SEM) image of serial 1T1C COP FeRAM cells in a 4 Mbyte memory, built using a 0.13µm five level Cu CMOS process [12].

	DRAM	SRAM	EEPOM	FLASH	FeRAM
Non-volatility	No	No	Yes	Yes	Yes
Radio-resistance	No	No	No	No	Yes
R/W endurance	unlimited	unlimited	10^{4} - 10^{6}	106	>10 ¹²
Speed (s)	10n	10 n	1-10 m	10 µ	50 n
Voltage (V)	2	2	12-18	12	<2

Table.1.1 Comparison of FeRAM with other existing memory technologies.

1.1.2 Ferroelectrics based microwave devices

With the development of wireless technology, electronic components working in high frequency regions become essential to the market. Very high Q values, narrow bandwidths, low power consumption, low insert loss, high isolation, and high operating speeds are of great concern in such microwave components [12-14], such as resonators, phase shifters, antennas, and tunable filters. However, in the RF-MEMS field in particular, traditional materials such as silicon, silicon dioxide, and silicon nitride, cannot provide efficient performance and competitive solutions due to the intrinsic nature of the materials, and new candidate materials are in demand in the microwave electronics field.

Recently, ferroelectric materials with ultra high dielectric constants, well-defined piezoelectric properties, and good magnetic performance, have been introduced into RF-MEMS related research. Many filters, resonators, and delays lines, used for the resonance of bulk or surface acoustic waves (BAWs or SAWs) are produced using ferroelectric materials such as LiTaO₃, and enhanced performance is demonstrated in such microwave related applications [8,12]. A ferroelectric-based resonator and a ferroelectric back-to-back resonator filler are shown in Fig.1.3 and Fig.1.4, respectively [15,16].



Fig.1.3 Schematic illustration of an yttrium iron garnet (YIG) and ferroelectric barium strontium titanate (BST) resonator [15].



Fig.1.4 Schematic configuration of the 3-pole back-to-back ferroelectric resonator filter [16].

Another interesting application of ferroelectrics in the microwave field is the ferroelectric-based varactor. As a component that is of similar importance as transistors, varactors are also widely used in microwave technologies for the purpose of analog tuning. In order to match the application development with market demand, the III-V semiconductor companies have put great effort into advancing existing CMOS and

bipolar junction transistor (BJT) technologies and have succeeded in producing commercial standard transistors with maximum oscillation frequencies above 100 GHz [8,12,17]. However, compared to developments achieved with transistors, no semiconductor-based varactor can provide a high enough Q factor even for frequencies above 10-20 GHz. In a typical semiconductor varactor, the Q value decreases proportionally with an increase in operational frequency, and falls below 10 when operated at 50 GHz; this effectively blocks any further development of this component in microwave electronics technology.

Reported in recent studies, the ferroelectric varactor may be employed to fulfill the need for a high Q factor component over this frequency gap. By using tunable permittivity ferroelectrics, it will be possible to make ferroelectric varactors with reasonable performance at frequencies above 10-20 GHz [8,17]. With larger Q factors, high tuning speeds, and low power consumption, the ferroelectric varactor and tunable devices have been proven to be a feasible solution for the high frequency microwave application, and can be well integrated with the standard silicon and GaAs fabrication processes. Moreover, due to the intrinsic high dielectric permittivity in ferroelectrics, the size of the ferroelectric varactor can be reduced significantly compared with CMOS technology, which provides extra freedom and flexibility for scaling down. A schematic illustration of a ferroelectric varactor and a typical varactor Q factor dependence on frequency are shown in Fig.1.5 and Fig.1.6, respectively [12].



Fig.1.5 Schematic illustration of parallel-plate and coplanar-plate ferroelectric varactor [12].



Fig.1.6 Q factor dependence on operational frequency [12].

1.1.3 Ferroelectric based optical applications

Optical applications are another important field in which ferroelectric materials can be used. Over the last few decades, ferroelectric materials such as PZT and PLZT have been extensively applied and investigated in photoelectron fields [18,19]. With remarkable optoelectronic properties, high optical transparency, a large electro-optic coefficient (10-20 times that of the traditional LiNbO₃ material), good thermal stability, and fast switching response, ferroelectric materials have been considered a promising candidate in the optical domain. In ferroelectric thin film based optical devices, the superior optical properties of the ferroelectric material, along with the design flexibility of thin film technology, offer more freedom in active optical applications and provide a number of innovative optical devices such as micro-actuators, waveguide devices, optical memories, optical phase retarders, optical and electro-optic switches, spatial light modulators, and devices based on optical phase conjugation [20]. Ferroelectric optical MEMS and ferroelectric-based E-O devices are two important application groups in the optical field, and the large piezoelectric coefficient and large E-O coefficient of ferroelectric materials provide a remarkable performance enhancement over traditional technologies.

1.1.4 Photovoltaic effect in ferroelectrics

Since the first report in Science 2009, the photovoltaic effect has been discovered and studied in ferroelectric BFO [21]. The obvious photovoltaic performance improvement in ferroelectric materials compared with traditional semiconductor p–n junctions is that the magnitude of the built-in electrical field that separates the photo generated carriers in the BFO crystal is nearly one order of magnitude higher than in a p–n junction. A higher band gap photo voltage and a significant photocurrent are reported by using single crystal BFO material of varying thickness and domain types [22,23]. As explained by the authors, such improved photovoltaic behaviour can be attributed to the domain walls of the ferroelectric material [22]. Another interesting phenomenon regarding this photovoltaic effect is that the output photo voltage can be tunable in ferroelectrics. Since ferroelectric domain structures can easily be modulated using an external electric field, by introducing

an external electric field higher than the ferroelectric coercive field, the photovoltaic voltage could be switched on and off, as well as flipped in polarity, after the manipulation of ferroelectric domain structures [24]. Additionally, due to the multiferroic nature of BFO, more control mechanics such as electricity, magnetism, heat, and stress, can be employed to determine the photovoltaic performance of the BFO material and can therefore be used to provide solar cells with novel functionalities [25].

1.2 Problem statement

1.2.1 Ferroelectric material: Selection and optimization

The family of ferroelectric materials has many group members. The first discovered ferroelectric material was Rochelle Salt [2]. In 1945, ferroelectric behaviour was reported in BaTiO3 [26]. Since then, a number of ferroelectric materials such as lead titanate (PbTiO₃), strontium bismuth tantalite (SBT), lead zirconate titanate (PZT), and lead lanthanum zirconate titanate (PLZT), have been discovered. Among all ferroelectric materials, the PZT material has been exploited extensively for various electrical [27-29] and optical [30-32] applications, due to its high remanent polarization value, high optical transmission, and strong electro-optic Kerr effect. However, PZT thin films are known to exhibit low fatigue endurance, especially when platinum is used as electrodes. As indicated by X. Du *et al.* [33], PZT thin films exhibit greater than 50% fatigue degradation after 10^9 switching cycles in fatigue resistance measurements.

Recently, Nd-doped Bismuth Titanate $B_{3.15}Nd_{0.85}Ti_3O_{12}$ (BNdT) was reported by Chon et al. [34] with a significantly larger remanent polarization ($2P_r=103 \ \mu C/cm^2$) compared to PZT. This surprisingly large remanent polarization can be attributed to the development of the polarization vector along the c-axis in the BNdT unit cell. Also, low fatigue degradation was observed in BNdT after 10¹⁰ switching cycles, indicating superior fatigue endurance versus PZT. There have been some studies based on the fabrication process and ferroelectric properties characterization of the BNdT material. However, a performance optimization process including an examination of different fabrication parameters and elemental constituent dependence of BNdT ferroelectric properties were not fully investigated, and research on this topic will provide a better understanding of the nature of the BNdT ferroelectric. This work will thus help to employ BNdT materials in more ferroelectric-based electrical applications.

1.2.2 Optical properties of ferroelectric materials

Since first being reported on by Chon *et al.* [34], there have been a number of papers published that discuss the electrical properties of the BNdT ferroelectric material, confirming the advantages of using this material in electrical related applications [35-37]. However, so far little attention has been paid to the optical properties of the BNdT material. There was one study regarding the band gap energy fitting from an ellipsometer measurement [38], which provided a basic theoretical understanding of the optical properties of BNdT material. However, a detail optical investigation including parameters such as transmittance T, refractive index n, extinction coefficient k, etc., was not performed in its entirety. To the best of our knowledge, there has been no systematic investigation of the optical properties of the BNdT material. Furthermore, different impact mechanisms such as the crystallization temperature, quantum scale, and ingredient substitution, of the BNdT thin film optical properties are never reported. Research on the
optical properties of BNdT and its optimization process will offer a useful understanding of the correlation between the structure and the optical properties of the material, and thus provide more information for the future optical applications of the BNdT material.

1.2.3 Ferroelectric properties enhancement

Recently, BiFeO₃ (BFO) has been recognized as a promising room temperature multiferroic material that exhibits a ferroelectric phase transition and an antiferromagnetic phase transition simultaneously [39]. Such room temperature multiferroic behaviour offers BFO more flexibility in electrical and magnetic related applications. However, the polarization properties of the BFO materials are only examined at low temperature [39], due to the low electric resistivity of the BFO material at room temperature; this is considered an obstacle which blocks the further application of the BFO material at room temperature. The relatively low electric resistivity of BFO may be attributed to the valence fluctuation of Fe ions (Fe^{2+} and F^{3+}), which requires oxygen vacancies for charge compensation and produces electron hopping in films. In order to improve the polarization properties of BFO at room temperature, the site-engineering concept has been proposed. Bi-site substitution with La and Nd atoms for controlling volatile Bi atoms and suppressing oxygen vacancies generation has been attempted in BFO thin films [40,41]. Meanwhile, Fe-sited substitution using Nb or Mn atoms have been reported by S. K. Singh and C.F. Chung et al. [42,43] to fill oxygen vacancies in bulk ceramics. However, un-doped BFO thin films still provide poor remnant polarization at room temperature, and research in improving the room temperature ferroelectric properties of pure BFO is necessary and will prove valuable to the ferroelectric research.

1.2.4 Ferroelectric photovoltaic effect and its principles

Since the first report in late 2009, there have been a few studies on the photovoltaic effect of the BFO material. Among the published works, T. Choi et al. [21] first reported the photovoltaic effect and a direction of bulk electric polarization induced diode behaviour in a single domain BFO crystal; S. Y. Yang et al. [22] demonstrated the electrical field control over the domain structure in a BFO crystal and revealed the nature of the high photovoltaic voltage in the BFO material; W. Ji et al. [44] studied the epitaxial BFO crystal by sputtering deposition and examined photovoltaic performance dependence on polarization. However, most of the research has focused on the single crystalline BFO and little work has been done towards investigating the polycrystalline BFO. To the best of our knowledge, there is only one report by B. Chen et al. [45] that presents the effect of the top electrode (ITO and Au) on the photovoltaic response of the polycrystalline BFO, with work that endeavors to investigate the photovoltaic properties in the sol-gel derived BFO crystal. In fact, though single crystalline BFO derived by epitaxy technology can exhibit well-defined photovoltaic properties, the single crystalline fabrication process is very complicated and costly, and cannot be widely applied in largescale productions. The polycrystalline BFO fabricated using the sol-gel method has been proven to be an effective and feasible candidate in commercial ferroelectric devices, and research on the polycrystalline BFO photovoltaic effect can be an interesting topic from the commercial perspective. Meanwhile, most of the existing photovoltaic studies are focused on the experimental aspect, with few theoretical models having been proposed for depicting the carriers' transportation behaviour during the ferroelectric photovoltaic process. Attaining and investigating the theoretical model can be an important milestone in understanding the photovoltaic behaviour of the BFO material and can provide us with more theoretical support in further BFO photovoltaic applications. Moreover, all of the work has used indium tin oxide (ITO) or metal (Au or Pt) as top electrodes, and searching for an alternative transparent electrode and investigating the transparent enhancement to the photovoltaic performance is always a key goal in photovoltaic research [23,45,46].

1.3 Research objective

The work conducted in this thesis aims to provide a systemic investigation of ferroelectric materials and their electrical and optical applications. Both experimental and theoretical examinations will be presented in detail. Broadly speaking, our research can be divided into three phases. First, we start with fabrication of the ferroelectric material, demonstrating a comprehensive ferroelectric parameter characterization and optimization. Second, with the optimized ferroelectric material, experimentally and theoretically, and supplement the latter with a deeper understanding of ferroelectric optical parameters for the first time. In the third phase, we advance our research into an innovative field of ferroelectric research, which arose in late 2009, namely, the photovoltaic effect and its applications; and fill some gaps existing in the development of ferroelectric photovoltaic research.

1.4 Original contribution

As will be presented in the forthcoming chapters, our study provides novel contributions to the field of ferroelectrics research; none of this work has been previously demonstrated. Evidence of the originality of our work is manifested through a series of peer-reviewed publications based on our research, which can be found listed in the Associated Publications Section of this thesis.

More specifically, the original contributions involved with each chapter are highlighted and listed as follows.

Chapter 3: Ferroelectric Properties and Optimization

• Investigate and optimize the fabrication method of the BNdT ferroelectric material.

• Explore the BNdT ferroelectric properties dependence on different fabrication parameters and elemental constituents.

Chapter 4: Optical Properties of Ferroelectrics and their Optimization

• Conduct a comprehensive optical investigation of the BNdT ferroelectric material.

• Present an experimental and theoretical investigation of the ferroelectric optical parameters dependence on fabrication parameters.

Chapter 5: Multiferroic and Optimization

• Establish and characterize a BFO/BNdT multilayer ferroelectric structure.

• Succeed in measuring the room temperature ferroelectric remnant polarization of pure BFO using the BFO/BNdT multilayer structure.

Chapter 6: Ferroelectric: Photovoltaic Effect and Theoretical Modeling

• Report the first photovoltaic enhancement of polycrystalline BFO ferroelectrics in a graphene/BFO heterojunction.

• Establish the first ferroelectric photovoltaic theoretical model and explain the carriers transportation behaviour.

Chapter 7: Photovoltaic Performance Enhancement and Application

• Investigate the first chemical and physical enhancements of the BFO photovoltaic performance, experimentally and theoretically.

• Implement the first optical application using the BFO photovoltaic effect.

Associated publications

The evidence of the original contributions to the overall existing body of the thesis is manifested by the 6 peer-reviewed journal articles, as follows.

[1] **Y. Y. Zang**, D. Xie, Y. Chen, X. Wu, T. L. Ren, H. W. Zhu, J. L. Cao, and D. V. Plant, "Investigation of the Improved Performance in a Graphene/polycrystalline BiFeO3/Pt Photovoltaic Heterojunction: Experiment, Modeling, and Application," *J. Appl. Phys.*, (Under minor revision)

[2] **Y. Y. Zang**, D. Xie, Y. Chen, X. Wu, T. L. Ren, J. Q. Wei, H. W. Zhu, and D. V. Plant, "Electrical and Thermal Properties of a Carbon Nanotube/Polycrystalline BiFeO3/Pt Photovoltaic Heterojunction with CdSe Quantum Dots Sensitization," *Nanoscale*, vol. 4, pp. 2926-2930, 2012.

[3] Y. Y. Zang, D. Xie, Y. Chen, M. H. Li, C. Chen, T. L. Ren, and D. V. Plant, "Temperature dependence of optical and structural properties of ferroelectric B3.15Nd0.85Ti3O12 thin film derived by sol–gel process," *J. Sol-Gel Sci. Technol.*, vol. 61, no. 1, pp. 236-242, 2012.

[4] Y. Y. Zang, D. Xie, Y. Chen, M. H. Li, X. G. Han, T. L. Ren, and D. V. Plant, "Comparative Study on Structural and Ferroelectric Properties of Dual-Site Rare-Earth ions Substituted Multiferroelectric BiFeO3," *Integr. Ferroelectr.*, vol. 132, no. 1, pp. 3038, 2012.

[5] **Y. Y. Zang**, D. Xie, Y. Chen, X. Wu, G. Li, and D. V. Plant, "Tuning the Structural and Optical Properties of Bismuth Titanate by Different Nd Substitution Content," *Integr. Ferroelectr.*, vol. 133, no. 1, pp. 73-80, 2012.

[6] **Y. Y. Zang**, D. Xie, X. Wu, Y. Chen, Y. X. Lin, M. H. Li, H. Tian, X. Li, Z. Li, H. W. Zhu, T. L. Ren, and D. V. Plant, "Enhanced photovoltaic properties in graphene/polycrystalline BiFeO3/Pt heterojunction structure," *Appl. Phys. Lett.*, vol. 99, no. 13, pp. 132904 (3 pages), 2011.

1.5 Thesis overview

Following this introductory chapter, the organization of the remainder of the thesis is as follows.

Chapter 2 provides the current state of the art in ferroelectric material research. We start with an introduction to ferroelectric properties, including ferroelectric mechanisms, fabrication methodologies, and ferroelectric performance characterization. Then, ferroelectric-based electrical applications such as Ferroelectric Random Access Memory (FeRAM) and the Ferroelectric Field Effect Transistor (FeFET) are briefly introduced. We discuss current optical applications based on ferroelectric materials, such as ferroelectric optical MEMS and ferroelectric-based EO devices. Finally, the ferroelectric photovoltaic effect and its current research progress are presented.

In Chapter 3, we investigate the fabrication process of the $Bi_{4-x}Nd_xTi_3O_{12}$ (BNdT) ferroelectric thin film, and obtain an optimized fabrication routine for further applications. We start with a discussion of the fabrication principle, and present the fabrication process

of the BNdT ferroelectric thin film utilized in this work. Second, we continue to analyze the structure, and show the obvious impacts of the fabrication conditions on BNdT microstructure properties. Third, the ferroelectric and electric properties of the BNdT thin films are investigated, and an optimized fabrication condition is obtained based on these studies. Finally, the effect of Nd doping concentration on the BNdT thin film optimization process is evaluated.

Chapter 4 presents the first systemic study on the correlation between different impact mechanisms and the optical properties of the BNdT material. We start with a theoretical analysis and introduce three different impact mechanisms, namely crystallization temperature, quantum scale effect, and ingredient substitution, on the optical properties of BNdT material. Then, we independently evaluate the effect of these three impact mechanisms on the BNdT optical properties.

In Chapter 5, we explore various attempts to optimize the ferroelectric properties of BFO material and realize room temperature characterization of the BFO material. We start with a multilayer methodology to study the room temperature enhancement of the BFO ferroelectric material. Fabrication technology, structural analysis, ferroelectric characterization, and dielectric examination are described in detail in this chapter. Then, we move on to another optimization approach, namely, dual-site substitution technology. We process the corresponding characterization, as well as a characterization of dual-site substituted BFO materials, demonstrated both experimentally and theoretically.

Chapter 6 presents an investigation of the enhanced photovoltaic properties in a graphene/BFO/Pt photovoltaic heterostructure. An equivalent electrical and thermal model is first proposed to aid in the understanding of carriers transportation behaviour.

We start with an introduction of a five-step fabrication process for the graphene/BFO/Pt heterojunction, followed by basic performance characteristics of the BFO material and graphene top electrode. Then, with band diagram construction, we establish an equivalent electrical model and calculate the BFO photocurrent *J-V* curves in theory. Third, we demonstrate a detailed photovoltaic characterization of the graphene/BFO/Pt heterojunction, and by using the theoretical model all aspects of photovoltaic performance are investigated experimentally and theoretically.

In Chapter 7, we further our BFO photovoltaic research on performance enhancements and the photovoltaic application. To start, we demonstrate the HNO₃ treatment and photovoltaic enhancement of the graphene/BFO/Pt. With comparison between the experimental result and theoretical calculation, the nature of this chemical routine is reported. We then introduce a study on physical improvements. The quantum dots (QDs) sensitization process is explained and examined. As a comparison, we also examine the chemical approach and the physical routine in the enhancement of the BFO photovoltaic effect. Finally we apply our graphene/BFO/Pt photovoltaic heterojunction to the optical and electrical fields; and a photo detector and tunable switch are built and their behaviour demonstrated in detail.

Finally, this thesis is summarized in Chapter 8. We conclude and reiterate the central points report in this study, and also provide ideas on the direction of future work and other research perspectives.

Chapter 2

Review of Current State-of-the-Art Research

2.1 Introduction

he study of ferroelectric materials and their applications has been widely reported over the past several decades, and significant research is still being dedicated to this now flourishing field. A number of research milestones, such as a comprehensive ferroelectric phenomenological theory and ferroelectric-based electrical/optical applications, have been achieved in this field. In this chapter, we will present the background and current progress of ferroelectrics research. This literature review will help provide a solid understanding of the principles and unique properties of ferroelectric materials, and will serve as an important theoretical basis for the forthcoming chapters. More specifically, in Section 2.2, we start with a brief introduction to the ferroelectric principle, followed by a review of current work on ferroelectric materials. Different fabrication technologies for ferroelectric materials, and a comparison of their advantages and disadvantages are also presented in this section. Section 2.3 presents ferroelectric-based electrical applications. As typical applications, ferroelectric random access memory (FeRAM) and ferroelectric field effect transistor (FeFET) are described in detail. In Section 2.4, we continue our discussion with ferroelectric-based optical applications, and present current applications of ferroelectric based optical MEMS

and EO devices. In Section 2.5, the photovoltaic effect of ferroelectric materials and related ongoing research is reviewed in detail.

2.2 Ferroelectric: Principles and material research

2.2.1 Ferroelectric principles

Ferroelectric materials are defined as a type of material that can possess spontaneous polarization in a certain temperature region with external stimulation, and the intensity and direction of the spontaneous polarization field can be modulated by external stimulation, typically an external applied electric field. From the definition, it can be noted that as a unique group of materials, ferroelectrics are recognized as a kind of *polar* material. They have two basic features, namely, the existence of spontaneous polarization and the ability to switch between these spontaneous polarizations. In fact, since the discovery of the first ferroelectric in Rochelle Salt (NaKC₄H₄O₆·4H₂O), more than 200 ferroelectric materials have been discovered and reported on [2]. Ferroelectric materials

From the crystallographic point of view, a dielectric medium that possesses a specific crystal structure can have ferroelectric properties and can be regarded as a ferroelectric material. As indicated in crystallographic point groups' theory, there are 32 crystallographic point groups in total, 10 of which are polar point groups. Only crystals that belong to these 10 polar point groups can exhibit spontaneous polarization. All spontaneous polarized crystals possess the common property that the state of the spontaneous polarization varies with the environmental temperature; such polarization dependence on temperature is defined as pyroelectricity [12]. Due to the spontaneous

polarization, the polar medium lacks central symmetry, a property that leads to piezoelectricity in the polar crystal. In other words, the spontaneous polarization can be affected by external mechanical stress and strain [12,47,48]. In ferroelectrics, the existence of spontaneous polarization is not only necessary, but it also must possess two or more orientations in the absence of an external electric field, and be able to be switched from one state to the other by applying an electric field [49]. From the definition, it can be concluded that all ferroelectric materials must be polar materials, with two or more spontaneous polarization orientations, and they all possess pyroelectricity and piezoelectricity. Due to the strong structural dependency of ferroelectric materials, most of the oxidated octahedral crystals, such as perovskite crystals, tungsten bronze crystals, and bismuth layer-structured crystals, are ferroelectrics. From a macroscopic point of view, spontaneous polarization in such crystals is attributed to the structural deformation caused by switching between the high valence numbers, and the small radius cation in the central of the octahedron.

As a typical example of ferroelectric crystals, perovskite crystals with an ABO₃ structure have been widely investigated and applied. Take for instance PbTiO₃ (PT): in its cubic perovskite phase Pb²⁺ ions occupy the vertices of the cube and O²⁻ ions stay on the face centers of the cube, thereby forming an oxidized octahedron. A Ti⁴⁺ ion occupies the center of the cube, i.e. the center of the oxidized octahedron. Such a PbTiO₃ crystal structure is defined as having paraelectric phase and there exists no spontaneous polarization in this phase, as shown in Fig.2.1 [50]. When the temperature is less than 490°C, the crystal structure deforms into a tetragonal perovskite phase, where two different polarization states arise. The relative upper or lower displacement of Ti⁴⁺

compared with other atoms leads to a net electrical dipole moment of dozens of μ C/cm², also called spontaneous polarization P_s . In the untreated PbTiO₃ crystals, it can be found that the spontaneous polarization exhibits an unordered orientation distribution, resulting in a random ferroelectric domain distribution. When a large enough external electric field is applied to the sample, all of the ferroelectric domains will be switched to the same direction, and we can thus change the ferroelectric domain orientation by switching the direction of the external electric field. This process can be regarded as switching between two independent states, namely polarization up (known as "0") and polarization down (known as "1").



Fig.2.1 Schematic illustration of the PbTiO₃ crystal structure [50].

The switching of spontaneous polarizations in ferroelectrics is known as the ferroelectric hysteresis loop. Fig.2.2 shows a typical hysteresis loop [51]. It can be seen that the shape of the loop is similar to the one-dimensional magnetic hysteresis loop; this is where the name *hysteresis loop* comes from. The polarization of the ferroelectric varies

with the external electric field. When the electric field is large enough, the ferroelectric polarization reaches saturation. Polarization decreases with decreasing external electric field, but when electric field reaches zero the ferroelectric polarization is a non-zero value, called remnant polarization (P_r). The remnant polarization is an important parameter in ferroelectric-based applications. When the electric field reaches a certain value, the ferroelectric polarization becomes zero; the electric field at this point is called the coercive field (E_c). It should also be noted that the remnant polarization value is stable. Ignoring the fatigue effect, both of these two remnant polarization states (P_{r+} and P_{r-}) are permanent without a large external electrical field, stress, or thermal stimulation; this is the principle underlying the non-volatility of ferroelectric based memory devices.



Fig.2.2 Typical ferroelectric hysteresis loop [51].

Temperature is an important parameter in determining the performance of ferroelectric materials. Ferroelectric materials can only exhibit ferroelectric properties within a specific temperature region. When the temperature exceeds a certain value, spontaneous polarization will disappear and the ferroelectric material will degrade into a paraelectric [52]. This transformation temperature is called the Curie temperature (T_c). The ferroelectric dielectric constant and permittivity will also exhibit an abnormal tendency to vary when the temperature passes the Curie temperature. In the paraelectric phase, the ferroelectric permittivity follows the Curie-Weiss Law as [53],

$$\varepsilon = C \cdot (T - T_0)^{-1} \tag{2.1}$$

where ε is the low frequency ferroelectric permittivity, *C* is Curie constant of the material, and T_0 is the Curie-Weiss temperature. In second-order phase transition ferroelectrics where the ferroelectric polarization exhibits a continuous variation, $T_0=T_c$. In first-order phase transition ferroelectrics where the ferroelectric polarization jumps with an increase or decrease in temperature, $T_0 < T_c$. Such a dielectric anomaly leads to a large dielectric constant in most ferroelectric materials. Fig 2.3 shows the dielectric constant and spontaneous polarization variation pattern of the PbTiO₃ ferroelectric [54]. In fact, the ferroelectric dielectric constant exhibits correlation with many factors besides temperature, such as applied voltage, chemical constituent, grain size, crystal axis, etc [55]. For example, Ba_{1-x}Sr_xTiO₃ exhibits a dielectric peak when x=0.3 and BaTiO₃ (BT) shows the largest dielectric constant when the grain size is between 0.7 to 1.0 µm. Further, in the tetragonal BaTiO₃ crystal, along the c-axis the dielectric constant is 400 whereas perpendicular to c-axis the dielectric constant is 4000 [56].



Fig. 2.3 PbTiO₃ dielectric constant and spontaneous polarization dependence on temperature [54].

Along with the properties of piezoelectricity, pyroelectricity, ferroelectricity, and high dielectric constant introduced above, ferroelectrics also exhibit anti-radiation properties, electrostriction properties, the electro-optic effect, nonlinear optical properties, and the photo-refractive effect. All of these properties make ferroelectrics promising candidates in many technically demanding applications [57-60].

2.2.2 Ferroelectric materials research

The first ferroelectric phenomenon was reported in Rochelle Salt (NaKC₄H₄O₆·4H₂O) by Valasek in 1920 [2], starting the saga of ferroelectric materials research. In 1930, scientists in Zurich reported a series of ferroelectric phosphates, the best-known representative of which is KH₂PO₄ (KDP) [61]. It has been indicated that all phosphates with a similar crystal structure to KDP exhibit certain ferroelectric properties. In 1945, ferroelectric behaviour was found in BaTiO₃ [26]. Since then, many other ferroelectric materials, such as lead titanate (PbTiO₃), strontium bismuth tantalite (SBT), lead zirconate titanate (PZT), lead lanthanum zirconate titanate (PLZT), have been springing up around the world. Now, ferroelectric materials are a big family that includes more than 200 members; most of such materials are from Pb-Zr-Ti-O, Ta-Bi-Sr-O, Sr-Ba-Nb-O, Ba-Ti-O, and Bi-Ti-O serial metallic compound materials.

Amongst all ferroelectric materials lead zirconate titanate $PbZr_0 {}_5Ti_0 {}_5O_3$ (PZT), discovered in 1952, has attracted significant research interest due to its high remanent polarization value (~35 µC/cm²), high optical transmission, and strong electro-optic Kerr effect. As well, a number of electrical [62-66] and optical applications [67,68] can be processed on PZT material. However, the PZT material demonstrates poor fatigue endurance when integrated with platinum electrodes, and more than 50% fatigue degradation upon 10^9 switching cycles was reported in fatigue resistance measurements. [33]. Also, the plumbiferous nature of PZT may not meet environmental-friendly criteria in innovative materials development and applications. Notable alternatives to PZT were extensively investigated and Bi-based compounds were claimed to possess the most improved fatigue endurance in electrical applications. More specifically, the lead free material strontium bismuth tantalite SrBi₂Ta₂O₉ (SBT) was reported in 1991 as the most feasible replacement of PZT material [12,69]. In contrast to PZT, SBT displays no apparent fatigue degradation on Pt electrodes. A schematic illustration of a SBT crystalline structure is shown in Fig.2.4 [70]. It can be seen that SBT possesses a bismuth-layered perovskite structure. A doubled-layered Ta-O anatase structure is secured in place between $(Bi_2O_2)^{2+}$ layers. There are net charges in the $(Bi_2O_2)^{2+}$ layers, which can be used to compensate for the space charge in the crystal and thus help improve the fatigue performance of SBT material. SBT can also operate at a lower switching voltage, and thus decreases power consumption in a FeRAM application.



Fig.2.4 Schematic illustration of the SBT crystal structure [70].

However, the switchable polarization charge of SBT is much lower than for the traditional PZT material. Another disadvantage of SBT, which may constrain its further application, is the processing and fabrication concerns. The crystallization temperature of SBT is significantly higher (150°C -200°C) than that of PZT. Though it is not a big issue in laboratory research, with the increase of device density, especially under integration with standard CMOS transistors, high process temperatures will lead to a compatibility issue in electrical and optical applications [71]. Therefore, the search for an ideal ferroelectric material is still of great importance in research circles today and work is continually being performed in this field.

In 1999, B. H. Park *et al.* [72] reported an innovative ferroelectric material made by replacing part of the Bi⁺ ions in the traditional Bi₄Ti₃O₁₂ (BTO) crystal with La⁺ ions; they named this new ferroelectric BLT (Bi_{4-x}La_xTi₃O₁₂), as shown in Fig.2.5 [73]. Experiments have shown that when x=0.75, the BLT compound demonstrates the largest

remnant polarization. BLT also exhibits well-defined fatigue endurance, and little fatigue deformation can be found upon 3×10^{10} switching cycles. Thereafter, lanthanide ions (La, Sm) substituted BTO ferroelectric materials have been widely studied and reported. Unfortunately, BLT materials are always derived using pulsed laser deposition (PLD), which is expensive in large-scale production and can only be used in laboratory studies.



Fig.2.5 Schematic illustration of the BLT crystal structure [73].

In 2002, U. Chon *et al.* [34] reported a novel ferroelectric material BNdT (Bi_{4-x}Nd_xTi₃O₁₂) with remarkable ferroelectric properties, created by replacing some Bi⁺ ions in the BTO with Nd⁺ ions. In the highly c-axis orientated BNdT, the remnant polarization $(2P_r)$ can reach 103 μ C/cm², compared with that of 30 μ C/cm² in the BLT material. Also, BNdT exhibits remarkable fatigue endurance under 6.5×10^{10} switching cycles. As explained by the author, this unexpected phenomena results from orientation of the polarization vector along the c-axis of the BNdT unit cell. The expected consequence of the higher c-axis orientation achieved in the BNdT material is that the remnant polarization will be higher [74].

Recently, multiferroic materials have attracted ample research interest due to their unique ferroelectric and ferromagnetic coupling [75]. The coupling of the electric and magnetic polarization provides an extra degree of freedom in device applications such as data storage, spintronics, sensors, actuators, and micro-electromechanical systems (MEMS) [76-77]. As reported by J. Wang *et al.* [3], multiferroic BiFeO₃ (BFO), as shown in Fig.2.6, has been considered among promising room temperature multiferroic candidates, since it exhibits both a ferroelectric phase transition at a high Curie temperature (T_{C} ~850°C) and an anti-ferromagnetic phase transition at a high Néel temperature (T_N ~370°C), rendering it both ferroelectric and ferromagnetic simultaneously [39,78,79]. Compared with other multiferroic materials which can only exhibit co-existing ferroelectric and ferromagnetic phase at ultra low temperatures, BFO can be utilized in novel memory applications at room temperature.



Fig.2.6 Schematic illustration of the BFO crystal structure [3].

However, due to an intrinsic constraint of the BFO material, it is difficult to characterize the ferroelectric properties of the pure phase BFO at room temperature [80,81]. The low resistivity of BFO is at the root of this phenomenon. During the annealing process, the density of oxygen vacancies reaches a dynamic balance at high temperatures. When the material cools down, some of the oxygen vacancies are stranded into assembled oxygen vacancies groups, resulting in an unbalanced oxygen distribution. Such an inequilibrium leads to a Fe atom valence variation from Fe^{3+} to Fe^{2+} , resulting in a large conductivity, and thus increasing the leakage density of the BFO material. On the other hand, BFO also possesses low dielectric constant and resistivity; this creates some difficulty in characterizing a saturated ferroelectric hysteresis loop at room temperature. To reduce the conductivity of BFO and measure the room temperature BFO ferroelectric properties, different routines such as single phase technology [82], a formation of solid solution with other ABO₃ pervoskite materials [83], and ion atoms substitution at Bi and Fe sites in the BFO crystal [84] have been widely investigated with some promising results having been achieved thus far.

2.2.3 Ferroelectric fabrication technology

In modern electrical and optical applications, ferroelectric materials are always used in the form of a thin film. There are many fabrication technologies for ferroelectric thin films, and most of the existing thin film fabrication technologies have already been attempted on ferroelectric materials. There are four major fabrication routines used in laboratory research and in commercial development; they are discussed in turn below.

Sputtering

In sputtering technology, a high-energy particle stream bombards the target material, and the target atoms fall and depose onto the surface of the substrate, thereby forming the desired material thin film, as indicated in Fig.2.7 [85]. Sputtering is a mature technology that was used in early titanates and bismuth ferroelectric thin film preparations. It has wide application perspectives for modern ferroelectric material thin film deposition. Due to the high energy of the sputtering particle stream, thin films prepared by sputtering can always exhibit a high surface mobility in electrical applications.



Fig.2.7 Schematic illustration of the sputtering technology [85].

The advantages of sputtering can be summarized as follows:

(1) The thin film achieved can exhibit a well-defined degree of crystallization, and with

appropriate fabrication parameters even single crystal thin film can be obtained;

- (2) A low fabrication temperature;
- (3) Good compatibility with the CMOS integration process;
- (4) Flexibility in depositing various kinds of ferroelectric materials.

However, there are also some disadvantages with using sputtering technology, such as the low deposition rate, small guaranteed chip area, and the constituent variation at different chip locations. Recently, many optimized sputtering technologies, such as RF sputtering, reactive sputtering, multiple targets sputtering, and ion beam sputtering, have been widely reported in fabricating ferroelectric thin films such as BaTiO₃, Bi₄Ti₃O₁₂, and SrBi₂Ta₂O₉. FeRAM from Ramtron is also fabricated using RF sputtering technology.

Pulsed Laser Deposition (PLD)

In PLD technology, a high intensity pulsed laser beam created by an excimer laser is focused on the surface of the target, heating and fusing the target material into a high temperature and high pressure plasma. This plasma expands and emits in a specific direction, and deposits on the heated substrate surface. Fig.2.8 shows a schematic depicting the PLD technology [86]. The advantages of the PLD method can be summarized as follows,

(1) Capable of fabricating complex constituent ferroelectric thin films;

(2) Introduces active gases such as oxygen, and can improve the crystallization quality of most multi-oxide ferroelectric materials;

(3) Capable of depositing multilayer thin films;

- (4) Provides a well-defined ferroelectric crystal structure;
- (5) Can have an in-situ annealing process for the deposited thin film.



Fig.2.8 Schematic depicting of the PLD technology [86].

PLD technology was initially used in depositing TC superconductive thin films. It has now been successfully applied to fabrication of ferroelectric thin films such as PZT, PLZT, and BST. However, the high cost and low yield make it inappropriate for largescale production, and it is for this reason that the technology is currently widely used only at the laboratory research level.

Sol-gel method

In the Sol-gel method, different metal alkoxides are dissolved into a predetermined solvent, and react into a complex alkoxide. With the help of the solvent and catalyst, complex alkoxide hydrolyzes or alcoholizes into solution and gelatin. A ferroelectric thin film can then be obtained using spin coating technology, drying, and sintering. There are two major steps that ensure the success of the sol-gel technology, namely, obtaining a stable solution and effective control over the condensation reaction during the gelation process. In order to obtain a stable solution, the following criteria for the metal alkoxides solute should be met:

- (1) Rich in metal content;
- (2) High solubility in the solvent;
- (3) No melting or evaporating during the drying and annealing processes;
- (4) Stable at room temperature.

The annealing temperature and ramping rate are two important parameters in sol-gel technology. The annealing temperature determines the final crystal structure achieved in the ferroelectric thin film. For example, the annealing temperature can fully determine the pyrochlore or perovskite structures in the as-prepared thin film. Meanwhile, the ramping rate determines the stress relaxation process and thus the microstructure of the thin film.

Sol-gel technology has several advantages including low cost, high production yield, high deposition rate, and that it is a promising fabricating method in large-scale commercial production. On the other hand, the crystals prepared using sol-gel are always polycrystalline, and may not compare with the materials achieved using other physical deposition methods such as PLD and RF sputtering. Many ferroelectric materials, such as PbTiO₃, PZT, PLZT, BaTiO₃, KNbO₃, Bi₄Ti₃O₁₂, and (Sr, Ba)NbO₃, have been reportedly fabricated using the sol-gel method.

Metal organic chemical vapor deposition (MOCVD)

In MOCVD technology, the metal organic chemical vapor is transported into the reaction chamber, decomposed and deposited on the surface of the heated substrate. Fig.2.9 shows a schematic illustration of the MOCVD process [87]. The vapor sources are always hydroxyl compounds, alkoxide, and aryl compounds. The advantages of MOCVD technology can be summarized as follows:

- (1) Low substrate temperature;
- (2) High growth rate;
- (3) Precise control in element constituent;
- (4) Large area of uniformity and consistency;
- (5) Can be deposited on non-planar substrates to directly fabricate a patterned device;
- (6) Suitable for large-scale commercial fabrication.



Fig.2.9 A schematic illustration of the MOCVD process [87].

There are more than ten ferroelectric materials including PZT, $PbTiO_3$, and $BaTiO_3$, that can be grown using MOCVD; however, due to limited suitable source vapors, many ferroelectric materials cannot yet be fabricated using this technology. Research and development for innovative, low volatilization temperature, and low toxic MO sources are still popular topics in the MOCVD field.

2.3 Ferroelectric based electrical application

In 1987, the first ferroelectric-based memory device was reported in the U.S., and significant attention has been paid to this thriving field ever since. Many academic and industrial institutions have invested substantial effort in the investigation and commercialization processes of this new technology, which also accelerates the development of ferroelectric-based electrical applications. As introduced in Chapter 1,

ferroelectric-based memory devices demonstrate remarkable application advantages over other existing memory devices. Due to their nonvolatile nature and unique ferroelectric related properties, ferroelectric based memory devices can not only replace existing nonvolatile memory devices, but may also be employed in novel applications that were unfathomable with traditional memory devices. For instance, ferroelectric based memory devices can be used in aerospace applications because of their significant anti-radiation resistance; and they can be employed in specific applications such as TV channel memories, digital memories for game machines, and counters for odometers or printers, owing to their well defined Read/Write endurance. This type of device could also be introduced into memory units in mobiles, beepers, and Radio frequency identifications (RFID), thanks to its natural low power consumption. Moreover the device's reprogrammability, low power consumption and long lasting properties make it a promising candidate in IC card related applications. In fact, some semiconductor companies have already begun research on integrating ferroelectric materials into the non-contact IC card application.

The operating principle of ferroelectric based memory devices is that the ferroelectric thin film memory unit can be polarized into two different polarization states (P_r + and P_r -) by an external electric field, and these two states can be regarded as "1" and "0", respectively, thus effectively realizing binary storage. There are two major application forms of ferroelectric based memory devices, namely, Ferroelectric Random Access Memory (FeRAM) and Ferroelectric Field Effect Transistor (FeFET).

2.3.1 Ferroelectric random access memory (FeRAM)

The operating principle of FeRAM is based on the ferroelectric spontaneous polarization, making FeRAM a kind of nonvolatile memory device. FeRAM has the fast Read/Write feature of static random access memory (SRAM), the high integration density of dynamic random access memory (DRAM), the nonvolatility of read only memory (ROM), and can be widely applied to many technically demanding applications.

In general, FeRAM has three different application structures, namely 1T1C, 2T2C and Chain structure. In the 2T2C structure, the cell circuit of FeRAM is similar to that of DRAM. In Fig.2.10, the schematic of one 1T1C ferroelectric memory unit is shown. One side of the ferroelectric capacitor is connected to the bit line (BL) through a MOSFET, for which ON/OFF is controlled by a word line (WL), and the other side is connected to a pulsed common plate (PLP) [88]. If two such memory units are operated as a pair, storing opposite data information, they can operate as a reference for each other. By employing a sensitive amplifier (SA) connected to the BL output, such a ferroelectric memory unit composed of two MOSFETs and two ferroelectric capacitors is defined as a 2T2C unit, as shown in Fig.2.11 [88]. The 2T2C unit is the most common FeRAM unit. It possesses high reliability and low design complexity. However, the large occupied chip area in such a structure does not meet the high-density design principle requirements. Compared with the 2T2C unit, the 1T1C unit saves 50% of the chip area, which is beneficial to the highdensity design. However, the generation of a reference signal and the reliability of the design involve more design and fabrication issues.



Fig.2.10 Schematic diagram of a 1T1C FeRAM unit [88].



Fig.2.11 Schematic diagram of a 2T2C FeRAM unit [88].

In the chain structure, shown in Fig.2.12 [89], multiple 1T1C FeRAM units are placed in series, and the ferroelectric capacitors are short-circuited by MOSFETs when accessed. Compared with the traditional memory structure, such chain structures exhibit a more compact design and can be employed in ultra high-density circuit applications.



Fig.2.12 Schematic diagram of a FeRAM chain [89].

2.3.2 Ferroelectric field effect transistor (FeFET)

An alternative approach to ferroelectric based nonvolatile storage is the ferroelectric field effect transistor (FeFET). Fig 2.13 (a) shows a cell diagram of a 1T FeFET cell, where a ferroelectric layer replaces the gate oxide layer on a typical MOSFET [12]. Using a ptype substrate, for example, the operating principle can be explained as follows. When the gate voltage exceeds the threshold voltage, a conducting channel is established between the source and drain. Unlike with the traditional MOSFET, an external applied voltage polarizes the ferroelectric thin film, and when the gate voltage is removed the conducting channel still exists due to the ferroelectric remnant polarization. The drain current can still be measured when an external voltage is applied between the source and drain electrodes. When a negative voltage is applied to the gate, the ferroelectric polarization will decrease and then reverse polarization. Consequently, the conducting channel will narrow or disappear, and the drain current will decrease correspondingly. When the voltage is removed, a negative ferroelectric remnant polarization field will maintain the majority carrier accumulation state, and prevent the formation of drain current. A transfer characteristic is given in Fig 2.13 (b), and it can be seen that by introducing a ferroelectric material as the dielectric layer, the drain current can be significantly amplified or reduced compared with that of the traditional MOSFET, and thus the drain current can be used to read the stored "1" or "0" information [12].



Fig.2.13 (a) Schemetic diagram of a FeFET cell. (b) A typical transfer characteristic of FeFET [12].

Although there has been significant research on FeFETs, compared with the wide application of FeRAM there have not yet been any commercial FeFET products reported. The major problems that constrain further application of FeFETs are the retention time and fabrication integration issues. Unlike the FeRAM, where the ferroelectric capacitor is approximately 100 nm apart from the MOSFET, the ferroelectric material is in direct contact with the conducting channel of the MOSFET transistor [12]. The FeFET itself is a single device and the ferroelectric thin film acts as the functional and active part in the transistor. Therefore, the interface properties, such as localized states and impurities between the ferroelectric thin film and silicon wafer, will play an important role in determining the electrical performance of parameters including threshold voltage, saturation voltage, C-V curves, etc., of the FeFET. In fact, research indicates that there is considerable inter-diffusion between the ferroelectric material and silicon, especially during the annealing process [90,91]. Such inter-diffusion, along with some charge parasitic effects, will deteriorate the interface properties and reduce the retention time of the FeFET [12]. Several approaches have been proposed to increase the retention time of the FeFET; the most effective solution is to incorporate a high-K dielectric buffer layer between the ferroelectric thin film and the silicon substrate, as shown in Fig 2.14 [12].

Such a metal-ferroelectric-insulator-silicon (MFIS) structure will significantly reduce the diffusion around the interface and improve the retention time of the FeFET [92,93]. Many buffer layer materials, such as SiO₂, Si₃N₄, SrTiO₃, TiO₂, etc., have been investigated over the past decade [94-96], and HfO₂ in particular has proven to be a promising candidate with which the retention time of the SBT based FeFET can be improved to more than 30 days [92,97].



Fig.2.14 Schemetic diagram of the MFIS FeFET cell [12].

Besides research on the insulating layer, there exist other approaches for improving the current performance of the FeFET. For example, more complex gate sequences, namely, a metal-ferroelectric-metal-insulator-silicon (MFMIS) structure has been reported, where the optimized MFM structure from FeRAM can be employed during FeFET fabrication. Also, such a multilayer gate can provide more flexibility in optimizing and matching the infection charge issue between the ferroelectric thin film and the silicon substrate [12,92,98]. Meanwhile, inspired by the refresh unit in DRAM, a FeDRAM unit, namely, a FeFET unit with a refresh circuit is also reported as a compromise to the retention concern in the traditional FeFET. Unlike the high refresh frequency in DRAM, the

improve the retention time of the FeFET unit can even further reduce the refresh frequency [99,100]. Though research aimed at solving many application concerns of FeFET is on going, development of innovative designs and fabrication optimization will make possible the commercialization of FeFET in the near future.

2.4 Ferroelectric based optical applications

2.4.1 Ferroelectric optical MEMS

Micro-electromechanical systems (MEMS) have been extensively investigated for use in various applications, including as integrated accelerometers for auto-sensors, micromirrors for display and telecommunications, and micro-cantilevers for microscopes [12,101-105]. In its early stages, silicon based technology was well incorporated into the MEMS production process, which provided a remarkable contribution to the commercialization of MEMS technology. It is for this reason that the term MEMS has been associated with CMOS for such a long time. As an important application device, flat micro-mirrors driven by MEMS actuators are widely used in laser scanner displays, barcode readers, and laser printers [106,107]. Due to limited material selection, the actuators that are used to drive the micro-mirrors are all silicon based electrostatic actuators or electrothermal actuators [105,108]. With the development of modern MEMS technology, especially with the increase in flat micro-mirror area, use of the traditional electrostatic force or electrothermal force cannot meet the requirements of modern driving forces, due to their high operation voltage, non-linear operation and pull-in phenomenon. Electromagnetic actuators can provide a large driving force, but the large bulk volume cannot meet the micro design criteria [101]. Innovative actuators that can provide higher output force and higher scan speeds with lower driving voltages are in demand for optical MEMS applications.

Recently, PZT based ferroelectric actuators have attracted much research interest due to their higher output driving force and small driving voltage compared with traditional silicon based actuators. Such advantages can be attributed to their higher energy density compared with other actuators [102,109,110], making the PZT ferroelectric actuator a feasible alternative to existing silicon based actuators. In optical MEMS applications, a micromirror with a large mirror area, large deflection angle, and smaller driving voltage is of great demand for use in optical scanning display, 2D optical switch, and variable optical attenuators applications. The report of a PZT based piezoelectric actuator makes the micromirror design possible [102]. Up to now, there have been many optical MEMS applications reported based on the PZT ferroelectric actuator. A large elliptical silicon mirror with a size of 1 mm×2 mm driven by PZT actuators was reported by Y. Yasuda et al. [101], as shown in Fig.2.15. This scanner demonstrates large scan angles of 23 degrees (4.3 KHz for X-scan) by 52 degrees (90.3 Hz for Y-scan) at low driving voltages of typically 10 to 20V AC with a 5 V DC offset. A smaller 0.5 mm×0.5 mm torsional micromirror detached by PZT actuators was also reported by Kim et al. [111], as shown in Fig.2.16 for the 2D optical switch application. The single-axis torsional micromirror generates a static rotational angle of 6.1 degrees at 16 V DV, which is six times larger than that of the value for a traditional micromirror attached by PZT actuators. Recently, a rotational 3D silicon based micromirror driven by PZT actuators for variable optical attenuators has also been reported by C. K. Lee et al. [102], as shown in Fig.2.17. The PZT driven variable optical attenuator with a large silicon reflection mirror can be



integrated with a dual core fiber collimator in a 3D light attenuation arrangement.

Fig.2.15 SEM micrograph of the as-fabricated 2D piezoelectric scanner [101].



Fig.2.16 (a) Conventional design where a tilting micromirror is attached to the PZT actuators; (b) Innovative design where a torsional micromirror is detached from the PZT actuators [111].



Fig.2.17 (a) Schematic illustration of MEMS VOA. The PZT actuator can provide static displacements to rotate the mirror against the torsion spring. (b) Optical microscope photograph of the as-prepared MEMS VOA driven by two piezoelectric PZT actuators [102].

2.4.2 Ferroelectric based EO devices

Electro-optic (EO) devices such as the optical modulator, optical phase retarder, spatial light modulator, and optical switch are considered crucial components in integrated optics and modern optical communications due to their high level of flexibility in integrating with signal processing circuits [112]. As a traditional EO material, lithuium niobate (LiNbO₃) has been thoroughly investigated and applied in the past decades because of its high and stable EO coefficient, acoustic-optic, piezoelectric, and birefringence properties [113]. A number of commercial nonlinear optical components, such as modulators, couplers, Wavelength-division multiplexers (WDM) and Wavelength-division multiple

access (WDMA), are produced based on lithium niobate (LiNbO₃). However, recent studies indicate that many typical ferroelectric materials, especially single crystalline ferroelectrics, may serve as a promising replacement for traditional LiNbO₃ materials thanks to their ultra high EO coefficients. Compared with LiNbO₃, whose high frequency EO coefficient (r_{33}) is 30.8 pm/V, single crystalline lithium titanate (LiTaO₃) demonstrates a r_{33} of 35.8 pm/V, the r_{33} value is reported to be as high as 820 pm/V in single crystalline barium titanate (BaTiO₃), and single crystalline potassium niobate (KNbO₃) exhibits a linear EO coefficient of 450 pm/V. Moreover, a solid solution of KNbO₃ and KTaO₃ (KTa_xNb_{1-x}O₃) has been reported with an ultra high EO coefficient of ~2000 pm/V [114,115].

Among the various ferroelectric materials, BaTiO₃ and PLZT should be highlighted for use in optical applications. The BaTiO₃ material exhibits a high self pumped phase conjugation reflection and optical two wave mixing efficiency, and has been widely applied in the optical modulator field. As shown in Fig.2.18, an optical waveguide modulator is built using the BaTiO₃ material; the low V_{π} voltage at 1550 nm wavelength and the short electrodes (3 nm) make it a promising candidate for use in modulators [116]. Also, another study demonstrates a BaTiO₃ waveguide modulator with voltage-length products of 0.5 Vcm and an effective EO coefficient of 360 pm/V at 1561 nm, as shown in Fig. 2.19 [117].


Fig.2.18 Geometry of a c-axis type modulator and cross section view of a strip waveguide [116].



Fig.2.19 Schematic diagram of the BaTiO3 EO waveguide modulator, cross section view [117].

The PLZT material has nanosecond-scale fast switching responses, high optical transparency in the visible wavelength region, optical isotropy, and good thermal stability. Such superb optical properties have lead to its extensive application in photoelectron components or devices such as optical phased arrays [111,118] and electro-optic switches [119]. In large area optical applications where sizeable phase retardation is important, such as optical switches, the advantageous properties of PLZT outshine those of other materials. In order to achieve large enough phase retardation, the thickness of the EO material thin film should reach 100 μ m, and the EO coefficient must be high enough

[120]. However, there are many fabrication concerns with thick film deposition, such as film uniformity and inner stress release, which constrains the further research of such optical applications. The employment of PLZT can somewhat reconcile the thickness requirement and thus reduce the complexity of the device's fabrication and integration. Also, the high optical transparency of PLZT offers more economical benefits in the device design and implementation. Further, the dielectric and optical properties of PLZT can be modulated by changing the elemental constituents of the PLZT material [121]. Such changes in elemental constituents can create materials with different EO performance and can be attractive in modern optical applications where optical parameter matching is of importance. Fig.2.20 shows the design of a ridge type Mach-Zehnder modulator based on a PLZT waveguide [122].



Fig.2.20 (a) A schematic diagram of the PLZT waveguide (b) Geometry of a Mach-Zehnder modulator based on the PLZT waveguide [122].

2.5 Photovoltaic effect in ferroelectrics

In 2009, the photovoltaic effect was first reported in multiferroic BFO materials by T. Choi *et al.* [21]. Since most ferroelectric materials possess relatively large band gap energy, the small optical band gap of ~2.2 eV in bulk BFO makes its use possible in photovoltaic applications. By using an Au electrode, the BFO single crystal bulk exhibits a diode-like photocurrent under visible light illumination. The ferroelectric photovoltaic effect also varies with the direction of the polarized-light electric field, as shown in Fig.2.21. When the BFO bulk rotates under illumination with a linearly polarization light, the photovoltaic effect reaches maximum when the polarized-light electric field and inplane component of the ferroelectric polarization are parallel, and it becomes minimum when the field is perpendicular to the in-plane component.



Fig.2.21 The photovoltaic performance dependence on different polarization states of incident light [21].

Immediately following this, in a report in *Nature nanotechnology*, S. Y. Yang *et al.* investigated specifically patterned ferroelectric bulks with different domain types, and

reported an ultra high measured photo voltage of 16 V [22]. As explained by the authors, such a high photo voltage originates from the domain walls of the ferroelectric material. With carefully designed experiments, and the exclusion of spurious signals such as pyroelectric current, the photovoltaic effect was found to be associated with the 71° and/or 109° domain walls [22,24]. Another interesting point is that the electric field generated with the photovoltaic effect is an order of magnitude larger than that of the traditional silicon material; the increased field helps to separates the photo generated carrier pairs. In the BFO photovoltaic effect, the domain wall operates in a similar fashion to the typical p-n junction in traditional silicon based solar devices. Across the 71° and 109° domain walls in the BFO material, the non-zero divergence of the polarization will lead to an electrostatic potential drop. Such a potential offset will result in a band bending across the domain wall, which is quite similar to the band bending effect in the depletion layer of a p-n junction [22,24]. However, the ultra thin nature (~ 2 nm) of the domain wall compared with that of the p-n junction depletion width makes the built-in electrical field much higher than for traditional p-n junction based devices, and thus increases the charge separation efficiency during the photovoltaic process. Also, the photo voltage increases with the increase of domain wall numbers [22,24], and an aboveband gap voltage can be obtained with multi BFO crystal of different domain wall types in series. A schematic illustration of the domain wall in the BFO crystal is shown in Fig.2.22. At the same time, other groups have also published research reports on the BFO photovoltaic effect. W. Ji et al. fabricated epitaxial BFO thin film using scalable sputtering deposition technology and demonstrated that the photovoltaic response of the

single BFO crystal is switchable with the variation of ferroelectric polarization, with the

direction of the photocurrent opposite to that of the polarization vector [44]. H. T. Yi *et al.* reported that electro-migration, such as oxygen vacancies, caused by large external voltages can also work to switch the ferroelectric photovoltaic and rectification directions [123].



Fig.2.22 Schematic illustration of different domains (71° and 109°) in the BFO crystal [22].

Though most of the power conversion efficiencies are still modest in the present study compared with those of commercial silicon based solar devices due to the low bulk conductivity nature of the BFO material, other advantages of ferroelectric properties still make BFO based solar cells attractive for photovoltaic applications. The most exciting property is that ferroelectric materials exhibit a tunable photo voltage. When an external electric field larger than the coercive field is applied to the ferroelectric material, it can switch the ferroelectric domain in the BFO, flip the remanent polarization, and thus the output photo performance can be managed [22,124]. Additionally, due to the multiferroic nature of BFO, more control mechanics such as electricity, magnetism, heat, and stress, can be employed to determine the photovoltaic performance of the BFO material; and can therefore be used to produce solar cells with novel functionalities.

Chapter 3

Ferroelectric Properties and Optimization

3.1 Introduction

he fabrication process and ferroelectric characterization are a fundamental part of all research related to ferroelectric materials. The investigation of an optimized fabrication process for ferroelectric materials is crucial in our work and is the basis of the optical and photovoltaic research in the coming chapters. In this chapter, we investigate the fabrication process of the Bi_{4-x}Nd_xTi₃O₁₂ (BNdT) ferroelectric thin film, and obtain an optimized fabrication process routine for further applications. More specifically, Section 3.2 discusses the principle behind the sol-gel/spin coating process, describes the precursor preparation process for the BNdT ferroelectric solution, and illustrates the fabrication process of the BNdT ferroelectric thin film achieved in this work. Section 3.3 starts with the structural analysis, and shows the obvious impacts of the fabrication conditions on the BNdT XRD, SEM, AFM, TEM, etc. microstructure properties. Next, in Section 3.4, the ferroelectric and electric properties of the BNdT thin films are investigated, and an optimized fabrication condition is obtained based on these studies. In Section 3.5, the Nd doping concentration, as a different point of view, is evaluated in the BNdT thin film optimization process. Finally, this chapter is summarized and concluded in Section 3.6.

3.2 Fabrication and optimization

The fabrication technology of ferroelectric materials involves all of the traditional semiconductor fabrication technologies, such as solution-gelatin (sol-gel), chemical vapor deposition (CVD), radio-frequency sputtering (RF sputtering), metal organic chemical vapor deposition (MOCVD), pulsed laser deposition (PLD), and molecular beam epitaxy (MBE), etc. Physical fabrication approaches, such as PLD, RF sputtering, and MBE, can provide a better ferroelectric phase orientation and precise control over the elemental constituents that make up the compounds; thus enabling better ferroelectric properties in applications. However, the high cost and low growth rate constrain their application in large-scale fabrications. Chemical routines, on the other hand, including sol-gel, CVD, and MOVCD, demonstrate a large fabrication efficiency and low facility cost, and have been widely utilized in many commercial ferroelectric industries.

In this study, the sol-gel/spin coating method is chosen as the principle fabrication method for the BNdT ferroelectric material. The low operation temperature and high uniformity and consistency make it a promising method in optical related applications.

3.2.1 Sol-gel technology

Sol-gel technology: Theory

The sol-gel method is a typical wet chemical route, with the starting material (precursor) being prepared with either inorganic salt or metal alkoxide. The principle reaction routine

can be classified through three steps. First, the precursor dissolves in water or an organic solvent until becoming a uniform and stable solution. Second, the precursor hydrolyzes or alcoholize, and the product assembles in particles with 1 nm in diameter, thereby creating the solution. Finally, the solution evaporates and turns into gelatin. This process can be explained through the following equations [125].

(1) Solvation: $M(H_2O)_n^{z^+} - M(H_2O)_{n-1}(OH)^{(z-1)^+} + H^+$

The metal cation M^{z^+} in the salt ionizes and combines with a water molecule, resulting in the solvent unit $M(H_2O)^{z^+}$. Many H^+ have been released in this process to maintain the ligancy of the metal cation. If other cations exist, a complex polyreaction can occur at this time.

(2) Hydrolyzation: M(OR)_n+XH₂O----M(OH)_X(OR)_{n-X}+XROH

The unionized molecule precursor, such as metal alkoxide $M(OR)_n$, hydrolyzes and produces $M(OH)_n$.

(3) Condensation, which includes:

Dehydration condensation: M-OH+HO-M-M-O-M+H₂O

Loss of alcohol condensation: MOR+HO-M-M-O-M+ROH

The reaction products are colloidal particles with different structures and sizes.

Sol-gel technology: Fabrication process

The sol-gel fabrication process can be described in three steps, as illustrated in Fig.3.1



Fig 3.1 Fabrication flowchart of sol-gel technology.

First, dissolve the metal alkoxide in solvent. Since the solubility of the metal alkoxide in the water is limited, alcohol is always introduced to aide the dissolution process. Catalysts such as HCl and NH₄OH will also be added to this process to modulate the rate of hydrolysis and condensation. In order to ensure the uniformity and homogeneity of the precursor, stirring is both necessary and indispensable throughout this process. The second step is to prepare the solution. There are two major routines during the solution preparation process, namely, solution polymerization and the particle method. The core difference between these two methods is the amount of solvent added to the system. In the solution polymerization, little solvent is introduced, and hydrolysate can continue to react with the non-hydrolyzed metal alkoxide. However, the particle method ensures the reaction occurs under completed hydrolyzation of the metal alkoxide, and therefore adequate solvent should be provided. Since the hydrolyzation and condensation play an important role in the solation reaction, reaction parameters such as the solvent load, catalyst, and pH of the solution, should be well managed in this process. Third, age the solution into the wet gelatin. When the as-prepared solution is left to stand in an open or closed container, the existing particles in the solution will exhibit a "survival growth", namely, particles with larger size will expand while smaller particles will further shrink. This process is named Ostwald ripening [125], as illustrated in Fig.3.2. During the aging process, the solution particles connect into a network structure, and the fluidness of the entire system decreases, changing the solution system from a Newtonian fluid to Bingham plastic [125-127]. The forming processes such as fibrosis, spin coating, and casting can be implemented during this step. Fourth, dry the gelatin. There is a large amount of solvent or water in the wet gelatin, and the volume of the system shrinks significantly during the drying process, increasing the possibility of deformation and cracking. Therefore, the prevention of deforming and cracking is a key technology during the sol-gel/spin coating process, especially for large bulk substrates. Precise control over the drying conditions, addition of chemical additives, and supercritical drying, are some of the commonly used technologies in the current sol-gel fabrication field. Finally, anneal the as-prepared dry gelatin. The purpose of this step is to minimize the remaining air and solvent in the gelatin, increase the gelatin density, and help to achieve the desired crystalline phase. Due to the high specific surface area and high activity of the gelatin, the annealing temperature is much lower compared with that of ceramic sintering. Hot pressed sintering is always introduced as a popular technology to reduce the sintering time and increasing sintering quality [127,128].



Fig 3.2 Schematic illustration of Ostwald ripening.

3.2.2 Precursor preparation

In this study, the molecular formula of the BNdT sample is $Bi_{4-x}Nd_xTi_3O_{12}$ (x=0.85), namely, $Bi_{3.15}Nd_{0.85}Ti_3O_{12}$. To obtain the desired element ratio in the BNdT thin film, the appropriate metal salt solute and corresponding solvent should be employed to provide a stable and uniform solution.

According to the literature, there are two major routines for preparing the BNdT precursor, as follows:

(a) As reported in the literature [34], three organic metal alkoxides can be introduced to provide the Nd, Bi, and Ti element, as follows:

Neodymium(III) acetate hydrate, namely, Nd(CH₃COO)₃; Bismuth 2-Ethylhexanoate, namely, Bi(C₅H₁₁COO)₃; and Titanium(IV) isopropoxide, namely, Ti(OCH₂CH₂OCH₃)₃.

(b) Reported by J. H. Li *et al.* [129], three metal inorganic salts can be introduced to provide the Nd, Bi, and Ti element, as follows:

Bismuth(III) nitrate pentahydrate, namely, $Bi(NO_3)_3 \cdot 5H_2O$; Neodymium(III) acetate hydrate, namely, $Nd(CH_3COO)_3 \cdot H_2O$; and Tetrabutyl titanate, namely, $Ti(C_4H_9O)_4$.

During the fabrication process, inorganic nitrate is more toxic than organic acetate, and volatized nitric acid during the dry and annealing process is more harmful than is the acetic acid. Moreover, nitrate is explosive and has strong oxidation potential, and thus entails more security concerns during storage and operation processes. Therefore, we decide to choose the first routine in our precursor preparation process.

Precursor list

All of the chemicals are provided by Sigma-Aldrich, Gelest Inc., and Fisher Scientific.

Name	Formula	Atomic Weight	Assay	CAS
		(at. wt)		
Neodymium(III)	Nd(CH ₃ COO) ₃	321.37	99.9%	334869-71-5
acetate hydrate				
Bismuth 2-Ethylhexanoate	Bi(C5H11COO)3	638.61	75%	67874-71-9
Titanium(IV) isopropoxide	Ti(OCH ₂ CH ₂ OCH ₃) ₃	284.26	97%	546689
Ethanolamine	NH ₂ CH ₂ CH ₂ OH	61.08	99.5%	141-43-5
2-Ethylhexanoic acid	$C_5H_{11}COOH_3$	144.21	99%	149-57-5
1-Propanol	CH ₃ CH ₂ CH ₂ OH	60.10	99.7%	71-23-8

Table.3.1 Chemicals used to prepare the BNdT precursor.

The atomic weights (at. wt) of all the elements in the calculation are listed as follows:

H: 1.00079	C: 12.011	O: 15.9994	
Bi: 208.98	Nd: 144.24	Ti: 47.9	

Precursor preparation recipe

According to the literature, we choose Ethanolamine, 2-Ethylhexanoic acid, and 1-Propanol as the solvents of Neodymium(III) acetate hydrate, Bismuth 2-Ethylhexanoate, and Titanium(IV) isopropoxide, respectively. In order to maintain the mol ratio of Bi, Nd, and Ti at 3.15:0.85:3, the mass of the metal salts are calculated as follows,

$$M[Nd(CH_{3}COO)_{3}] = \frac{0.025 \times 0.2 \times 321.37 \times 0.85}{99.9\%} = 1.367 \text{ g}$$
$$M[Bi(CH_{3}COO)_{3}] = \frac{0.025 \times 0.2 \times 638.61 \times 3.15 \times (1+10\%)}{75\%} = 14.752 \text{ g}$$
$$M[Ti(OCH_{2}CH_{2}OCH_{3})_{3}] = \frac{0.025 \times 0.2 \times 284.26 \times 3}{97\%} = 4.396 \text{ g}$$

As shown in Fig 3.3, a detailed precursor preparation process can be described as follows,

(1) 1.367 g Nd(CH₃COO)₃ is dissolved in NH₂CH₂CH₂OH until 10 ml.

(2) 14.752 g Bi(CH₃COO)₃ is dissolved in $C_5H_{11}COOH_3$ until 25 ml. Excess bismuth nitrate of 10% is added to compensate the Bi loss during the thermal annealing process.

(3) 4.396 g Ti(OCH₂CH₂OCH₃)₃ is dissolved in CH₃CH₂CH₂OH until 25 ml.

(4) Pour the Nd(CH₃COO)₃ solution into the Bi(CH₃COO)₃ solution, and clean the wall of the beaker using CH₃CH₂CH₂OH. Stir the mixed solution for 1 hr.

(5) Pour the $Ti(OCH_2CH_2OCH_3)_3$ solution into the as-prepared mixed solution, and clean the wall of the beaker using $CH_3CH_2CH_2OH$. Stir the mixed solution for 48 hrs.

(6) Add appropriate amount of CH₃CH₂CH₂OH until 50 ml. Stir the mixed solution for 1 hr.

(7) Filter the as-prepared solution using a 0.2 μ m filter and store the solution in a conical beaker.

A photographic image of the as-prepared BNdT solution is shown in Fig 3.4; it can be seen that a clear, uniform, and stable solution is achieved in our experiment.



Fig 3.3 Precursor preparation recipe.



Fig.3.4 A photographic image of the as-prepared BNdT solution.

3.2.3 Thin film fabrication

The fabrication process of the BNdT ferroelectric thin film can be concluded as follows.

(1) Substrate cleaning. A P-type (100) silicon wafer is ultrasonically cleaned using hydrofluoric acid (HF), acetone, isopropanol, and deionized water, in that order, prior to deposition. The hydrofluoric acid is introduced to remove the natural oxide layer on the

silicon wafer, and the acetone and isopropanol are used to remove the organic impurities attached to the wafer surface. One thing to note is the order of the chemical cleaning: since there might be some hydrogen dangling bonds introduced during the HF cleaning process, the acetone, isopropanol, and deionized water cleaning must be done after the HF cleaning so as to minimize the hydrogen dangling bonds generated in the previous step.

(2) Thermal oxidization. 300 nm silicon dioxide (SiO₂) is deposited on top of the silicon wafer by a wet oxidation process at 1100° C.

(3) Bottom electrode sputtering. A bottom electrode consisting of a platinum (Pt) layer of 200 nm and a titanium (Ti) layer of 30 nm is then deposited using a DC-sputtering process. Since the Pt layer and SiO₂ possess an intrinsic poor adhesiveness, the Ti layer is applied to increase the adhesiveness between the Pt layer and SiO₂ substrate, and thus preventing the upper layer from being peeled-off in subsequent fabrication steps.

(4) Recovery annealing. The as-prepared platinum substrate is introduced to a rapid thermal annealing (RTA) process (heating rate: 120 °C/s) at 650°C for 1 minute in an oxygen atmosphere to remove the residual stress during the sputtering process.

(5) Spin coating deposition. The BNdT thin film is then deposited on top of the Pt(200 nm)/Ti(30 nm)/SiO₂(300 nm)/Si(100) substrate, with a spin rate of 3000 rpm lasting for 30 s. This process is repeated until the desired thickness (300 nm) of the BNdT thin film is obtained.

(6) Pyrogenation. The as-prepared BNdT thin film is left to a pyrogenation process at 380°C for 30 s in the air atmosphere, in order to help the organic solvent volatilize and the ferroelectric crystallize.

(7) Pre-crystallization annealing. The BNdT thin film is introduced to a RTA process in an oxygen atmosphere. The temperature quickly rises from room temperature to 200°C where it is kept for 20 s, and then increases up to 650°C in 3.9 s (heating rate:110°C/s) and is held for a further 60 s.

(8) Crystallization annealing. After processes (5) to (7) have been repeated an appropriate amount of times, a crystallization annealing process is applied to the asprepared BNdT thin films. Different annealing temperatures of 300°C, 400°C, 500°C, and 650°C, for 45 min in an oxygen atmosphere, are investigated to seek an optimized fabrication recipe for the BNdT thin film.

(9) Top electrode sputtering. Top Pt electrodes are introduced by means of DC magnetron sputtering with a shadow mask. The diameter of the top electrode is typically 200 μm.

The as-prepared BNdT thin film demonstrates a neat and clear surface, which can be evaluated by the Keyence photographic image (as shown in Fig 3.5) and scanning electron microscope (SEM) image (as shown in Fig 3.6). More advanced structure and performance characterization methodologies will be examined in the coming sections.



Fig 3.5 Keyence photographic image of the upper electrode in the as-prepared BNdT thin film.



Fig 3.6 SEM image of the upper electrode in the as-prepared BNdT thin film.

3.3 Structure characterization

The structural properties play an important role in determining the electrical, optical, and ferroelectric behaviour of the BNdT ferroelectric material. Different fabrication methods will lead to significant structural variation in the ferroelectric crystal and thus different properties. In this section, structural characterization technologies including X-ray diffraction (XRD), scanning electron microscopy (SEM), atomic force microscopy (AFM), and transmission electron microscopy (TEM), will be introduced to investigate the microstructure of the BNdT thin film and how the fabrication process affects the various structure-related parameters.

3.3.1 X-ray diffraction

Measurement principle

When a crystal is exposed to X-rays, the electron inside the crystal is forced to vibrate, leading to coherent scattering. All of the scattered waves generated by different electrons of the same atom interfere and create the atomic scattering wave. Due to the periodic

manner of the atoms inside the crystal, all atomic scattering waves exhibit a set phase difference, and thus interfere with each other. In some specific directions, constructive interference occurs, resulting in a diffracted wave. Therefore, the diffracted wave of the crystal comes from the superposition of the atomic scattering waves.

XRD is based on the measurement of the diffracted wave of the crystal, as stimulated by external X-ray radiation. The diffraction direction and diffraction intensity are two important parameters in such an analysis. The XRD analysis method is non-destructive, and the diffraction patterns can offer following information regarding the as-measured crystal:

- (1) Qualitative phase analysis,
- (2) Quantitative phase analysis,
- (3) Degree of crystallinity analysis,
- (4) Residual stress analysis,
- (5) Grain size and distribution analysis,
- (6) Orientation and structural analysis.

Measurement parameter configuration

Instrument: X-Ray Diffractometer (Philips PW1710, Holland) with Cu Ka radiation

Parameter configuration: At Normal Pressure and Temperature (NPT), due to the existence of silicon substrate in the BNdT sample, the strong single crystal diffraction will damage the diffractometer. Therefore, the scan angle (2θ) is set from 5° to 65° so as to skip over the silicon diffraction peak in our experiment.

Results and analysis

Fig 3.7 shows the XRD patterns of BNdT thin films deposited on the Pt(200 nm)/Ti(30 nm)/SiO₂(300 nm)/Si(100) substrate at post annealing temperatures of 400°C, 500°C, and 650°C. Most of the diffraction peaks can be indexed according to the standard powder diffraction data of $Bi_4Ti_3O_{12}$ and $Bi_{3.6}Nd_{0.4}Ti_3O_{12}$ [35,130]. In the BNdT thin film annealed at 400°C, a nanocrystalline structure without any obvious orientation can be found. With increasing annealing temperature, the BNdT thin film becomes crystallized, exhibiting similar diffraction peaks as BLT thin films without any pyrochlore phase. Although Nd ions occupy Bi sites in the BNdT crystal, the Nd substitution does not seem to affect the layered perovskite structure. The BNdT thin film annealed at 500°C shows a bismuth layer perovskite structure with weak diffraction peaks and a comparatively strong random orientation. As the annealing temperature increases, sharper peaks with high intensity can be observed in the pattern, implying that a bismuth layer perovskite structure.



Fig.3.7 XRD patterns of BNdT thin films annealed at different post annealing temperatures.

C-axis oriented peaks such as (004), (006), (008), and (0014), can be found in the BNdT thin film processed at 650°C. In order to estimate the degree of preferred orientation, the volume fraction $\alpha_{(00l)}$ of *c*-axis-oriented grains in the BNdT thin film can be defined as: [131,132]

$$\alpha_{(00l)} = \sum_{i} I^{i}(00l) / \sum_{i} I^{i}(hkl)$$
(3.1)

where I(hkl) is the measured intensity of the (*hkl*) peaks for the thin film. The $\alpha_{(00l)}$ values obtained at the three different temperature are: 15.8%, 21.4%, and 44.7%, respectively, indicating a remarkable increase of *c*-axis-oriented grains in the thin films with increasing annealing temperature. The BNdT thin film annealed at 650°C possesses an $\alpha_{(00l)}$ of 44.7%, indicating a preferred c-axis orientation. As reported by Chon *et al.* [34] such highly orientated BNdT thin films will exhibit good ferroelectric properties.

Assuming that the BNdT thin film has an orthorhombic structure, the lattice parameters of the BNdT thin film can be calculated to be a=5.413 Å, b=5.285 Å, c=32.916 Å, compared with the lattice parameters of the Bi_{3.6}Nd_{0.4}Ti₃O₁₂ (a=5.429 Å, b=5.406 Å, c=32.832 Å), indicating that the substituted Nd ions do not affect the perovskite structure of the crystal.

3.3.2 Scanning electron microscope

Measurement principle

In the SEM characterization, an ultra-narrow electron beam scans a test sample. Many secondary electrons are stimulated around the surface of the sample, and the amount of secondary electrons is determined by the incidence angle of the electron beam. In other words, the amount of the secondary electrons is determined by the surface structure of the

sample. Secondary electrons will be collected by a specific detector and changed into an optical signal by a photoelectric converter. Then, the optical signal will be amplified and converted back to an electrical signal to control the intensity of the electron beam on the fluorescent screen, resulting in a scanning pattern image that is synchronous with the electron beam. In order to increase the emission efficiency of the secondary electron, and thus increase the imaging quality, a heavy metal atom such as Au or Cr will be coated on top of the sample's surface before the SEM measurement.

Measurement parameter configuration

Instrument: Field-emission scanning electron microscopy (Hitachi S-4700, Japan)

Parameter configuration: The SEM measurement is classified in two segments, namely, cross section analysis and top-view analysis. The cross section analysis is used to examine the longitudinal performance of the multilayer, such as consistence and compactness. On the other hand, the top-view analysis reveals the surface properties of the sample including smoothness, flatness, and uniformity.

After cutting the sample into an appropriate size (1cm*1cm), a thin layer of amorphous Cr is coated using a DC-sputtering process. The thickness of the Cr layer is estimated to be 0.05 nm/s*300s = 15 nm.

Results and analysis

Fig. 3.8 shows the cross section SEM micrograph of the BNdT thin film annealed at 650°C, exhibiting a clear and sharp boundary between different layers. We conclude that a dense and smooth film is achieved and the film thickness is estimated to be 300 nm in this measurement. The surface morphology of the same sample can be seen from Fig.3.9, indicating that the perovskite layer was oriented randomly and that the surface is uniform

without any cracks. The mean grain size can be estimated to be ~ 200 nm in this experiment.



Fig.3.8 Cross section SEM micrograph of BNdT thin film annealed at 650°C.



Fig.3.9 SEM top-view of the BNdT thin film processed at 650°C.

3.3.3 Atomic force microscopy

Measurement principle

AFM examines the ultra-weak inter-atomic forces between the surface of the asmeasured sample and a micro piezosensor, thereby allowing investigation of the surface structure and properties. In general, during the AFM measurement, a microprobe is placed on one end of an elastic micro-cantilever beam, while the other end of the microcantilever beam is fixed. When the probe scans over the surface of the sample, the atomic repulsion between the probe and the surface of the sample will cause a tiny distortion in the micro-cantilever beam. Such distortion in the micro-cantilever beam can be regarded as an indirect measure of the atomic repulsion between the probe and the surface of the sample. A laser beam reflected off the back of the micro-cantilever beam is guided into a photodetector. It can precisely measure the tiny distortion of the micro-cantilever beam and thus the surface topography of the sample can be indirectly reflected by the repulsion between the probe and the surface of the sample.

Measurement parameter configuration

Instrument: Atomic force microscopy (Dimension/Veeco 3100, USA).

Parameter configuration: At NPT, the sample is prepared into an appropriate size (2cm*2cm), and the measurement range is ~2.5 nm*2.5 nm.

Results and analysis

Fig.3.10 (a)-(d) shows the AFM surface morphologies of BNdT thin films annealed at different temperatures. A smooth and uniform surface is observed and the BNdT thin film is seen to be composed of close-packed spherical grains. The grain size measured increases remarkably with increasing post annealing temperatures, from 79 nm at 300°C to 202 nm at 650°C, in agreement with the sol-gel derived BNdT thin film reported by J. H. Li *et al.* [129]. The surface roughness (R_a) of the 250 nm BNdT thin film also increases with increasing post annealing temperature as follows: R_a is 1.77 nm, 2.36 nm, 2.79 nm, and 3.90 nm, for the samples annealed at 300°C, 400°C, 500°C, and 650°C,

respectively. The surface roughness variations and the grain size changes are consistent with the results reported by G. Jang *et al.*, [133] C. P. Luo *et al.*, [134] X. Z. Ding *et al.*, [135] and can be corroborated by the increase of peak sharpness in XRD patterns shown in Fig.3.7.





Fig.3.10 AFM images of BNdT thin film surface topography annealed at different temperatures, (a) 300°C, (b) 400°C, (c) 500°C, and (d) 650°C.

3.3.4 Transmission electron microscopy

Measurement principle

Transmission electron microscopy (TEM) has an ultra large magnification ($\sim 10^6$) and thus is widely used in the fields of microstructure characterization, cytobiology, and virology. There are major functional modules in the TEM, namely, an electron beam gun that can generate an ultra narrow electron beam, and an electromagnetic lens that can control the trace of the electron beam in tasks such as focusing and enlarging. The highenergy electrons generated by the electron beam gun are focused on the surface of the asmeasured sample using a magnetic field. Scattering will be observed when the highenergy electrons pass through the sample body. Since different parts of the sample possess different structural properties such as variations in density, deficiency and crystallographic orientation, the intensity of the electron scattering also varies correspondingly. The transmitted electrons will be focused on the fluorescent screen, resulting in an image with different contrasts. The differing contrasts in the image reflects the intensity of the electron scattering and therefore the structure variation of the sample, and can be used to investigate the microstructure of the sample.

Measurement parameter configuration

Instrument: Transmission electron microscopy (HRTEM, FEI Tecnai F20, USA).

Parameter configuration: Since the electron beam should be able to pass through the sample in the experiment, the sample should be milled to less than 100 nm in thickness.

Results and analysis

To evaluate the nano-scale structure, TEM was employed to examine the BNdT thin film annealed at 650°C. Fig.3.11 (a) shows a bright field cross-section TEM micrograph of the thin film indicating a spherical growth. The average sphere size is estimated to be 200 nm, which corresponds to the in-plate grain size and is consistent with the result shown by AFM measurement. Since the interface properties play a critical role in target applications, high resolution TEM (HRTEM) was employed, as shown in Fig.3.11 (b). It can be seen that an amorphous layer with a 3 nm thickness is formed at the interface; a similar result to that reported by J. H. Li *et al.* [129]. This interfacial layer might be silicate caused by the interaction between Si and Bi atoms. When Pt is employed as the bottom electrode, a similar interaction and diffusion can also be seen between Bi and Pt. As reported in the literature, Bi atoms can diffuse into the ferroelectric/Pt interface during the annealing process, forming Bi-Pt alloy around the interface. The alloy formation will influence the electronic properties of the ferroelectric capacitor and impact the mechanical stability of the electrode [132, 136-139].



Fig.3.11 (a) TEM micrograph of the BNdT thin film deposited on Si substrate. (b) High resolution TEM image of the BNdT thin film deposited on Si substrate.

3.4 Ferroelectric properties characterization

3.4.1 Remnant polarization

Research into ferroelectric properties is the principle part of the BNdT ferroelectric thin film investigation, and the remnant polarization plays an important role in such properties. As a crucial parameter of ferroelectrics, almost all ferroelectric properties can be reflected in the ferroelectric hysteresis loop. Important ferroelectric parameters such as the remnant polarization and coercive field can both be extracted from examination of the hysteresis loop.

According to the literature, the most significant advantage of the BNdT thin film is the remarkable remnant polarization value compared with traditional ferroelectrics such as PZT and SBT. Fabrication methods can impact the ferroelectric remnant polarization significantly. As reported by T. Kojima *et al.* [140], BNdT deposited by the MOCVD method possesses a remnant polarization of ~25 μ C/cm², while MOD derived BNdT can

exhibit a remnant polarization of >56 μ C/cm². Meanwhile, the annealing temperature also plays a key role in determining the remnant polarization of the BNdT thin film. In this section, the variation of BNdT remnant polarization for different annealing temperatures is demonstrated and investigated.

Fig.3.12 shows the polarization-voltage (*PV*) hysteresis loops of the BNdT thin film capacitors with different annealing temperatures in an oxygen atmosphere. It can be concluded that the remnant polarization (2*P*_r) increases with increasing annealing temperature from 400°C to 650°C. In the BNdT sample processed at 650°C, a well established hysteresis loop is obtained exhibiting a remnant polarization (2*P*_r) of 39.6 μ C/cm² and a coercive field of 85 kV/cm with an applied voltage of 5 V, which is much larger than for with BNdT prepared by RF magnetron sputtering (~13.2 μ C/cm²) [133] and chemical solution deposition (~21 μ C/cm²) [141]. This result indicates that 650°C is an optimized annealing temperature, and it can help the crystallization process of the BNdT ferroelectric thin film. All of the forthcoming research will be conducted based on the 650°C processed samples.



Fig. 3.12 Ferroelectric hysteresis loops of BNdT thin films annealed at different temperatures.

Since the minimum non-volatile polarization is 3 μ C/cm² for basic memory design [72,142], the BNdT thin films achieved in this study are well suited for such an application. As well, the saturation voltage is only 5 V; a value much smaller than the result reported in [34] and such saturation voltage can be demanding in low power consumption FeRAM applications. The difference in remnant polarization and saturation voltage in our study compared to literature reports can be attributed to many factors. First, BNdT thin films achieved by different fabrication methods exhibit different crystalline qualities and thus different properties. It is believed that the ferroelectric properties are always better following some chemical routes compared with PLD and sputtering processes. Indeed, a degree of preferred grain orientation and a better ferroelectric performance are always reported in some chemical routes [141,143-148]. Secondly, even by the same sol-gel method, different starting materials and solvents will possess different hydrolysis processes of the metal ions, and thus impact the properties of the solution achieved. As well, different preparation details, such as the RTP heating rate, will impact the crystallization of BNdT and therefore the ferroelectric properties in the measurement. Another important factor in determining the remnant polarization and saturation voltage is the volume fraction $\alpha_{(00)}$ of *c*-axis-oriented grains in the BNdT thin film, as studied in section 3.3.1. As reported by Chon *et al.* [34], the polarization of lanthanide-substituted Bi₄Ti₃O₁₂ was along the c-axis and the remnant polarization of the BNdT film would be larger if a bigger volume fraction $\alpha_{(00)}$ of c-axis-oriented grains are achieved in the thin film. Since the c-axis orientation in the thin film deposited is somewhat smaller than that of the BNdT thin film prepared by Chon et al. [34], it would be reasonable to expect a difference in the remnant polarization value as well.

Since the operation frequency is an important performance parameter in many electrical and optical applications, the frequency dependence of the polarization-voltage (PV) hysteresis loops is also investigated, as shown in Fig. 3.13. It can be seen that the remnant polarization values and the saturation of loops decrease significantly with an increase in operation frequency. This can be explained by the nature of ferroelectricity. In ferroelectrics, the remnant polarization field is created by an external electric field. However, the variation of remnant polarization field does not occur simultaneously with that of the external electric field. Such hysteretic behaviour can be observed through the existence of remnant polarization when the external electric field is removed. Since there is a hysteretic behaviour between the remnant polarization field and the external electric field, the variation of external electric field cannot be too rapid. Otherwise, the remnant polarization field will not be able to catch up with the external electric field, and there will be degradation in the ferroelectric properties due to the ferroelectric relaxation phenomenon. In Fig. 3.13, it can be seen that in the 100 Hz frequency region, the external electric field varies within the ferroelectric relaxation, and the polarization dipoles in the BNdT crystal have sufficient response time to be set along the polaxis and thus exhibit a high remnant polarization value. Increasing the measurement frequency to 1 KHz, the kinetics of polarization reversal of the BNdT thin film becomes unable to follow the increase in measurement frequency, and ferroelectric degradation is then observed. Actually, most ferroelectric materials reveal well-defined performance in such a high frequency application. As introduced earlier in this section, a polarization of 3 μ C/cm² is adequate for non-volatile applications. Since the remnant polarization is higher than necessary but the operational frequency is relatively low, a trade-off such as increasing



the frequency with a reasonable sacrifice in remnant polarization, can make this material feasible for modern usage.

Fig. 3.13 Ferroelectric hysteresis loops of the BNdT thin films measured at different frequencies from 100 Hz to 2 KHz.

3.4.2 Fatigue properties

The BNdT ferroelectric exhibits a superb fatigue endurance compared with traditional ferroelectric PZT [149]. Reported by Chon *et al.* [34], with an applied voltage of 5 V, BNdT exhibits <2% degradation in remnant polarization and <1.5% degradation in coercive field after 6.5×10^{10} switching cycles. In this section, we will investigate the fatigue performance of the BNdT ferroelectric, and the fatigue variation with different test frequencies and test amplitudes.

Fig. 3.14 (a) and (b) shows the BNdT polarization as a function of the polarization switching cycles at 2.5 V/10 MHz and 2.5 V/1 MHz. It can be seen that in the 2.5 V/10 MHz test case, the BNdT thin film exhibits good fatigue properties, and little fatigue degradation in remnant polarization (<1.5%) and coercive field (<1.6%) is demonstrated

under 1×10^{10} switching cycles; indicating that a good fatigue endurance for the BNdT thin film is achieved in this experiment. However, in the 2.5 V/1 MHz test case, >29.4% degradation in remnant polarization and 12.7% degradation in coercive field are observed.



Fig. 3.14 Fatigue curves of polarization as a function of switching cycles at (a) 2.5 V/1 MHz and (b) 2.5 V/10 MHz.

Such a frequency dependence of the ferroelectric fatigue can be explained by the ferroelectric domains reorientation effect. Due to the nature of remnant polarization, the ferroelectric domains re-orient to a preferred direction when an external electrical field is applied. This results in the redistribution of crystalline lattice stress, which can be characterized by an atomic force analysis. As reported by N. X. Zhang *et al.* [150], the

external electric field plays an important role in the ferroelectric domains re-orientation process, and only external electric fields meeting certain criteria can cause the re-orientation. The minimum electric field E_{\min} required for ferroelectric domain re-orientation, and the switching time τ_s , should satisfy the following relationship [151],

$$E \ge E_{\min} = \zeta(\tau_s)^{\alpha}, \tag{3.2}$$

where ζ and α are two set empirical constants derived in the experiment.

It can be seen that given a fixed external electrical field E_{γ} and a switching time τ_{γ} , the switching frequency $1/\tau_{\gamma}$ can be calculated; and any external electric field with frequency higher than $1/\tau_{\gamma}$ cannot cause ferroelectric domain re-orientation. Therefore, application in this frequency range will cause little fatigue degradation. Hence, from an application point of view, the higher operational frequency a material can reach, the more application prospects it will have. As discussed in section 3.3.1, we can sacrifice some remnant polarization of the BNdT ferroelectric in order to increase the operational frequency. This compromise not only expands the potential application fields, but also skips the "fatigue frequency interval" and as such is a method that achieves both goals simultaneously.

The amplitude dependence of the BNdT fatigue variation is shown in Fig. 3.15 (a) and (b). It can be seen that under polarization switching cycles at 2 V/10 MHz and 3 V/1 MHz, BNdT demonstrated a similar fatigue performance (<1.5%). This can also be explained by Eq.3.2. Since there is no amplitude term in the equation, the amplitude of the external electric field does not affect determination of the fatigue degradation of the BNdT thin film.



Fig. 3.15 Fatigue curves of polarization as a function of switching cycles at (a) 3 V/10 MHz and (b) 2 V/10 MHz.

3.4.3 Leakage properties

The large remnant polarization in the BNdT thin film can be attributed to the good interaction properties of the BNdT ferroelectric thin film and the Pt substrate. As studied in section 3.3.4, the amorphous inter-diffusion is only 3 nm in thickness between the BNdT ferroelectric thin film and the Pt substrate, indicating a well-defined interface property.

Leakage properties can also allow examination of the interface behaviour of the BNdT/Pt capacitor. The leakage current density of the BNdT thin film is measured to be 5×10^{-7} A/cm² at an applied voltage of 5 V, as shown in Fig. 3.16, indicating a fairly low leakage density.



Fig.3.16. IV curves of BNdT thin film annealed at 650°C.

Such a leakage density value is desirable in FeRAM and FeFET related applications. A low leakage density indicates a slow discharge process and thus a strong charge retention endurance. In the FeFET application, charge retention endurance plays a significant role in determining the reliability and lifetime of the memory device. In fact, there has been significant research reported towards further increasing the leakage properties of the ferroelectric capacitor and thus improving the reliability and lifetime of the applications. Buffer layer technology, for example, has been regarded as an effective method for increasing the retention properties. By inserting an ultra thin dielectric buffer layer such as HfO₂, ZnO, or SrTiO₃, between the ferroelectric thin film and the substrate, the high-K essence of these buffer layers will further prevent inter-diffusion between the ferroelectric layer and the substrate, and increase the leakage endurance of the
ferroelectric structure. Moreover, some buffer layers with ABO₃ structures possess a similar lattice constant with ferroelectric crystal, and will help the crystallization process of the upper ferroelectric thin film.

3.5 Doping methodologies and optimization

In the previous section, we discussed the variation of ferroelectric structural and electrical properties for different annealing temperatures. Actually, since the BNdT ferroelectric is Nd doped bismuth titanate in nature; different Nd doping concentrations can also modulate the structural and ferroelectric properties in the application. Since the major application concern of the BNdT thin film is the ferroelectric remnant polarization and $Bi_{3.15}Nd_{0.85}Ti_3O_{12}$ is proven to possess the largest $2P_r$ value, $Bi_{4-x}Nd_xTi_3O_{12}$ (x=0.85) is always utilized in memory based ferroelectric research. However, different Nd doping concentrations and their impact on structural properties have not been widely reported in the literature. In this section, we fabricate $Bi_{4-x}Nd_xTi_3O_{12}$ (x=0, 0.25, 0.5, and 0.85) materials with different Nd contents, and report the dependence of the $Bi_{4-x}Nd_xTi_3O_{12}$ structural properties on the Nd content. Our work indicates that Nd substitution can be utilized to tune and modify the structural parameters of $Bi_{4-x}Nd_xTi_3O_{12}$ in ferroelectric-based applications.

3.5.1 Bi_{4-x}Nd_xTi₃O₁₂ ferroelectric thin film fabrication

Precursor preparation recipe

In a procedure comparable to that described in section 3.2.1, we choose a similar recipe to fabricate the $Bi_{4-x}Nd_xTi_3O_{12}$ (x=0, 0.25, 0.5, and 0.85) precursors.

In order to maintain the desired mol ratio of Bi, Nd, and Ti, the corresponding mass of all the metal salts are calculated as follows,

(1) x=0, $Bi_4Ti_3O_{12}$ $M[Nd(CH_{3}COO)_{3}] = \frac{0.025 \times 0.2 \times 321.37 \times 0}{99.9\%} = 0 g$ M[Bi(CH₃COO)₃]= $\frac{0.025 \times 0.2 \times 638.61 \times 4 \times (1+10\%)}{75\%}$ = 18.733 g M[Ti(OCH₂CH₂OCH₃)₃] = $\frac{0.025 \times 0.2 \times 284.26 \times 3}{97\%}$ = 4.395g (2) x=0.25, Bi_{3.75}Nd_{0.25}Ti₃O₁₂ $M[Nd(CH_{3}COO)_{3}] = \frac{0.025 \times 0.2 \times 321.37 \times 0.25}{99.9\%} = 0.402 \text{ g}$ $M[Bi(CH_3COO)_3] = \frac{0.025 \times 0.2 \times 638.61 \times 3.75 \times (1+10\%)}{75\%} = 17.562 \text{ g}$ M[Ti(OCH₂CH₂OCH₃)₃] = $\frac{0.025 \times 0.2 \times 284.26 \times 3}{97\%}$ = 4.395g (3) x=0.5 Bi_{3.5}Nd_{0.5}Ti₃O₁₂ M[Nd(CH₃COO)₃] = $\frac{0.025 \times 0.2 \times 321.37 \times 0.5}{99.9\%} = 0.804 \text{ g}$ M[Bi(CH₃COO)₃] = $\frac{0.025 \times 0.2 \times 638.61 \times 3.5 \times (1+10\%)}{75\%} = 16.391 \text{ g}$ M[Ti(OCH₂CH₂OCH₃)₃] = $\frac{0.025 \times 0.2 \times 284.26 \times 3}{97\%}$ = 4.395g (4) x=0.85 Bi_{3.15}Nd_{0.85}Ti₃O₁₂ $M[Nd(CH_{3}COO)_{3}] = \frac{0.025 \times 0.2 \times 321.37 \times 0.85}{99.9\%} = 1.367 \text{ g}$

$$M[Bi(CH_{3}COO)_{3}] = \frac{0.025 \times 0.2 \times 638.61 \times 3.15 \times (1+10\%)}{75\%} = 14.752 \text{ g}$$
$$M[Ti(OCH_{2}CH_{2}OCH_{3})_{3}] = \frac{0.025 \times 0.2 \times 284.26 \times 3}{97\%} = 4.396 \text{ g}$$

Excess bismuth nitrate of 10% is added in all of the precursors to compensate the Bi loss during the thermal annealing process.

Fabrication process

Similar to the procedure described in section 3.2.3, Pt(200 nm)/Ti(30 nm)/SiO₂(300 nm)/Si(100) was introduced as the substrate and ultrasonically cleaned in acetone, isopropanol, and deionized water prior to deposition. The spin rate was 3000 rpm, lasting for half a minute for each step. The as-deposited BNdT films were introduced to a rapid thermal annealing (RTA) process (heating rate: 120°C/s) at 650°C for 1 minute in oxygen atmosphere. To obtain the desired thickness, the spin coating process was repeated several times. The as-deposited BNdT films were then introduced to a rapid thermal annealing (RTA) process at 600°C for 10 minutes in the air.

3.5.2 Bi_{4-x}Nd_xTi₃O₁₂ structure analysis

Fig.3.17 (a)-(d) shows the surface topography of the BNdT thin films measured by atomic force microscopy (AFM). Smooth and uniform surfaces and close-packed spherical grains can be observed in all BNdT samples. The mean grain size decreases from 190 to 80 nm with increasing Nd substitution content; indicating a suppression of crystal upon Nd substitution.



Fig.3.17 AFM surface topography of (a) $Bi_4Ti_3O_{12}$, (b) $Bi_{3.75}Nd_{0.25}Ti_3O_{12}$, (c) $Bi_{3.5}Nd_{0.5}Ti_3O_{12}$, and (d) $Bi_{3.15}Nd_{0.85}Ti_3O_{12}$ thin films.

Fig.3.18 shows the Raman spectra of $Bi_{4-x}Nd_xTi_3O_{12}$ (x=0, 0.25, 0.5, and 0.85) crystals at room temperature, from 50 to 1000 cm⁻¹. Raman selection rules allow 24 Raman active modes ($6A_g+2B_{1g}+8B_{2g}+B_{3g}$) for the orthorhombic $Bi_4Ti_3O_{12}$ [152-154]. However, only 8 Raman modes can be indexed, which can be attributed to the symmetry breaking, TiO₆ octahedron distortion, vibration mode overlap, and the weak feature of some Raman peaks [155-157]. Raman active modes located at 60, 90, and 121 cm⁻¹ originate from the bismuth displacement in the pseudo-perovskite slab and (Bi_2O_2)²⁺ fluorite-like layers, and the modes from 268 to 853 cm⁻¹ can be classified as internal vibration modes of TiO₆ octahedral of perovskite unit [156,158]. Moreover, the internal modes of 268 and 329 cm⁻¹ can be attributed to the O-Ti-O bending, while the mode at 853 cm⁻¹ is caused by the Ti-O symmetric stretching of TiO₆ octahedral, and the Raman modes at 552 and 627 cm⁻¹ can be ascribed to the combination of bending and stretching of TiO₆ octahedral [154].



Fig.3.18 Raman scattering spectrum of Bi_{4-x}Nd_xTi₃O₁₂ (x=0, 0.25, 0.5, and 0.85) thin films.

It can be seen that Raman modes at 90 and 121 cm⁻¹ corresponding to the Bi mode in $(Bi_2O_2)^{2+}$ layers become broad and soft with high Nd substitution content, indicating an increased lattice distortion due to the substitution of Bi with Nd atoms. However, no obvious mode shift is observed in this region, showing that the Nd additive stays mainly inside the perovskite units and does not incorporate into the fluorite-like layers [144,154,158]. Meanwhile, significant changes can be indexed at modes from 268 to 853 cm⁻¹ with the increase of Nd doping concentration, such as the shift of the mode at 268 cm⁻¹, and the broadening and softening of the modes at 268, 552, and 853 cm⁻¹, indicating tilting and distortion in TiO₆ octahedral and more difficulty in achieving perovskite phase with increased Nd content [156,158].

3.6 Conclusion

In this chapter, we demonstrated the fabrication process and properties characterization of the BNdT ferroelectric thin film. From the precursor preparation to the sol-gel/spin coating fabrication, and from the structural characterization to the ferroelectric investigation, the fabrication dependence of BNdT properties were investigated in detail. An optimized fabrication process was obtained based on previous research, and will be further applied in the coming chapters. $Bi_{4-x}Nd_xTi_3O_{12}$ thin films with different Nd doping concentrations were also prepared to study the dependence of BNdT properties on Nd doping concentration.

Chapter 4

Optical Properties of Ferroelectrics and their Optimization

4.1 Introduction

Since the first report by Chon *et al.* [34], there has been much research done examining the electrical properties of BNdT ferroelectric thin films, confirming the advantages of using this material in electrical-domain applications [35-37]. However, so far little attention has been paid to the optical properties of the BNdT material. There was one report regarding the band gap energy fitting from an ellipsometer measurement [38], which provided a basic theoretical understanding of the optical properties of the BNdT material. However, a detail optical investigation including parameters such as transmittance T, refractive index n, extinction coefficient k, etc. was not entirely done. To the best of our knowledge, there has been no systematic investigation of the optical properties of the BNdT material. Furthermore, different impact mechanisms such as the crystallization temperature, quantum scale, and ingredient substitution on the BNdT thin film optical properties are never investigated. In this chapter, we present the first experimental study on the subject, and provide a useful understanding of the correlation between different impact mechanisms and the optical properties of BNdT thin films.

The remainder of this chapter is organized as follows. Section 4.2 introduces three different impact mechanisms on the optical properties of BNdT thin film, and discusses the physical nature of these impact mechanisms. From Sections 4.3 to 4.5, we independently evaluate the effect of these three impact mechanisms on the BNdT optical properties. More specifically, Section 4.3 explores the dependence of the BNdT optical parameters on the crystallization temperature such as the transmittance spectrum, refractive index, extinction coefficient, and band gap energy. In Section 4.4, the impact of quantum scale is presented and investigated. Section 4.5 continues this research by testing scenarios of different Nd ingredient substitution. Finally, this chapter is summarized and concluded in Section 4.6.

4.2 Three different mechanisms

Optical properties are an intrinsic part of all ferroelectric materials. The optical behaviour is determined by the material itself and by the microstructure of the as-prepared samples. Different materials possess different optical properties; for example, PZT and SBT materials exhibit different refractive indexes and EO coefficients, and thus have different application prospects. Even within the same material, optical properties may exhibit significant variations due to different fabrication approaches. As explained in the previous section, different fabrication methods will provide obvious differences in crystal quantity, residual stress, lattice constant, etc., and will thusly impact the properties of the material in optical applications. In general, microstructure plays an important role in

determining the properties of the ferroelectric material. As discussed in the previous chapter, the ferroelectric properties are significantly affected by the microstructure of the material itself; similarly, the optical properties of the ferroelectric thin film are also impacted. There are three major mechanisms that can be involved when researching the optical properties of the BNdT ferroelectric thin film, namely, crystallization temperature, quantum scale, and ingredient substitution.

4.2.1 Crystallization temperature

As a critical fabrication parameter, the crystallization process directly determines the growth and properties of the BNdT ferroelectric material. During the crystallization process, the ferroelectric material transforms from an amorphous phase to the desired perovskite phase [132]. The annealing temperature and annealing time determine the transformation rate and efficiency. If the annealing temperature is too low, the BNdT will end up with pyrochlore phase rather than perovskite phase [158,159]. If the annealing temperature rises too high, a large amount of Bi will volatilize, resulting in more vacancies and defects in the crystal. The annealing time is also very important in this process, as even though the temperature rises past the phase transition temperature, the transformation process will still start with amorphous phase to pyrochlore phase as an intermediate state, and it will continue to change to a perovskite phase. Moreover, due to the sparse nature of the pyrochlore phase, compared with the dense structure in the perovskite phase, the intermediate pyrochlore phase will tend to stay during the transformation process [158,159]. Only with a sufficiently long annealing time can the transformation process go forward and allow the transition from the amorphous phase to the desired perovskite phase. However, a long annealing time will also accelerate the volatilization of the Bi atoms and introduce crystal defects.

Recently, the wide usage of RTA has reconciled this dilemma to some degree. In the RTA process, the high gradient of temperature variation (>100 °C/s) will create active crystal vibrations and will help the BNdT material transform from amorphous phase to the desired perovskite phase in less than 1 s. The intermediate pyrochlore phase can be negligible in this process and all the energy will go towards the perovskite crystal nucleation and growth process. However, when reducing the annealing time and thus the Bi volatilization, the high gradient of temperature variation leads to more residual stress in the thin film and impacts the microstructure of the BNdT crystal. In summary, the crystallization process plays an important role in determining the microstructure and thus the optical properties of the BNdT thin film. In the coming subsection, more experiments will be presented to investigate this correlation.

4.2.2 Quantum scale

Though optical properties are intrinsic properties of materials and correlate with their microstructure and constituent components, the thin film thickness can also be an important parameter that has an impact on the optical performance of the material. The thickness of the thin film will affect the optical transmittance and absorption of the incident light, and therefore changes the transmittance of the material in the visible region. Moreover, when the film thickness is on the quantum scale, namely ~100 nm, this thickness dependence will be more notable. As reported by D. H. Bao *et al.* [160] and J. Puustinena *et al.* [161], a so-called "quantum-size" effect can be observed in the

semiconducting thin film when the film thickness drops below 200 nm. It can be observed that the optical band gap energy of the thin film increases with decreasing thin film thickness. As explained by the authors, when the crystallite dimension decreases, atoms are separated, unit cell volume is reduced by the strong residual compression stress, and grain boundaries and imperfections are increased, resulting in a quantum-size effect in the thin film and increasing the optical band gap energy. In the coming section, the optical properties dependence on film thickness will be investigated in detail.

4.2.3 Ingredient substitution

The BNdT ferroelectric material is Nd-doped bismuth titanate, where Nd atoms substitute the Bi atoms in the crystal. Since Nd and Bi possess different atomic radii, Nd substitution introduces distortion of the lattice and thus changes the lattice constant of the $Bi_{4-x}Nd_xTi_3O_{12}$ material. Different Nd doping concentrations will provide different degrees of lattice distortion, from pure $BiTi_3O_{12}$ crystal to highly distorted $Bi_{3.15}Nd_{0.85}Ti_3O_{12}$ crystal. As discussed in the previous chapter, Raman scattering analysis shows the shift, and broadening and softening, of the active modes with the increase of Nd substitution concentration. These effects indicate a tilting and distorting in the TiO₆ octahedral, and lead to more difficulty achieving perovskite phase upon increased Nd content [156,158]. Such a tendency for variation leads to a deterioration in the microstructure and modulates the optical properties of the BNdT thin film correspondingly. In this chapter, different Nd substitution concentrations from x=0 to x=0.85 will be investigated in the $Bi_{4-x}Nd_xTi_3O_{12}$ material and accordingly, the optical property variation will be recorded and illustrated.

4.3 Crystallization temperature

In this section, the Bi_{3.15}Nd_{0.85}Ti₃O₁₂ thin film is processed at different crystallization temperatures from 300°C to 650°C, and different optical parameters such as the optical transmittance spectrum $T(\lambda)$, refractive index *n*, extinction coefficient *k*, and optical band gap $E_{\rm g}$, are characterized and investigated.

4.3.1 Optical transmittance

Measurement principle

The optical transmittance of a thin film material is always characterized by an Ultraviolet-visible-near infrared (UV-Vis-NIR) Spectrophotometer. The absorption spectrum of a material is explained as follows: molecules and atoms absorb photons at a specific wavelength of incident light, resulting in transition of the corresponding molecular vibration level or electron level. Since different materials possess different molecules and atoms and thus different molecular vibrations and electron levels, the absorption spectrum can be used to distinguish between different materials. Moreover, the same material with different microstructures also possesses different transition levels and can possess different absorption spectrums in measurements. Therefore, the absorption spectrum can be used as an identification method to differentiate between different material natures and structures. Absorption or transmittance intensities at a specific wavelength can be further used to analyze the constituents of the material achieved. Spectrophotometric analysis can be a simple but effective way of characterizing the material constituent, structure, and inter-reaction. According to the different absorption spectrum regions, spectrophotometric analysis can be classified into

the ultraviolet region (100 to 400 nm), the visible region (400 to 800 nm) and the near infrared region (800 to 3000 nm).

The major principle of UV-Vis-NIR analysis is the Lambert-Beer law, described as follows,

$$A = \log_{10}\left(\frac{1}{T}\right) = \varepsilon bl, \qquad (4.1)$$

where A is the absorption coefficient, T is the optical transmittance, ε is the molar absorption coefficient, b is the molar concentration, and l is the thickness of the sample.

The Lambert-Beer law is an ideal formula that assumes that the incident light is monochromatic and normally incident, the absorbance media are homogeneous, and incident optical path lengths are equivalent. Under imperfect measurement conditions, the Lambert-Beer law can only provide an approximation.

Measurement parameter configuration

Instrument: Lambda 19 spectrophotometer (Perkin Elmer, USA).

Parameter configuration: Samples are cut into 2cm*2cm squares. To minimize the substrate absorption in the UV region, optical graded fused quartz was employed as the substrate, and a blank contrast sample was used to calibrate the spectrophotometer each time after a full wavelength scan.

Results and analysis

Fig.4.1 (a) shows the optical transmission spectra $T(\lambda)$ of the BNdT samples at UV-Vis-NIR wavelengths from 200 to 2000 nm. There are three transmission spectra for BNdT thin films with 200 nm thickness post-annealed at temperatures from 400°C to 650°C. The absorption edge can be observed in the vicinity of 350 nm. According to the definition by R. Swanepoel *et al.* [162], the region from 930 to 2000 nm can be considered as the weak absorption region of BNdT, while from 480 to 930 nm, BNdT shows medium absorption capacity and up to 480 nm is the strong absorption region. Around the 1550 nm region, which is the typical operating range for optical communications, the BNdT thin film exhibits more than 80% transmittance [132]. Based on the oscillatory characteristics of the transmission curves, we conclude that BNdT thin films have a flat surface and a uniform thickness, consistent with the SEM and AFM results shown in the previous sections.



Fig.4.1 (a) Transmission spectra of BNdT thin films with thickness of 200 nm at different postannealing temperatures from 400° C to 650° C. (b) Zoomed-in figure of optical absorption band in UV region.

We also observe that the transmission of BNdT increases with increasing post annealing temperature as follows: from 67% at 400°C to 88% at 650°C, at a wavelength of 1550 nm. This phenomenon can be explained by three factors. As reported by J. Lappalainen *et al.* [163], the transmission of ferroelectric thin films can be increased by an improved crystallinity. As shown in the XRD analysis of Section 3.3.1, by increasing the post annealing temperature, crystallinity increases and the percentage of amorphous phase decreases, resulting in a better perovskite structure with higher c-axis orientation. Another reason for the transmission behaviour is the stress relaxation that occurs during the annealing process. In the XRD measurement, it can be seen that the full width at half maximum (FWHM) of the BNdT crystal changes due to the macroscopic stress of the peak shift as well as the microscopic stress of the peak narrowing with the increase of post annealing temperature. This leads to a stress relaxation process and changes the optical transmission properties of the BNdT thin film. Thirdly, the glass transformation process might also be considered since it plays an important role in determining the optical properties of amorphous and polycrystalline materials including silicon based oxide compounds [132,164]. When the initially amorphous material is annealed above the glass transformation temperature, it will transform into a viscous liquid state. Nucleus formation and crystallization processes will then take place and will affect the optical properties of the material. By increasing the annealing temperature from 400°C to 650°C, the glass transmission temperature of BNdT should be reached and the optical properties would be impacted correspondingly.

4.3.2 Refractive index and extinction coefficient

Measurement principle

Spectroscopic ellipsometry is a precise characterization method that can be used to measure the optical parameters of a bulk or a thin film material. It has a non-destructive, non-disturbing measurement mechanism, and a flexible operation environment, making it a popular characterization method in the modern optical measurement and modeling field. The basic principle of the spectroscopic ellipsometry measurement can be explained as follows: when a beam of polarized light is incident on the surface of the sample, the polarization state will change during reflection and refraction, and the study of such polarization state variation can help to extract optical parameters such as the refractive index and the extinction coefficient of the as-measured sample.



Fig.4.2 Schematic illustration of the multi-reflection and multi-refractive pattern of the light transmission.

When a beam of light is incident on the top surface of a thin film material, reflection and refraction co-exist. Usually, the refractive indexes of different dielectric layers are presented as n_1 , n_2 , and n_3 . The incidence and refraction angles are θ_1 and θ_2 , respectively. Fig.4.2 shows a multi-reflection and multi-refractive pattern of light transmission. It can

$$2\omega = \frac{4\pi d}{\lambda} \sqrt{n_2^2 - n_1^2 \sin^2 \theta_1} . \tag{4.2}$$

The total amplitude of reflected light A_{tr} can be calculated as the sum of all the reflected light (a), (b)...(n), as follows,

$$A_{ir} = r_1 + t_1 t_1^* r_2 e^{-i2\omega} + t_1 r_2^2 r_1^* t_1^* e^{-i4\omega} + \dots = r_1 + t_1 t_1^* r_2 e^{-i2\omega} \sum_{l=0}^{\infty} r_2 r_1^* e^{-i2\omega}$$
$$= r_1 + \frac{t_1 t_1^* r_2 e^{-i2\omega}}{1 - r_2 r_1^* e^{-i2\omega}}$$
(4.3)

where r and t are the reflectance and transmission coefficients, respectively, of the thin film.

According to the analysis of Snell's Law, $r_1^* = -r_1$ and $t_1 t_1^* = 1 - r_1^2$.

This substitution allows Eq.4.3 to be rewritten as,

$$A_r = \frac{r_1 + r_2 e^{-i2\omega}}{1 + r_1 r_2 e^{-i2\omega}}.$$
(4.4)

Therefore, the total reflectance coefficient R can be given as,

$$R = \frac{A_r}{A_i} = \frac{r_1 + r_2 - 2r_2 \sin^2 \omega - 2ir_2 \sin \omega \cos \omega}{1 + r_1 r_2 - 2r_1 r_2 \sin^2 \omega - 2ir_1 r_2 \sin \omega \cos \omega}$$

= $\frac{(r_1 + r_2 - r_2 \sin^2 \omega - 2ir_2 \sin \omega \cos \omega)(1 + r_1 r_2 - r_1 r_2 \sin^2 \omega + 2ir_1 r_2 \sin \omega \cos \omega)}{(1 + r_1 r_2 - r_1 r_2 \sin^2 \omega)^2 + 4r_1^2 r_2^2 \sin^2 \omega \cos^2 \omega}$
= $\frac{r_1 + r_1 r_2^2 + r_2 \cos 2\omega + r_2 r_1^2 \cos 2\omega - ir_2 \sin 2\omega + ir_1 r_2 \sin 2\omega}{1 + 2r_1 r_2 \cos 2\omega + r_1^2 r_2^2 \cos^2 2\omega + r_1^2 r_2^2 \sin^2 2\omega}$. (4.5)

Since the polarized light can be orthogonally decomposed into horizontal component P waves and vertical component S waves, the reflectance coefficient can also be decomposed into P and S components, as follows,

$$R_{p} = \frac{r_{1p} + r_{2p}e^{-i2\omega}}{1 + r_{1p}r_{2p}e^{-i2\omega}}$$
(4.6)

$$R_s = \frac{r_{1s} + r_{2s}e^{-i2\omega}}{1 + r_{1s}r_{2s}e^{-i2\omega}}.$$
(4.7)

We can define a complex reflectance ratio G, by using $\tan \xi$ and Γ to represent its absolute value and argument, as follows,

$$G = \frac{R_p}{R_s} = tg\xi e^{i\Gamma} .$$
(4.8)

Incorporating Eq.4.2 to Eq.4.8, we can calculate

$$\tan \xi = \sqrt{\frac{r_{1p}^{2} + r_{2p}^{2} + 2r_{1p}r_{2p}\cos 2\omega}{1 + r_{1p}^{2}r_{2p}^{2} + 2r_{1p}r_{2p}\cos 2\omega}} \cdot \frac{1 + r_{1s}^{2}r_{2s}^{2} + 2r_{1s}r_{2s}\cos 2\omega}{r_{1s}^{2} + r_{2s}^{2} + 2r_{1s}r_{2s}\cos 2\omega}$$
(4.9)

$$\Gamma = \arctan\left[\frac{r_{1p}^{2}r_{2p}\sin 2\omega - r_{2p}\sin 2\omega}{r_{1p} + r_{1p}r_{2p}^{2} + r_{2p}\cos 2\omega + r_{1p}^{2}r_{2p}\cos 2\omega}\right] - \arctan\left[\frac{r_{1s}^{2}r_{2s}\sin 2\omega - r_{2s}\sin 2\omega}{r_{1s} + r_{1s}r_{2s}^{2} + r_{2s}\cos 2\omega + r_{1s}^{2}r_{2s}\cos 2\omega}\right]$$
(4.10)

$$(n_{2} + jk_{2}) = (n_{1} + jk_{1})\sin\theta \sqrt{1 + \left(\frac{1 - G}{1 + G}\right)^{2} \tan^{2}\theta}$$
(4.11)

Therefore, it can be concluded that the material's optical parameters correlate with G, tan ξ , Γ , and θ . Further, in the Spectroscopic ellipsometry method, tan ξ and Γ can be precisely measured; and by using a linear regression algorithm with the Multiple Lorentz oscillator model [165], the refractive index *n* and extinction coefficient *k* can be fitted using the following equations [166,167],

$$n(\lambda) = \alpha_n + \frac{10^6 \beta_n}{\lambda^2} + \frac{10^{12} \gamma_n}{\lambda^4}$$
(4.12)

$$k(\lambda) = \alpha_k + \frac{10^6 \beta_k}{\lambda^2} + \frac{10^{12} \gamma_k}{\lambda^4}$$
(4.13)

where α_n , β_n , and γ_n are the refractive index Cauchy coefficients, and α_k , β_k , and γ_k are the extinction coefficient Cauchy coefficients.

Results and analysis

Fig.4.3 (a)-(b) shows the refractive index n and extinction coefficient k of the BNdT thin films as a function of wavelength at different post annealing temperatures. It can be observed that the refractive index curves are flat in the UV-Vis region and increase abruptly towards shorter wavelengths, indicating a typical dispersion characteristic. The strong increase in the refractive index around 350 nm can be attributed to the band gap absorption, which was investigated in Fig.4.1. The extinction coefficient k also decreases as the wavelength increases, which is consistent with the Kramers-Kronig relations [168]. The extinction coefficient is high at shorter wavelengths, indicating material absorption in the UV region, and decreases rapidly from the visible region where the thin films are nearly transparent. The dependence of refractive index on the annealing temperature can also be observed from the curves. It can be seen that the refractive index of the thin film increases gradually with increasing the post annealing temperatures, from 2.33 at 300°C to 2.49 at 650°C, at a wavelength of 1550 nm. This variation can be attributed to the percentage of amorphous phase in the BNdT thin film. As reported by Y. M. Chen et al. [38], polycrystalline thin film shows a larger refractive index compared with the amorphous thin film. With the increase in post annealing temperature, the proportion of amorphous film decreases, affecting the crystal structure as well as the electronic band gap and the lattice constant [169], leading to the improved refractive index. Another factor is the mean grain size induced refractive index improvement. With increasing annealing temperature, the thin film's mean grain size increases, which was confirmed by the AFM results discussed in the previous section. This leads to a change in the volume ratio of the grain boundary and perovskite phase fraction, resulting in a change in the high frequency dielectric constant and thus the refractive index of the thin film.



Fig.4.3 (a) Refractive index n of BNdT thin films at different post-annealing temperatures. (b) Extinction coefficient k of BNdT thin films at different post-annealing temperatures.

4.3.3 Optical band gap energy

Measurement Principle

Optical transmittance data can be used to determine the optical band gap energy. To fit the band gap energy, the measured transmittance T should be converted into the absorption coefficient α , using the following relationship,

$$\alpha = -\ln(T) / d \tag{4.14}$$

where *d* is the thickness of BNdT thin film. In the strong absorption region, the absorption coefficient α and band gap energy E_g can be given by the Tauc relation [170]:

$$(\alpha hv)^m = C(hv - E_{\sigma}) \tag{4.15}$$

where *C* is a constant, and *m* is an exponent representing the transition type in the material. More specifically, m=2 refers to a direct band gap, while m=1/2 suggests indirect band gap behaviour. The band gap energy can thus be obtained by extrapolating the linear portion of $(\alpha h v)^m$ and hv to $(\alpha h v)^m=0$. As shown in Fig.4.4 (a), for the BNdT thin film of 250 nm annealed at 300°C, good linear fits above the band gap can be observed in the $(\alpha h v)^2$ versus hv graph, while $(\alpha h v)^{1/2}$ versus hv does not show the clear slope expected in an indirect bang gap material; therefore the optical transitions of BNdT are direct.





Fig4.4 (a) Optical absorption coefficient vs. photon energy of BNdT thin film (250 nm) processed at 300°C (b) Band gap energy of BNdT thin films (250 nm) at post annealing temperatures from 300°C to 650°C.

Fig.4.4 (b) shows the band gap energy E_g values of the BNdT thin films (250 nm) processed at different annealing temperatures from 300°C to 650°C, indicating a modulation effect of the band gap energy during the fabrication process. It can be seen that, in the 250 nm thick samples, E_g values drop from 3.42 to 3.02 eV as the post annealing temperature increases from 300°C to 650°C. This variation agrees with the results of traditional ferroelectric material PZT reported in the literature [171,172]. As indicated in these papers, amorphous thin films exhibit larger E_g values compared to polycrystalline films. In the lower temperature annealed samples, more amorphous material is remanent, leading to larger free carrier concentrations and more potential barriers across the boundaries, yielding larger internal electric fields and thus increasing the optical band gap.

4.4 Quantum scale

In this section, $Bi_{3.15}Nd_{0.85}Ti_3O_{12}$ thin films with thicknesses from 50 to 100 nm are processed at a crystallization temperature of 650°C, and different optical properties such as the optical transmittance spectrum $T(\lambda)$ and optical band gap E_g , are characterized to investigate the importance of quantum scale in determining the optical performance of the BNdT ferroelectric thin film.

4.4.1 Optical transmittance

Fig.4.5 shows the optical transmission spectra of the BNdT samples at UV-Vis-NIR wavelengths from 200 to 2000 nm. There are three transmission spectra for BNdT thin films with thicknesses of 50, 100, and 200 nm, post-annealed at 650°C. It can be seen from Fig.4.5 (a) that the optical transmittance at 1550 nm does not show obvious differences with increasing of thin film thickness, indicating that compared with the obvious impact provided by the crystallization temperature, quantum scale does not play an important role in determining the optical transmittance of the BNdT ferroelectric thin film. However, an optical absorption edge blue shift is observed by decreasing the film thickness, which is in agreement with the result reported in traditional ferroelectric PZT materials [165], indicating an increase in the band gap energy. This effect will be discussed in the upcoming section.



Fig.4.5 (a) Transmission spectra of BNdT thin films with thicknesses from 50 to 200 nm at 650°C post-annealing temperature. (b) Zoomed-in figure of optical absorption band in UV region.

4.4.2 Optical band gap energy

Fig.4.6 shows the band gap energy E_g values of the BNdT thin films. For ease of comparison with Section 4.3.3, BNdT thin film with thicknesses from 50 to 250 nm are processed at different annealing temperatures from 300°C to 650°C, and both the E_g values dependence on film thickness and annealing temperature can be observed. At the same post annealing temperature, the band gap energy increases as the film thickness decreases. As presented in Fig.4.6, for the annealing temperature of 300°C, E_g increases

from 3.42 to 3.76 eV as the thickness decreases from 250 to 50 nm. This is similar to the results reported by D. Bao *et al.* [160], in which the measured optical band gap energy in $SrTiO_3$ thin layers is larger than in thick layers. The quantum-size effect in semiconducting thin films can explain this phenomenon. When the thickness decreases, the crystallite dimension also decreases, separating the inner atoms and reducing the unit cell volume by means of increased residual compression stress. The grain boundaries and imperfections are increased during this process. Such quantum-size effect, caused by the thin film thickness scaling down, will eventually impact the optical performance of the thin film and increase the optical band gap energy.



Fig.4.6 Band gap energy of BNdT thin films with thicknesses from 50 to 250 nm at post annealing temperatures from 300°C to 650°C.

4.5 Ingredient substitution

In this section, we prepare $Bi_{4-x}Nd_xTi_3O_{12}$ (x=0, 0.25, 0.5, and 0.85) material with different Nd contents and report on how the Nd content affects the optical properties of

the Bi_{4-x}Nd_xTi₃O₁₂ material. It will be seen that, as with annealing temperature, different ingredient substitutions also exhibit considerable impact on the material's optical properties. Due to the ingredient change, some of the Bi_{4-x}Nd_xTi₃O₁₂ material with a thickness of 200 nm exhibits mild cracking during the annealing process. In order maintain the same comparison criteria, we change the fabrication condition to ensure the flatness and uniformity of the films utilized in the experiment. We increase all the Bi_{4-x}Nd_xTi₃O₁₂ films to 500 nm thickness, change the excess amount of bismuth titanate from 10% to 5%, and replace the crystallization annealing process with a RTA process at 600°C for 10 minutes in an air atmosphere. With this change, we finally obtained clear and uniform BNdT thin films.

4.5.1 Optical transmittance

The measured optical transmittance spectra $T(\lambda)$ of Bi_{4-x}Nd_xT₃O₁₂ (x=0, 0.25, 0.5, and 0.85) thin films (500 nm in thickness) at wavelengths from 300 to 800 nm are presented in Fig.4.7 (a). It can be seen that all BNdT thin films exhibit a transmittance of >50% in the region from 600 to 800 nm, indicating a relatively weak optical absorption. The films also exhibit a weak transparency of <10% with wavelengths less than 350 nm due to the UV absorption in this region. The absorption edge can be observed around 330 nm. The oscillatory manner of the transmittance curves indicates that a uniform and flat surface topography of the BNdT thin films has been achieved.

Nd content plays a critical role in determining the optical transmittance properties of BNdT thin films. It can be concluded that the BNdT thin film's transmittance decreases from 63% to 43%, at a wavelength of 600 nm, as the Nd content increases from 0 to 0.85.

This phenomenon can be attributed to the crystallinity variation with Nd substitution. In the previous section, explained by Raman analysis, crystallinity decreases with the increase in Nd substitution content. Since the transmittance of ferroelectric thin films can be reduced by a degraded crystallinity quality [163], less optical transparency will be observed under an increase in Nd substitution. Another contributing reason is the substitution induced stress relaxation process. Due to the radius differences in Nd and Bi atoms, the lattice constant will vary with increasing Nd content, resulting in an amplification of the lattice distortion, and thus a larger stress relaxation in the crystallization process and a corresponding change in the optical properties of the thin film. Meanwhile, the optical absorption edge shift can be observed by changing the Nd content, as shown in Fig.4.7(b), implying that a band gap energy variation also exists upon Nd substitution, which will be investigated in the coming section.





Fig.4.7 (a) Transmission spectra of $Bi_{4-x}Nd_xTi_3O_{12}$ (x=0, 0.25, 0.5, and 0.85) thin films with thickness of 500 nm. (b) Zoomed-in figure of the optical absorption band in the region from 320 to 360 nm.

4.5.2 Refractive index and extinction coefficient

Fig.4.8 shows the dependence of the refractive index n and extinction coefficient k on wavelength, for BNdT thin films (500 nm in thickness) with different Nd substitution contents, as obtained from an ellipsometer measurement. A typical dispersion characteristic can be observed in the refractive index curves of all the BNdT thin films, namely, a flat curve beyond the 400 nm wavelength region, and a quick increase towards shorter wavelengths. The abruptly increase in refractive index curves around 330 nm can be attributed to the band gap absorption around this wavelength, which was illustrated in Fig.4.7. The extinction coefficients exhibit large values below 330 nm indicating a strong optical absorption, and drops quickly to near zero upon longer wavelengths indicating a good transparency characteristic in this region. The optical transparency obtained from the ellipsometer measurement shows good agreement with the transmittance measurement, and confirms the optical properties of the BNdT thin films achieved in our work. The refractive index dependence on Nd doping content is shown in Fig.4.8. It can

be seen that the refractive index decreases slightly with an increase in Nd content, from 2.48 at x=0 to 2.2 at x=0.85, at 800 nm wavelength. The mean grain size variation upon Nd substitution can be also an important factor. As indicated in the AFM measurement, the mean grain size of the BNdT crystal decreases with the increase of Nd doping content, leading to a change in the perovskite phase fraction and the volume ratio of the grain boundary, thus changing the high frequency dielectric constant of BNdT and the measured refractive index correspondingly [173].



Fig.4.8 Refractive index and extinction coefficient of $Bi_{4-x}Nd_xTi_3O_{12}$ (x=0, 0.25, 0.5, and 0.85) thin films.

4.5.3 Optical band gap energy

The band gap energy of BNdT thin films is plotted as a function of Nd substitution content in Fig.4.9. It can be seen that the band gap energy increases from 3.4 to 3.5 eV as the Nd substitution content increases from x=0 to x=0.85. The lattice parameter variation and crystal distortion during the doping process can be recognized as an important

contributing factor to the change in band gap energy. By increasing the Nd substitution content in the BTO system, the lattice parameter varies and the crystal distortion increases, as explained by XRD and Raman analysis, working together to impact the crystallinity quality of the BNdT thin film achieved, and thus impacting the measured band gap energy. In the weak doping region, the introduction of Nd atoms with larger atomic weight compared to the Bi atoms will help increase the energy of the chemical bond with oxygen atoms and thus increase the band gap energy. However, with the increase of Nd doping concentration, the non-bridging oxygen ions will also increase. Such non-bridging oxygen ions will possess less binding capacities with the excited electrons compared with the bridging oxygen [174,175], resulting in a negative factor to the band gap energy increase, and thus a decrease in growth rate following an Nd content increase. Further, the Nd-O bonds may also be broken or dangled by the non-bridging oxygen ions [174], leading to more crystal distortion in the BNdT thin film.



Fig.4.9 Band gap energy variation with Nd substitution contents from 0 to 0.85 eV.

4.6 Conclusion

In this chapter, several optical parameters such as transmittance *T*, refractive index *n*, extinction coefficient *k*, and optical band gap energy E_{g} , of the BNdT ferroelectric thin film were investigated in detail. We started with the BNdT optical properties variation due to crystallization temperature, demonstrating that different annealing temperatures will impact the amorphous percentage and stress relaxation process, and thus change the optical performance of the BNdT material. Then, the quantum scale effect was examined and found to be responsible for changes in the unit cell volume and grain boundaries, variations that have an impact on the optical performance of the BNdT material. Finally, the ingredient substitution effect was examined. It was concluded that different Nd substitution concentrations could change the crystallization distortion of Bi_{4-x}Nd_xT₃O₁₂ materials, and modulate the optical parameters. Our study presented the first systematic experimental study on this subject and demonstrated well-defined optical properties of the BNdT material. Moreover, the study presented here, on different impact mechanisms, provides us with more freedom to optimize the optical performance of BNdT.

Chapter 5

Multiferroic and Optimization

5.1 Introduction

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polarization (P_r) of 100 μ C/cm², and other chemical solution deposition (CSD) derived BFO thin films also exhibit good polarization performance [183].

However, it is difficult to characterize ferroelectric properties at room temperature because the BFO material has low resistivity, which prevents it from exhibiting maximum polarization performance [80,81]. The low resistivity can be attributed to the Fe ions (Fe³⁺ and Fe²⁺) valence fluctuation, Bi atoms volatile nature, oxygen vacancies, and impurity phases [41,79]. In this chapter, we examine different attempts to optimize the ferroelectric properties of the BFO material, and demonstrate successful room temperature characterization of it.

The remainder of this chapter is organized as follows. Section 5.2 introduces two different optimization approaches used in this experiment and describes the physical nature of these two methods. Starting from Section 5.3, we focus on the first optimization routine, namely, the multilayer methodology. Fabrication technology, structural analysis, ferroelectric characterization, and dielectric examination are described in detail in Sections 5.3 to 5.6. In the latter part of this chapter, we move on to discuss another optimization approach, namely, dual-site substitution technology, and we process the corresponding characterization. From Sections 5.7 to 5.9, a detailed characterization of dual-site substituted BFO materials is provided experimentally and theoretically. This chapter is summarized and concluded in Section 5.10.

5.2 Different optimization approaches

To reduce the conductivity of BFO, three different routines have been investigated and reported in the literature, namely, a single phase BFO compound [82], a formation of a

solid solution with other ABO₃ pervoskite materials [83], and ion atoms substitution at Bi and Fe sites in the BFO crystal [84]. However, the first two methods have intrinsic disadvantages that prevent their further application in the multiferroic field. In the single phase BFO, leakage paths are dramatically reduced due to the improvement in ferroelectric phase, and the ferroelectric hysteresis loop can be measured by deducing the conductivity. However, single phase BFO can only be achieved by molecular beam epitaxy (MBE). MBE is an expensive fabrication technology and the growth rate is fairly low, preventing it from meeting large-scale production demands. The solid solution approach mixes BFO and other ABO₃ perovskite materials, such as BaTiO₃, PbFe_{0.5}Nb_{0.5}O₃, PZT, PbTiO₃, PrFeO₃, and DyFeO₃ [184-187]. The similar crystal structure promotes the crystallization process of the BFO material and helps to induce a relatively well-defined pseudo single crystal phase in the BFO material. However, the high operational temperature in the process is not compatible with existing silicon-based technology and prevents the integration of BFO into current silicon-based memory applications. Moreover, the addition of different ABO₃ materials introduces impurities

In this study, we initiate an innovative multilayer technology by introducing a seeding layer between the BFO ferroelectric and the silicon substrate. With this seeding layer, the crystallization process of the upper BFO material can be induced, resulting in a better

and results in a transition phase in the fabrication process. Among the three routines, ion

atoms substitution is the most effective technology in reducing the conductivity of BFO.

Numerous doping elements were introduced into BFO, and rare-earth ions such as La, Nd,

and so on, are considered to be the most successful attempted thus far due to their control

over the volatile nature of Bi and the suppression of oxygen vacancies [41].

degree of crystallinity and lower leakage properties. Meanwhile, we improve the existing ion atoms substitution technology and demonstrate a Bi and Fe dual-site substitution in the optimization of BFO ferroelectric properties.

5.2.1 Multilayer technology

Multilayer technology is guite mature in thin film fabrication and characterization. By depositing different thin film materials on the substrate, the as-prepared multilayer can exhibit different properties compared to films of any other composition. During the deposition process, different layers impact each other and change the structural and thus the functional properties of the entire multilayer. In this multi-inducing process, the lower layer, known as the seeding layer, plays an important role in the crystallization process of the upper layer. During all thin film deposition processes, the nucleation and crystallization process is highly determined by the substrate; the same fabrication recipe will result in completely different material crystallizations with different substrates. In multilayer technology, the seeding layer is carefully selected and only materials with the same crystal type, similar lattice parameters, and compatible fabrication conditions will be considered. An appropriate seeding layer will improve and induce the crystallization process of the upper layer and dramatically improve the functional properties in an application [188]. In our experiment, BNdT thin film, discussed in Chapters 3 and 4, is used as the seeding layer of the BFO material. The well-defined ferroelectric properties and similar lattice parameters make BNdT a promising option for the seeding layer in this multilayer structure.
5.2.2 Rare-earth ions substitution

As with multilayer technology, rare earth substitution also aims to improve the electrical resistivity of the BFO material and thus improve the room temperature application performance. As explained at the beginning of this chapter, the relatively low electric resistivity of BFO is attributed to the valence fluctuation of Fe ions (Fe^{3+} to Fe^{2+}), which requires oxygen vacancies for charge compensation and produces electron hopping in films. The oxidation state of Fe greatly depends on the processing conditions and the type and amount of dopants [79]. In order to improve the polarization properties of BFO at room temperature, the site-engineering concept has been proposed. There has been much research done on enhancing the room temperature ferroelectric properties of the BFO thin film with rare earth and other ions substitution. For example, Bi-site substitution with La and Nd atoms for controlling volatile Bi atoms and suppressing generation of oxygen vacancies has been attempted in BFO thin films [40,41]; as well, Fe-sited substitutions such as Nb and Mn atoms have been reported by S. K. Singh and C. F. Chung, et al. to fill oxygen vacancies in bulk ceramics [39,42,43]. However, most of the reports to date focus on single-site substitution (Bi-sited or Fe-sited), and less attention has been devoted to Bi and Fe dual-site substitution in the optimization of BFO ferroelectric properties. In this chapter, we report the Bi and Fe dual-site substituted BFO crystal with La, Nd, Nb, and Mn. The structural, ferroelectric, and electrical properties of different substituted BFO materials will be investigated and compared. An optimized substitution pattern that can be applied in BFO-based electrical and magnetic applications is obtained from this study.

5.3 Multilayer fabrication

In our experiment, the multilayer structure is composed with a thin BNdT seeding layer and a relatively thick BFO functional layer. The precursor preparation and film fabrication process will be discussed in the following sections.

5.3.1 Seeding ferroelectric layer

The precursor preparation and film fabrication processes of the BNdT thin film are kept almost the same as in previous chapters. A typical Nd doping concentration of 0.85%, namely $Bi_{3.15}Nd_{0.85}Ti_3O_{12}$, is chosen as the formula for the seeding material, and the thickness of the BNdT thin film is 20 nm.

5.3.2 Functional ferroelectric layer

BFO is chosen as the functional material in the multilayer structure, and the precursor preparation and film fabrication processes are described below.

Precursor preparation

Since the molecular formula of the BFO sample is BiFeO₃, in order to achieve the appropriate elemental ratio in the BFO thin film, metal salt solute and the corresponding solvent should be carefully designed to provide a stable and uniform solution.

According to the literature, we choose Bismuth(III) nitrate pentahydrate, namely, $Bi(NO_3)_3 \cdot 5H_2O$, and Iron(III) nitrate nonahydrate, namely, $Fe(NO_3)_3 \cdot 9H_2O$, as the organic metal alkoxides used to provide the Bi and Fe elements. We select citric acid, $HOC(COOH)(CH_2COOH)_2$, and 2-Methoxyethanol, $CH_3OCH_2CH_2OH$, as the main solvents.

Precursor list

All chemicals are provided by Sigma-Aldrich.

Nama	Formula	Atomia Waight	Access	C 1 S
Name	Formula	Atomic weight	Assay	CAS
		(at. wt)		
Bismuth(III) nitrate	Bi(NO ₃)₃•5H ₂ O	485.07	≥98.0%	10035-06-0
pentahydrate				
Iron(III) nitrate	Fe(NO ₃) ₃ •9H ₂ O	404.00	≥98.0%	7782-61-8
nonahydrate				
Citric acid	$HOC(COOH)(CH_2COOH)_2$	192.12	≥99.5%	77-92-9
2-Methoxyethanol	CH ₃ OCH ₂ CH ₂ OH	76.09	99.8%	109-86-4

Table.5.1 Chemicals used to prepare the BFO precursor.

Precursor preparation recipe

In order to maintain the mol ratio of Bi and Fe at 1:1, the mass of both the metal salts are calculated as,

M[Bi(NO₃)₃·5H₂O] =
$$\frac{0.025 \times 0.2 \times 485.07 \times (1+10\%)}{98\%}$$
 = 2.722 g

M[Fe(NO₃)₃·9H₂O]=
$$\frac{0.025 \times 0.2 \times 404.00 \times 1}{98\%}$$
 = 2.061 g

A detailed precursor preparation process is described as follows.

(1) 2.722 g Bi(NO₃)₃·5H₂O and 2.061 g Fe(NO₃)₃·9H₂O are both dissolved in CH₃OCH₂CH₂OH for a total volume of 50 ml. Excess bismuth nitrate of 10% is added to compensate for the Bi loss during the thermal annealing process. The mixed solution is stirred for 10 hrs.

(2) 1.584 g HOC(COOH)(CH_2COOH)₂ is then added as the deducing agent.

(3) The as-prepared precursor is stirred at 500 rpm for 10 hrs and left to stand for 24 hrs at room temperature.

(4) The as prepared solution is filtered using a 0.2 μ m filter and stored in a conical beaker.

A photograph of the as-prepared BFO solution is shown in Fig 5.1; it can be seen that a uniform and stable solution is achieved in our experiment.



Fig.5.1 A photograph of the as-prepared BFO solution.

BFO thin film fabrication

The fabrication process of the BFO ferroelectric thin film can be summarized as follows.

(1) Spin coating deposition. The as-prepared BNdT thin film is introduced as the substrate and the BFO thin film is deposited on top of the substrate. The spin rate is 2000 rpm, lasting for 1.5 min each time. This process is repeated until the desired thickness (200 nm) of the BFO thin film is obtained.

(2) Pyrogenation. The as-prepared BFO thin film is subject to a pyrogenation process at 550°C for 30 s in air, in order to help the organic solvent volatilize and the ferroelectric crystallize.

(3) Pre-crystallization annealing. The BFO thin film is then introduced to a RTA process in oxygen atmosphere. The temperature quickly rises from room temperature to 200°C, at which it is kept for 20 s, followed by an increase up to 550°C in 3.9 s (heating rate: 90 °C/s), lasting for 60 s.

(4) Crystallization annealing. After processes (1) to (3) are repeated an appropriate number of times, a crystallization annealing process of 550°C for 10 min in air is applied to the as-prepared BFO thin films.

(5) Top electrode sputtering. Top Pt electrodes are introduced by means of a DC magnetron sputtering with a shadow mask. The diameter of the top electrode is $200 \,\mu\text{m}$.

A schematic illustration of the as-prepared BFO/BNdT multilayer structure is demonstrated in Fig.5.2. For comparison purposes, different multilayer structures are fabricated and investigated. It can be concluded that different multilayer structures will display completely different performance, and that the seeding layer plays an important role in determining the ferroelectric properties of the upper BFO ferroelectric layer [188].



Fig.5.2 (a) Multilayer structure of Pt/BFO(200 nm)/BNdT(20 nm)/Pt, (b) Multilayer structure of Pt/BNdT(20 nm)/BFO(200 nm)/Pt, (c) Pt/BFO(200 nm)/Pt, and (d) Pt/BNdT(20 nm)/Pt.

5.4 Multilayer structural characterization

5.4.1 X-ray diffraction analysis

Fig.5.3 shows the XRD patterns of the BFO(200 nm)/BNdT(20 nm) multilayer, BNdT(200 nm), and BFO(200 nm) thin films. It is easy to index all of the diffraction peaks of the BFO and BNdT thin films achieved. In the Pt/BFO/Pt and Pt/BNdT/Pt structures, it is found that both the BFO and BNdT thin films achieve a good perovskite structure without any secondary phases. The BFO thin film exhibits a high (110) orientation, which is consistent with the result reported by J. G. Wan, et al. [189]. The diffraction peaks of BNdT reveal high c-axis orientation with few random oriented peaks (117), indicating good ferroelectric properties, as reported by Chon, et al. [34]. In the BFO/BNdT/Pt multilayer, BNdT still exhibits high c-axis orientation, such as (004), (006), (008), indicating that the upper BFO layer and post fabrication process does not impact the crystallization process of the BFO material. Notably, the BFO thin film is seen to have a high (110) preferred orientation and a relatively high degree of 42% (111) preferred orientation in the multilayer structure. It is also seen that the BNdT seeding layer helps enhance the growth of (111) preferred BFO grains. Coupling reactions should occur between the two ferroelectric materials, and the BNdT layer induces the crystallization and growth of the upper BFO film. As reported in the literature, the spontaneous polarization of BFO is along [111]; therefore such (111) preferred orientation BFO in the multilayer should provide better ferroelectric properties [190].



Fig.5.3 XRD patterns of multilayer Pt/BFO(200 nm)/BNdT(20 nm)/Pt, Pt/BFO(200 nm)/Pt, and Pt/BNdT(200 nm)/Pt structures.

5.5 Multilayer ferroelectric characterization

5.5.1 Ferroelectric polarization enhancement

Fig.5.4 shows the hysteresis loops of the pure BFO thin film and the multilayer BFO/BNdT capacitors with an applied voltage of 4 V. As shown in Fig.5.4 (a), the pure BFO thin film exhibits large leakage in the measurement and no saturated hysteresis loops can be observed. In the BFO/BNdT multilayer, however, it can be seen that a relatively well-defined hysteresis loop is obtained in the measurement for the first time. Further, the remnant polarization $(2P_r)$ of the multilayer is 22.1 μ C/cm², which is much higher than the value reported in single sited BFO materials [79,191]. The coercive field (E_c) is 50 kv/cm, indicating a reasonable performance improvement in the multilayer structure.



Fig.5.4 Ferroelectric hysteresis loops of (a) Pt/BFO(200 nm)/Pt, and (b) Pt/BFO(200 nm)/BNdT(20 nm)/Pt capacitors.

The enhancement in ferroelectric properties of the multilayer may be attributed to two different factors [188]. One potential reason is the coupling reaction between the two thin films, which causes an enhancement in the crystallization process and thus in the ferroelectric properties of the BFO film. Another possible reason is that it is the BNdT layer with 20 nm thickness that exhibits the excellent remnant polarization, rather than the multilayer. However, the BNdT (20 nm) sample exhibited poor remnant polarization in the measurement. The remnant polarization was about 1.2μ C/cm², as shown in Fig. 5.5

(a), which confirms for us that the improved properties are not related to the BNdT layer (20 nm) itself. Therefore, the phenomena can be attributed to the coupling reaction between the BFO upper film and the BNdT seeding layer; thus the BNdT layer plays an important role in enhancing the ferroelectric properties. In order to confirm our hypothesis, an additional experiment was conducted to verify the importance of the BNdT layer. The BFO and BNdT thin films are maintained with the same thicknesses, but now the BNdT layer is deposited on top of the BFO film instead of the other way around, using all the same fabrication processes. In this experiment, the Pt/BNdT(20 nm)/BFO(200 nm)/Pt multilayer exhibits poor ferroelectric properties, as shown in Fig.5.5 (b). Thus, it can be concluded that the dramatic enhancement of the BFO/BNdT multilayer induced the growth and crystallization of the BFO upper film, leading to a larger remnant polarization, which is consistent with the XRD analysis mentioned above.





Fig.5.5 Ferroelectric hysteresis loops of (a) Pt/BNdT(20 nm)/Pt, and (b) Pt/BNdT(20 nm)/BFO(200 nm)/Pt capacitors.

5.5.2 Fatigue properties enhancement

We perform ferroelectric fatigue tests by applying pulses of 1 MHz to the multilayer capacitors. Fig.5.6 (a) shows the normalized polarization as a function of polarization switching cycles; as well, the hysteresis loop before and after the fatigue test is shown in Fig.5.6 (b). The multilayer exhibits good fatigue properties, and it demonstrates little fatigue degradation (<5%) upon 1×10^{10} switching cycles at an applied voltage of 4 V, with little degradation observed in the two hysteresis loops. As reported by J. Wang, *et al.* [3], BFO is very sensitive to small changes in lattice parameters; also the origin of the good fatigue resistance may be attributed to the coupling between the two ferroelectric layers. Therefore, the BNdT layer induces the crystallization of the BFO film, affecting the lattice parameters of the BFO film, leading to a good fatigue resistance.



Fig.5.6 (a) Fatigue curves of normalized polarization as a function of number of switching cycles at 4V. (b) Ferroelectric hysteresis loop before and after the fatigue test.

5.5.3 CV/IV properties enhancement

CV investigation is an important topic in the study of ferroelectrics. Due to the unique memory characteristics of ferroelectrics, a ferroelectric capacitor exhibits a different CV pattern compared with that of traditional MOS capacitors. In common ferroelectrics-based memory devices, the CV patterns can be classified as MFM (Metal-Ferroelectric-Metal) type or MFS (Metal-Ferroelectric-Semiconductor) type. In the MFM type, a butterfly-shaped CV curve can be observed in the measurement. The symmetry of the CV

pattern is about the Y-axis, and the peaks of the CV curve lie on different sides of the origin.

The MFS type capacitor, on the other hand, can be classified into two subtypes: injection type and polarization type. In the injection scenario, because trapped states exist in the ferroelectric thin film, electrons will be directly injected from the semiconductor surface into the trapped states of the ferroelectric thin film. Such ferroelectric memory devices operate because of the charge injection, and an external electric field must be applied to maintain the information stored in the device. The corresponding CV curves exhibit a clockwise behaviour in the ferroelectric thin film deposited on an n-type silicon wafer, and a counter clockwise behaviour when a p-type silicon wafer is used as the substrate. In the polarization scenario, information storage is achieved through the semiconductor surface charge compensation due to the ferroelectric polarization. Since the ferroelectric material can maintain its polarization under the removal of an external electrical field, this type of memory mechanism is non-volatile. Unlike injection-based memory, the CV curves exhibit a counter clockwise behaviour in the ferroelectric thin film deposited on an n-type silicon wafer, and a clockwise behaviour with p-type silicon wafer.

In this experiment, the MFM structure is built using the Pt/BFO/BNdT/Pt multilayer capacitor, and butterfly-shaped CV curves can be observed in Fig.5.7. No polarization gap spot can be found in the CV curve under either forward or backward scans, indicating a symmetry and concordance in the spontaneous polarization. It can be concluded that the spontaneous capacitance drops to near zero around the coercive field, demonstrating that

the BFO/BNdT multilayer exhibits a random electric domain orientation and a high domain energy density.



Fig.5.7 CV curves of the Pt/BFO/BNdT/Pt multilayer capacitor.

Fig.5.8 shows the *J-V* curves of the Pt/BFO/BNdT/Pt multilayer capacitor, and a leakage density of 2×10^{-9} A/cm⁻² with an applied voltage of 2 V is observed in the multilayer. Compared to the 3×10^{-7} A/cm⁻² leakage density of the Pt/BNdT/Pt capacitor, an improvement of nearly two orders of magnitude in *J-V* curves is obtained with the Pt/BFO/BNdT/Pt multilayer structure. The BNdT seeding layer induces the crystallization process of the BFO upper layer, and improves the degree of crystallization in the multilayer. A well-defined perovskite structure with less leakage paths will be desirable in many ferroelectric-based electrical applications.



Fig.5.8. Leakage density characteristic of Pt/BFO/BNdT/Pt multilayer and BNdT capacitors.

5.5.4 Magnetic enhancement

Magnetic hysteresis of the multilayer is measured using a vibrating sample magnetometer, as shown in Fig.5.9. It can be concluded that the multilayer exhibits a weak saturated ferromagnetic response at room temperature, and that the multilayers are anti-ferromagnetic. The highest saturation magnetization (M_s) is measured to be 2.47 emu/cm³, which is comparable to that of the BFO thin film reported by R. Y. Zheng, *et al.* [192]. The weak ferromagnetic behaviour can be explain by the existence of Fe²⁺ and the change in the canting angle of Fe³⁺ cations [3]. It can also be considered that the ferromagnetic behaviour is not highly affected by the coupling reaction between BFO and BNdT.



Fig.5.9 Magnetic hysteresis loop of the Pt/BFO/BNdT/Pt structure measured using a vibrating sample magnetometer.

5.6 Multilayer dielectric properties enhancement

Fig.5.10 shows the frequency dependence of both the dielectric constant ε_r and the loss tangent (tan δ) for the BFO/BNdT multilayer and BNdT thin film (200nm). The BNdT thin film exhibits a typical ε_r value of 535 at 100 kHz and it decreases slightly to 510 while the applied frequency increases from 100 kHz to 1 MHz, which is comparable with those values reported for highly c-axis oriented BNdT thin films [190]. The dielectric constant of the multilayer was about 373 at 100 kHz and deceases linearly to 362, with the increase of test frequency from 100 KHz to 1 MHz. Since the dielectric constant of the multilayer to that of BNdT, the average dielectric constant of the multilayer is relatively less than that of the BNdT alone.

It can also be seen from Fig.5.10 (b) that the typical value of tanδ is about 0.07 in the BNdT thin film measured at 100 KHz, and the value increases rapidly with frequencies above 1 MHz. However, the loss tangent of the multilayer was 0.05 at 100 kHz, relatively smaller than the BNdT value. Since the dielectric loss of BFO is in the range of 0.02-0.05

[79], the result seems to be reasonable. Compared to the BNdT thin film, it can be proposed that the BFO/BNdT multilayer may show better performance in high frequency applications. This difference in dielectric properties may be attributed to the coupling reaction between the two ferroelectrics, which adjusts the dielectric constant and optimizes the dielectric loss.



Fig.5.10 (a) Dielectric constant of the multilayer as a function of frequency (b) Loss tangent of the multilayer as a function of frequency.

5.7 Dual-site substitution fabrication

From this section on, we will discuss a different approach to improving the room temperature ferroelectric properties of the BFO material, namely, using dual-site substitution technology. Unlike the previous multilayer approach, where the aim was to improve the degree of crystallization in the BFO material, dual-site substitution technology intentionally introduces substitution atoms to the system and changes the BFO crystal structure correspondingly. Substituted atoms with different atomic radii will replace the Bi and Fe sites in the BFO crystal, distort the BFO crystal, and control the volatile nature of Bi and the suppression of oxygen vacancies.

Rare earth elements La, Nd, Nb, and Mn are introduced as the substitution elements. BFO crystals were substituted with 5 at. % ions (La, Nb, Nd, and Mn) with different chemical compositions. The stoichiometric BFO, Bi_{0.95}Nd_{0.05}Fe_{0.95}Nb_{0.05}O₃ (BNFNO), Bi_{0.95}Nd_{0.05}Fe_{0.95}Mn_{0.05}O₃ (BNFMO), and Bi_{0.95}La_{0.05}Fe_{0.95}Nb_{0.05}O₃ (BLFNO) are used in our experiment; the fabrication processes are the same as described in Section 5.3.2.

5.8 Dual-site substitution structural characterization

5.8.1 X-ray diffraction analysis

Fig.5.11 shows the X-ray diffraction patterns of the BFO, BNFNO, BNFMO, and BLFNO thin films. It can be seen that all of the XRD peaks can be indexed using a rhombohedral structure with some impurities and secondary phases. Merging and shifting of the diffraction peaks in the doped BFO thin films can be observed, indicating a structural transformation induced by substitution. In the pure BFO and BLFNO crystals, the (100) peak exhibits relatively larger intensity compared with the BNFNO and

BNFMO samples; the cause of this effect is that the La and Nb substitutions help enhance the crystallization of the BFO material in a c-axis preferred orientation. As found for the BNFNO crystal, diffraction peaks (104) and (110) in pure BFO crystal emerge and shift to a higher angle, describing a structural transformation. As reported in the literature, by changing the substitution concentration, the BFO structure will change from rhombohedral to tetragonal; this result is in agreement with what is seen in our experiment. Furthermore, impurities and secondary phases can be suppressed by using substitution. The intrinsic stability of La, Nd, Nb, and Mn atoms compared with the volatile nature of Bi contributes to this phenomenon, indicating that refined crystallization of BFO with less impurities and secondary phases can be achieved by modulating different ion substitutions. Further, since the chemical bond strengths of La, Nd, Nb, and Mn atoms with oxygen are not equal to that of the Bi-O bond, the crystallization temperature will vary compared to pure BFO [193]. This difference in bond strengths can be manipulated in order to study the substitution induced crystallization temperature variation of the BFO material.



Fig.5.11. XRD patterns of BFO, BNFNO, BNFMO, and BLFNO thin films.

5.8.2 Raman scattering analysis

Raman scattering spectra of BFO, BNFNO, BNFMO, and BLFNO thin films are shown in Fig.5.12. The peak position of each component, i.e., the natural frequency of each Raman active phonon mode, can be obtained by fitting the measured spectra and decomposing the fitted curves into individual Lorentzian components [193]. As reported in the literature, the Raman active phonon modes of the rhombohedral R3c BFO crystal can be given by the following irreducible representation $\Gamma=4A_1+9E$ [194-196], where A1 modes can only be observed in parallel polarization, but E modes can be found in both parallel and crossed polarizations [197]. As shown in Fig.5.12 (a), four A₁ modes and four E modes can be observed in our sol-gel derived BFO thin film. It can be seen that there are A_1^{-1} , A_1^{-2} , and A_1^{-3} modes with strong scattering intensities located at 140, 170, and 217 cm⁻¹, respectively, and an A_1^{-4} mode with relatively weak scattering intensity at 470 cm⁻¹. These results are comparable with those reported for PLD derived single crystalline BFO $(A_1^{-1}, A_1^{-2}, A_1^{-3} \text{ and } A_1^{-4}, \text{ at } 136, 168, 211, \text{ and } 425 \text{ cm}^{-1} \text{ respectively})$ [194,195]. The slight difference in Raman peak positions between reported results and our study is attributed to the oxygen stoichiometry and internal stress during the fabrication process. Also, four E modes with medium scattering intensity can be indexed at 90, 270, 368, and 539 cm⁻¹.

The substitution induced Raman peak shift and suppression is also investigated, as shown in Fig.5.12 (b). The Raman active phonon mode A_1^{-3} (~217 cm⁻¹) exhibits a positive shift after ion substitution, which is consistent with the result reported by A. Lahmar, *et al.* [198]. This scattering peak shift can be attributed to the stiffening of the A-O bond induced by the substituted ions with different atomic radii, resulting in a change

towards a more covalent type of bond. The A_1^{-1} mode, which corresponds to the Bi-O vibration at 140 cm⁻¹, exhibits the largest scattering intensity in the pure BFO crystal and is significantly suppressed in BNFNO, BNFMO, and BLFNO thin films. This difference occurs because the smaller Bi site substitutions change the length of the Bi-O bond and thus reduce the intensity of this band correspondingly. The Raman peak shift and suppression confirm that the crystal structure transformation due to substitution [193].



Fig.5.12 (a) Measured Raman scattering spectrum and decomposed Raman active phonon modes of the BFO thin film. (b) Comparison between the Raman spectra of BFO, BNFNO, BNFMO, and BLFNO thin films.

5.8.3 Electron microscope analysis

AFM surface morphologies of BFO, BNFNO, BNFMO, and BLFNO thin films are each examined and are shown in Fig.5.13 (a)-(d). Close-packed spherical grains and a smooth and uniform surface can be found in all of the samples. It is concluded that ion substitution plays a critical role in determining the grain size. The pure BFO exhibits a mean grain size of ~150 nm, whereas in the BNFMO and BLFNO thin films the mean grain size is reduced to ~50 nm. In the BNFNO crystal, the mean grain size is measured to be ~10 nm, only one fifteenth of the value for the pure BFO crystal. Since the grain size is a substantial contributing factor to the leakage properties, and crystals possessing small grain sizes always exhibit lower leakage current density, the ion substitution will help reduce the leakage current density and thus improve the ferroelectric properties [193], as will be discussed in the coming section.









Fig.5.13 AFM surface topography of BFO (a), BNFMO (b), BNFNO (c), and BLFNO (d) thin films.

5.9 Dual-site substitution ferroelectric properties characterization

5.9.1 Remanent polarization

Fig.5.14 shows the *P-E* hysteresis loops of the BFO, BNFNO, BNFMO, and BLFNO thin films. The pure BFO thin film exhibits a distorted hysteresis loop, indicating a large leakage current density. By substituting ions, a small remanent polarization is observed in the BNFNO, BNFMO, and BLFNO thin films, as shown in Fig.5.14 (b)-(d). It can be seen that none of the hysteresis loops are saturated, suggesting that the required saturation voltage of BNFNO, BNFMO, and BLFNO thin films is higher than the maximum output that our equipment can offer. However, an obvious improvement in ferroelectric properties can still be inferred from the *P-E* measurement, indicating the usefulness of ion substitution.





Fig.5.14 Ferroelectric hysteresis loops of BFO (a), BNFMO (b), BNFNO (c), and BLFNO (d) thin films. (Curves with different colours are obtained under different measurement voltages)

An additional interesting phenomenon is the dual-site substitution induced ferroelectric enhancement using La and Nd ions. As reported by S. K. Singh, *et al.* [39,41,42] and H. Uchida, *et al.* [80], the remnant polarization will be degraded in single-site doped BFO with La or Nd. The reason for such a decrease in remnant polarization is not yet fully understood, but degradation of crystal anisotropy and Curie temperature may be principle factors, as is the case with other pervoskite-based ferroelectrics, such as PZT and BTO. However, in our current study, the remnant polarization is increased in the dual-site doped BNFNO, BNFMO, and BLFNO thin films compared with pure BFO. The following represent possible reasons for the increase in remnant polarization: the interaction between different substituted ions, the variation in dual-site substitution induced Bi-O covalent bonds, and the involvement of stereochemical activity in the Bi lone electron pair.

5.9.2 Leakage properties

Leakage current density versus electrical field (J-V) curves for the BFO, BNFNO, BNFMO, and BLFNO thin films are shown in Fig5.15. It can be seen that the leakage density behaviour for different thin films depends on the substitution ion species. The pure BFO crystal exhibits the largest leakage current density, specifically 2.8×10^{-3} A/cm² at an applied electrical field of 0.1 MV/cm. This value is consistent with that reported by H. Uchida, et al. [80], indicating the low resistivity intrinsic to BFO at room temperature. The leakage density of the BNFMO thin film is measured to be 1.8×10^{-3} A/cm² at an applied electrical field of 0.1 MV/cm, exhibiting only a weak improvement compared with that of pure BFO crystal. As reported by S. K. Singha, et al. [41,42] and C. F. Chung, et al. [43], single-site substituted Mn and Nb ions in the form of BiFe_{1-x}Mn_xO and BiFe₁₋ _xNb_xO will increase the leakage current density due to chemical reactions during the fabrication process. However, in our experiment, dual-site substituted Mn and Nb ions provide only a weak improvement in the leakage properties, indicating the unique physical nature of dual-site substitution. A clear improvement in the leakage properties is achieved in BLFNO and BNFNO thin films. As illustrated in Fig.5.15, BLFNO shows a leakage of 1.2×10^{-4} A/cm² at an applied electrical field of 0.1 MV/cm, and BNFNO shows a leakage of 6.9×10^{-7} A/cm² at an applied electrical field of 0.1 MV/cm, four orders of magnitude lower than for pure BFO. Such abnormal leakage enhancement in dual-site substituted BFO thin films will offer more freedom of control in optimizing the electrical properties of modified BFO materials.

The improvement in leakage density when using ion substitution can be attributed to two factors. First, as explained above, the large current conduction in the pure BFO crystal is caused by charge defects induced by the Fe ions (Fe³⁺ and Fe²⁺) valence fluctuation and oxygen vacancies. With ion substitution, such defects tend to be reduced and thus better leakage properties can be obtained [193]. Another reason for the enhancement in leakage density is the improved crystallization in the ion substituted BFO. As shown with the AFM results, a smaller mean grain size is found in doped BFO thin films. Due to the inter-grain depletion described by the grain boundary limited conduction (GBLC) theory [199,200], the current density will be suppressed by local space charges near the grain boundaries, and the overlapping of depletion regions for neighbouring grain boundaries can cause the low leakage density.



Fig.5.15 Leakage current density-voltage (*J-V*) curves of BFO, BNFNO, BNFMO, and BLFNO thin films.

5.10 Conclusion

In this chapter, we have presented an investigation and optimization process for the ferroelectric properties of multiferroic BiFeO₃ (BFO). Two different optimization approaches were examined and studied in detailed. By introducing a 20 nm-thick BNdT

ferroelectric seeding layer, the structural and ferroelectric properties of BFO were significantly improved, and room temperature ferroelectric hysteresis loops with reasonable ferroelectric saturation were observed for the first time. This achievement can be attributed to the inducing effect introduced by using the BNdT seeding layer to the BFO upper layer. Many of the ferroelectric related properties, such as remanent polarization, fatigue endurance, CV/IV, dielectric properties, and magnetic properties were carefully studied and analyzed. Furthermore, we reported for the first time a dualsite substitution technology for the BFO material. By adding La, Nd, Nb, and Mn elements as the Fe-site and Bi-site substitutions, the volatile nature of the Bi and oxygen vacancies was reconciled, and the leakage properties and therefore the ferroelectric properties of BFO were optimized accordingly. Our work indicates that multilayer technology and dual-site substitution are two effective approaches for improving the room temperature performance of multiferroic BFO. With such technologies, BFO can be optimized to exhibit a low leakage current density and good ferroelectric properties; thus it may be a promising candidate in ferroelectrics-based applications.

Chapter 6

Ferroelectrics: Photovoltaic Effect and Theoretical Modeling

6.1 Introduction

ecently, the photovoltaic effect has been reported in single crystalline BFO with appreciable photoconductivity in the visible light region [21,22,44,201-203]. The observation of the photovoltaic effect expands the possible applications of BFO to new solar-related fields. In the photovoltaic domain, BFO exhibits unique properties compared to those of the traditional silicon-based solar cell. As reported in the literature [21,22], the built-in electrical field that separates the photo-generated carriers is about one order of magnitude higher than for silicon-based solar cells, due to the small direct band gap and narrow domain wall in the BFO material. Also, the output photo voltage of the BFO material can be tuned with an external electrical field, an effect which can be explained as follows: an external electric field larger than the coercive field can switch the ferroelectric domain in the BFO, flip the remanent polarization, and thus modulate the output photo voltage correspondingly [24,25,201,202]. Additionally, due to the multiferroic nature of BFO, more control mechanics including electricity, magnetism, heat, and stress can be employed to manipulate the photovoltaic performance of the BFO material and therefore can be used to provide solar cells with novel functionalities. However, most of the present studies are focused on experimental work and little attention has been paid thus far to proposing any theoretical or electrical models for describing the carrier mobility during the photovoltaic process. Furthermore, all of the past studies have been conducted using Indium tin oxide (ITO) and metals (Au and Pt) as top electrodes [45,46], without effort being spent in finding replacements for the traditional ITO material.

In this chapter, we introduce the graphene sheet as a replacement for ITO material, and we build a graphene/BFO/Pt photovoltaic heterostructure for the first time. An equivalent electrical and thermal model is first proposed to aid in the understanding of the transportation behaviour of the carriers. All important photovoltaic parameters are investigated both experimentally and theoretically. More specifically, Section 6.2 introduces the five-step fabrication process for the graphene/BFO/Pt heterojunction. Section 6.3 shows some basic performance characterizations of the BFO material and graphene top electrode. In Section 6.4, we start by constructing the band diagram, and then we establish an equivalent electrical model and calculate the theoretical photocurrent *J-V* curves. In Section 6.5, we provide a detailed photovoltaic characterization of the graphene/BFO/Pt heterojunction and using the theoretical model we investigate all photovoltaic parameters experimentally and theoretically. Finally, this chapter is summarized and concluded in Section 6.6.

6.2 Ferroelectric photovoltaic heterojunction fabrication

The fabrication process for the graphene/BFO/Pt photovoltaic heterojunction involves five basic steps, as illustrated schematically in Fig.6.1 (a) to (e). To begin with, a BFO precursor is prepared as discussed in the previous chapter. In the second step, a polycrystalline BFO thin film of 300 nm is deposited onto a Pt(180 nm)/Ti(20 nm)/SiO₂(300 nm)/Si(100) substrate using a sol-gel/spin coating process. Detailed fabrication processes can be found in the previous chapter. At the next step, a single layer polymethyl methacrylate (PMMA) thin film (~200 nm) with a circular window 3.5 mm in diameter is coated on top of the BFO thin film as an isolation layer. In the fourth step, a multilayer graphene sheet derived using an improved chemical vapor deposition (CVD) method and transferred by PMMA is employed as the transparent electrodes. Finally, silver paint is applied to the graphene film to make the contact for the electrical measurement. Our as-prepared unit is also integrated into a package with an optical window; a photograph of the as-packaged graphene/BFO/Pt photovoltaic heterojunction is presented in Fig.5.1 (f) [204].





Fig.6.1 Schematic illustration of the fabrication process. (a) Synthesis of the BFO precursor. (b) Deposition of the BFO crystal onto the Pt/Ti/SiO₂/Si substrate. (c) Transfer of the PMMA isolation film onto the as-prepared BFO crystal. (d) Transfer of the multilayer graphene sheet onto the PMMA isolation window. (e) Deposition of the electrode contact. (f) Photograph of the packaged graphene/BFO/Pt photovoltaic heterojunction.

6.3 Basic characterization

6.3.1 Graphene transparent electrode

Graphene is considered a promising candidate in the development of next generation photovoltaic devices due to its attractive optical and electrical properties [205-209]. With properties including a 2-dimensional (2D) atomic sheet structure, ballistic electronic transport, ultra-high carrier mobility, high conductivity and transparency, good mechanical strength, and flexibility, graphene has been the focus of a considerable number of research studies [210-214]. Further, in the absence of the contact resistance in CNT films caused by interconnected nanotube bundles, a continuous graphene sheet can exhibit high conductivity at ultra-low thicknesses (~atomic range) [213-215]. Several solar applications that use graphene as transparent/conductive electrodes have been investigated in depth, and exhibit interesting prospects for future application development [209,216-219]. Inspired by the unique optical properties of grapheme and its superiority in stability, transparency, and conductivity compared with ITO, we chose a graphene sheet as the transparent electrode in this BFO photovoltaic device.

A scanning electron microscope (SEM) image, shown in Fig.6.2, depicts the surface topography of the as-grown graphene sheet. A smooth and dense surface can be identified over a wide lateral scale. The Raman scattering spectrum, shown in Fig.6.2, reveals the multilayer nature of the as-prepared graphene sheet. The expected G and 2D bands with full width at half maximums (FWHM) of 16 and 34 cm⁻¹ can be indexed at the positions 1589 and 2685 cm⁻¹, respectively. Both peaks can be fitted using a single Lorentzian function that exhibits a symmetric and sharp shape. The distribution of the peak intensity ratio between the 2D and G bands, as shown with 2D micro-Raman mapping (Fig.2 (c)), further confirms the multilayer pattern, as well as the uniformity and consistency of the graphene film achieved. Furthermore, the negligible D band implies that the grapheme sheet obtained from this experiment is of high quality and is defect-free. As reported by S. Bae *et al.* [220], the transparency and the sheet resistance both decrease as the graphene sheet thickness increases, indicating a trade-off between transparency and resistance. In our experiment, a multilayer graphene sheet with much lower sheet resistance and slightly inferior transparency compared with those of a monolayer graphene film is

introduced as the transparent electrode, and this sheet exhibits optimized photovoltaic performance.



Fig.6.2 SEM top view morphology of the as-deposited graphene film.



Fig.6.3 (a) Raman spectrum of as-deposited graphene showing G and 2D peaks. 2D micro-Raman intensity mapping of (b) G band (1589 cm⁻¹) and (c) 2D band (2685 cm⁻¹). (d) 2D micro-Raman intensity ratio (I_{2D}/I_G) mapping from the same regions as (b) and (c).

A high optical transparency (~90%) of the as-prepared graphene sheet is seen from the UV-vis transmission spectrum shown in Fig.6.4. An optical quartz substrate is used to minimize the optical absorption in the UV range. Since the optical transmission of the monolayer graphene film is reported to be ~97% and it is usually degraded by ~2.2-2.3% for each additional graphene layer [221], our transmission result further confirms the multilayer nature of the graphene film obtained in this experiment.



Fig.6.4 UV-vis transmission spectrum of the as-prepared graphene sheet.

6.3.2 BFO characterization

In order to verify the ferroelectric performance of BFO in the graphene/BFO/Pt heterojunction structure, some basic structural characterizations are performed for the BFO thin film. Fig.6.5 (a) provides the X-ray diffraction (XRD) pattern of the asprepared BFO thin films, indicating polycrystalline behaviour without any preferred orientation. Most of the diffraction peaks, such as (110), (012), (024), and (112), can be indexed according to the standard powder diffraction data of the BiFeO₃ crystal; it is seen that a perovskite structure phase has been achieved [42,222]. The Raman scattering spectrum of the as-grown BFO crystal, shown in Fig.6.5 (b), is also investigated. In total, 11 Raman phonon modes, including 4 A_1^{-1} modes (141, 176, 220, and 475 cm⁻¹) and 7 E modes (88, 261, 286, 356, 443, 533, and 620 cm⁻¹), can be achieved by fitting the spectrum into individual Lorentzian components. Since all of the active modes can be given by the irreducible representation Γ =4 A_1 +9E [194-196], a rhombohedrally distorted ferroelectric perovskite with the *R3c* space group has been achieved in the BFO crystal prepared in this experiment. Therefore, it can be concluded that the graphene sheet does not impact the crystallization process of the BFO material. We will further examine the effect of the graphene sheet on the photovoltaic parameters in the coming sections.




Fig.6.5 (a) XRD patterns of the BFO crystal achieved in the experiment. (b) Measured Raman scattering spectrum and decomposed Raman active modes of the as-prepared BFO thin film.

6.4 Theoretical modeling

6.4.1 Band diagram construction

In order to understand the carriers transport behaviour in the graphene/BFO/Pt photovoltaic heterojunction, the band diagram of the heterojunction must first be constructed. To construct the band diagram, the work functions (Φ) of graphene and Pt are taken as 4.8 and 5.6 eV, respectively [215]. The electron affinity (χ) of BFO is estimated at 3.3 eV [223]. Since the band gap energy (E_g) of ferroelectrics exhibits a strong dependence on the fabrication procedure, the E_g value of BFO utilized in this experiment should be determined from the transmission spectrum using the Tauc relationship [170].

To obtain the band gap energy of BFO, an optical graded quartz substrate is employed, and the UV-vis transmission spectrum of the BFO thin film in the wavelength range from 250 to 800 nm is measured, as shown in Fig.6.6 (a). For wavelengths of incident light longer than 550 nm, BFO exhibits high transparency of >80%, indicating a weak optical absorption. Since the transmittance *T* varies exponentially with the absorption coefficient α in a high absorption region, the α -value can then be determined from the following equation:

$$\alpha = -(\ln T) / d \tag{6.1}$$

where *d* is the thickness of the BFO thin film (~300 nm). Further, as a direct band gap material, the absorption coefficient α and band gap energy E_g can be related through the Tauc relationship: [170]

$$\alpha = \sqrt{C(h\nu - E_g)} / h\nu, \qquad (6.2)$$

where hv is the photon energy and *C* is a constant. The E_g value can then be extracted from the graph of $(\alpha hv)^2$ versus hv by extrapolating the linear portion of the curve to $(\alpha hv)^2 = 0$, as shown in Fig.6.6 (b). In this way, the E_g value of the BFO achieved in this work is calculated to be 2.9 eV.





Fig.6.6 (a) Optical transmittance of the as-grown BFO crystal. (b) Photon energy dependence of the optical absorption coefficient in the as-prepared BFO thin film.

Given the values listed above, we can construct the band diagram. When BFO and graphene or Pt are joined together, two Schottky barriers will be formed and the barriers at both interfaces will inhibit the Schottky emission, forming two built-in electrical fields in opposite directions. This band diagram, which is simulated in the next section, is referred to as the "virgin state", where two Schottky junctions serve as back-to-back diodes and no current can be measured regardless of the polarity of the applied electrical field. However, as reported by C. Wang and C. Ge, *et al.* [224,225], the ferroelectric remanent polarization P_r caused by an external electrical field will charge the neutral oxygen vacancy. The released electrons, along with the depolarization field and interface states, will form a narrow positive/negative charged region near the interface, resulting in an "upward/downward band bending" at the graphene/BFO and BFO/Pt interfaces.

More specifically, when BFO and graphene or Pt are joined, two Schottky barriers will be formed with two built-in fields in opposite directions [204]. The two interface

junctions are both depleted. The width of the depletion region (x_{dc}) can be given as follows:

$$x_{dc} = \sqrt{\frac{2\varepsilon_0 \varepsilon_s V_s}{q N_D}},\tag{6.3}$$

where, ε_0 is the vacuum permittivity, ε_s is the relative dielectric constant of the BFO material, N_D is the carrier density, and V_s is the surface potential defined as:

$$V_S = V_{x=surface} - V_{x=x_{dc}}, ag{6.4}$$

which can be used to describe the potential barrier difference between the surface and body, and represents the band bending.

By calculating the widths of the depletion regions at both the graphene/BFO and BFO/Pt sides, it can be found that the entire width of the two depletion regions (~ 500 nm) is larger than the BFO thickness (~300 nm) in this experiment. Therefore, the entire BFO thin film is depleted across the top and bottom electrodes without any neutral region.

Thus, the modified Poisson Equation can be applied at both interfaces of graphene/BFO and BFO/Pt [204]:

$$\nabla^2 V(x, y, z) = -\frac{1}{\varepsilon_0 \varepsilon_s} (\rho(x, y, z) - \nabla \cdot P_r(x, y, z))$$
(6.5)

where V(x, y, z) is the voltage potential, $\rho(x, y, z)$ is the charge density, $P_r(x, y, z)$ is the ferroelectric remnant polarization, ε_0 is the vacuum permittivity, and ε_s is the relative dielectric constant of BFO.

To simplify the calculation we examine the one-dimensional case, for which Eq. (6.5) is written as follows:

$$\frac{d^2 V(x)}{dx^2} = -\frac{1}{\varepsilon_0 \varepsilon_s} \left(\rho(x) - \frac{dP_r(x)}{dx}\right). \tag{6.6}$$

Further, $\rho(x)$ can be determined from:

$$\rho(x) = q[p_D(x) + p(x) - n_A(x) - n(x)], \qquad (6.7)$$

where n(x) and p(x) are the electron and hole density, respectively; and $n_A(x)$ and $p_D(x)$ are the ionized donor and acceptor density, respectively. Here, we can assume that electrons and holes can be described by the Fermi Distribution:

$$n(x) = n_0 e^{qV(x)/K_B T} p(x) = p_0 e^{-qV(x)/K_B T}$$
(6.8)

where n_0 and P_0 are the electron and hole density, respectively, at thermal equilibrium. Also, $n_0 \approx N_D$, and K_B is the Boltzmann constant.

When the electro neutrality condition $q[p_D + p_0 - n_A - n_0] = 0$ is met, then

$$p_D - n_A = n_0 - p_0. ag{6.9}$$

For completeness, it is noted that:

$$\frac{qV(x)}{K_BT} = u(x). \tag{6.10}$$

Therefore, Eq. (6.7) can be rewritten as follows:

$$\rho(x) = q[p_0(e^{-u} - 1) - n_0(e^u - 1)].$$
(6.11)

For BFO, $n_0 >> p_0$, therefore Eq. (6.9) can be simplified as

$$\rho(x) = -qn_0(e^u - 1). \tag{6.12}$$

 $P_r(x)$ can be calculated by

$$P_r(x) = \frac{P_{r\max}}{E_{c\max}} E_c(x), \qquad (6.13)$$

where $P_{r\max}$ and $E_{c\max}$ represent the remnant polarization and the coercive field in the saturated polarization-electric field (*P-E*) hysteresis loop, respectively, and E_C is the electric field.

Therefore, Eq. (6.6) can be given as,

$$\frac{d^2 V(x)}{dx^2} = \frac{1}{\varepsilon_0 \varepsilon_s} [q n_0 (e^u - 1) + \frac{dP_r(x)}{dx}],$$
(6.12)

Then using Taylor expansion,

$$e^{u} - 1 = u + \frac{u^{2}}{2} + \dots + \frac{u^{n}}{n!} + \dots$$
,

we can subsequently solve Eq.(6.11).

In a one-dimensional scenario, by taking the interface state into account, the boundary conditions during the derivation process can be expressed as:

$$V(0) = V_{sGS-BFO} = \Phi_{GS} - \Phi_{BFO}$$
(6.13)

$$V(L) = V_{sBFO-Pt} = \Phi_{BFO} - \Phi_{Pt},$$
(6.14)

where L is the thickness of the BFO thin film, and $V_{sGS-BFO}$ and $V_{sBFO-Pt}$ are the surface potentials at graphene/BFO and BFO/Pt, respectively.

By applying these boundary conditions, three possible energy band diagrams of the graphene/BFO/Pt heterojunction can be simulated using MATLAB[®]; these are given in Fig.6.7 (a)-(c), where a switchable diode in series with a variable resistance is used in the theoretical model of the graphene/BFO/Pt heterojunction.

Virgin states



Fig.6.7 (a) Depletion regions are formed on both sides. Such a band diagram is equivalent to two back-to-back diodes, and no current will be observed regardless of whether the applied voltage is positive or negative.



Upward bending

Fig.6.7 (b) Electrons are accumulated at the graphene/BFO side and can be regarded as a variable resistance. The BFO/Pt side is depleted and can be treated as a Schottky diode.



Downward bending

Fig.6.7 (c) Electrons are accumulated at the BFO/Pt side and can be regarded as a variable resistance. The graphene/BFO side is depleted and can be treated as a Schottky diode.

6.4.2 Theoretical *J-V* model

As explained above, interface trapped charges and a high enough electric field will switch the ferroelectric polarization in the BFO thin film and stimulate neutral oxygen vacancies to release electrons, forming a narrow electron region near the interface and resulting in energy band bending.

When a positive electrode is connected to the Pt electrode, a depletion region will be formed at the BFO/Pt side, as shown in Fig.6.7 (b).

When the diffusion model dominates, the current density can be written as:

$$j = q \mu_n E N_C e^{-\frac{q \Phi_B}{K_B T}} (e^{\frac{q V_F}{K_B T}} - 1), \qquad (6.15)$$

where μ_n is the electron mobility, $N_C = 2(\frac{m_{dn}K_BT}{2\pi\hbar^2})^{3/2}$ is equivalent density of states at

the bottom of conduction band, m_{dn} is the effective mass of an electron, Φ_B is the built-in

potential, and V_F is the junction bias. Also, *E* is the electrical field of the space charge region, and can be defined as:

$$E = \sqrt{\frac{2qN_D(\phi_i - V_F)}{\varepsilon_0 \varepsilon_s}}, \qquad (6.16)$$

where $\phi_i = (E_{C_{x=surf}} - E_{C_{x=x_{dc}}}) / q$ represents the band bending.

When the thermal emission model dominates, the current density can be written as:

$$j = A^* T^2 e^{-\frac{q\Phi_B}{K_B T}} (e^{\frac{qV_F}{K_B T}} - 1), \qquad (6.17)$$

where $A^* = 4\pi q m_{dn} K_B^2 / h^3$ is the Richardson constant.

In our experiment, the BFO thin film is prepared using the sol-gel process, and thus the two models described above should both be taken into account. The optimized current density can be described as:

$$j = \frac{q \overline{v} N_{V}}{4 + \frac{\overline{v}}{v_{D}}} e^{-\frac{q \Phi_{B}}{K_{B} T}} (e^{\frac{q V_{F}}{K_{B} T}} - 1),$$
(6.18)

where V_F is the junction bias, $\overline{v} = \left(\frac{8K_BT}{\pi m_p}\right)^{\frac{1}{2}}$ is the average thermal velocity, N_C is the equivalent density of states, Φ_B is the built-in potential, $v_D = \mu nE = \mu n \left(\frac{2qN_D(\phi_i - V_F)}{\varepsilon_0 \varepsilon_s}\right)^{\frac{1}{2}}$ is the carrier drift velocity, and $\phi_i = (E_{Cx=surf} - E_{Cx=x_{dc}})/q$ represents the band bending with x_{dc} as the junction width.

6.4.3 Equivalent electrical model construction

Electrons are accumulated at the graphene/BFO side and can be modeled as a variable resistance,

$$\sigma = qp\mu_p + qn\mu_n \approx qn\mu_n, \tag{6.19}$$

which can be regarded as constant. In fact, the width of the depletion region will change with different external applied voltages, and the resistance will vary as follows:

$$R = \frac{1}{\sigma} (L - x_{dc}) \,. \tag{6.20}$$

Vice versa, when the positive electrode is connected to the graphene electrode, a depletion region will be formed at the graphene/BFO side, as shown in Fig.6.7 (c), and a similar analysis to above can be applied.

The equivalent electrical model is obtained based on this analysis. The corresponding circuit diagram is shown in Fig.6.8.



Fig.6.8 Equivalent electrical model of the graphene/BFO/Pt heterojunction.

In Fig.6.8, S_1 and S_2 are the Schottky barrier diodes, R_{s1} and R_{s2} are the variable resistances, R_{c1} and R_{c2} are the contact resistances of BFO with the graphene and Pt electrodes, R is the edge resistance caused by imperfect factors, and C_1 to C_4 are the junction capacitances. J_{p1} and J_{p2} are introduced to characterize the photocurrent term upon illumination.

According to this electrical model, the short circuit current should be zero without illumination. However, interface trapped charges offer a weak ferroelectric polarization δ at the interface, leading to a weak band bending and a sub on-state of the diode even at zero bias, resulting in a non-zero dark current. Therefore, a voltage source V_{sub} is added to characterize the *I-V* curve offset at zero bias.

Moreover, the electrical model should be dynamic and flexible for use in a practical application. The parameters of diodes S_1 and S_2 , such as the width of depletion region, potential barrier height, and so forth, will vary with different applied voltages. In order to simplify our model, the parameters of S_1 and S_2 are set using an approximation, and a current supply J_R is introduced to describe such circuit parameter induced current variation and leakage terms in the heterojunction.

The modified equivalent electrical model is given in Fig.6.9. This equivalent electrical model, along with the band diagram model, will be applied to characterize the electrical and optical properties of the graphene/BFO/Pt photovoltaic heterojunction in the coming sections.



Fig.6.9. Modified equivalent electrical model of the graphene/BFO/Pt heterojunction.

6.5 Photovoltaic characterization

6.5.1 Dark current properties

The dark current density of the graphene/BFO/Pt heterojunction is measured and plotted in Fig.6.10. A simulated dark current density derived from the equivalent electrical model and from Eq.(6.18) is also presented, and is in good agreement with the experimental result. As shown in Fig.6.10, the dark current exhibits a substantial current density of 2.3 μ A/cm² at zero bias; this current density can be characterized by the voltage source V_{sub} in the electrical model. The non-zero short circuit dark current can be attributed to the remanent ferroelectric polarization δ at the interface. As explained above, an external electrical field will polarize the ferroelectric material BFO, trapping some charge at the interface, leading to a "bending" of the heterojunction band diagram and a sub on-state of the diodes (S_1 and S_2) shown in the electrical model, resulting in the non-zero dark current [204].



Fig.6.10 Measured and simulated dark/photo current density of the graphene/BFO/Pt photovoltaic heterojunction with external voltage ranging from -1 to 1 V (a) and -3 to 3 V (b).

6.5.2 Photovoltaic performance characterization

A significant increase in photocurrent can be observed by applying illumination $(100 \text{mW/cm}^2, \text{AM 1.5})$ to the graphene/BFO/Pt photovoltaic heterojunction. As shown in Fig.6.10, the short circuit current density (J_{sc}) and open circuit voltage (V_{oc}) are measured to be 61 μ A/cm² and 0.52 V, respectively. The open circuit voltage is much higher than for the PLD derived highly (00*l*) orientated BFO crystal (~40 mV) reported by T. L. Qu,

et al. [46], and the sol-gel fabricated polycrystalline BFO (~0.08 V) with an ITO electrode [45]. This obvious improvement in photovoltaic performance can be attributed to the superior properties of graphene compared to the traditional ITO electrode. First, the optical transparency of the graphene sheet is higher than for ITO [220], allowing more light to pass through the transparent electrode. Second, the flexible nature of the graphene sheet provides a better electrical contact with the BFO crystal, reducing the contact resistance and resulting in better photovoltaic performance. Third, the theoretical carrier mobility of graphene is much higher than for the ITO material, and an experimental result of ~7×10⁴ cm²/V·s was recently reported using single crystal PZT as the substrate [226]. The weak power conversion efficiency, which can be attributed to the relatively large band gap of the BFO material, is found to be ~8.0×10⁻³%. This result is comparable with the value (~3×10⁻³%) reported by T. Choi *et al.* [21], and is larger than that of ~7×10⁻⁴% reported by W. Ji *et al.* [44].

To obtain the theoretical photocurrent density upon illumination, Eq. (6.18) is rewritten as follows:

$$I = I_L - I_F = A_E j_L - A_T j_{dk}(V), (6.21)$$

where
$$j_L = q \int_0^\infty \int_0^{x_{dc}} \beta \Phi_0(\lambda) [1 - \rho(\lambda)] \alpha e^{-\alpha x} dx d\lambda$$
, (6.22)

 A_{E} is the illumination area, A_{T} is the cell area, j_{L} is the photocurrent density, j_{dk} is the dark current density, β is the generation coefficient, Φ_{0} is the intensity of photons at wavelength λ , ρ is the reflectance, and α is the absorption coefficient. Using Eq. (6.21)-(6.22), the simulated light photocurrent density is plotted and compared with the experimental result, as shown in Fig.6.10. This comparison indicates a good consistency in results. It is concluded from both simulated and experimental curves that the

photocurrent density is not symmetric with applied voltage, that is, the forward portion exhibits faster growth rate under an applied voltage than does the reversed segment. This discrepancy is explained by the difference in potential barrier heights at the two interfaces. Since the photo generated carriers are separated by the built-in electrical field at the interface, the height of the Schottky barrier plays a critical role in determining the photocurrent density. Upon forward bias, when a positive voltage is applied to the Pt substrate, the Schottky junction on the BFO/Pt side is equivalent to a Schottky diode which promotes the photocurrent; the Schottky junction on the graphene/BFO side can be regarded as a resistance. The functionality of these two Schottky junctions will be switched upon reverse bias. Since the potential barrier is much higher on the BFO/Pt side (2.7 eV) compared to the graphene/BFO interface (1.9 eV), a stronger built-in electrical field and thus faster growth rate can be observed upon forward bias compared with the reversed bias [104].

6.5.3 Illumination intensity dependence

The short circuit photocurrent of the graphene/BFO/Pt heterojunction for incident light intensities from 0.8 AM to 1.4 AM is also measured and presented in Fig.6.11 (a). It can be seen that J_{sc} varies proportionally with incident light intensity, which is consistent with the increase in light-induced photo carriers upon an increase in light intensity.

To further confirm the photoconductivity variation under different illumination intensities, conductive AFM (CAFM) is used to examine the local current behaviour and leakage path distribution on a microscopic level. Equipped with a conductive tip, CAFM is considered an effective method for investigating the local conductivity of dielectric materials. During the CAFM measurement, a DC bias of 1 V is applied to the BFO thin film through a Pt-Cr coated silicon tip (tip apex ~15 nm), and the point current is acquired simultaneously when the AFM works in tapping mode (TM). The current sensitivity is set at 3 nA in this experiment. A photocurrent distribution map within an area of 5×5 um² is presented for different illumination intensities in Fig.6.11 (b)-(f). The bright region indicates high conductivity, while the dark region implies good dielectric properties between the probe and the BFO substrate. All of the images are obtained from the same surface area; the slight mismatch is caused by thermal drift during the measurement. It can be seen that the conductivity and the charge transportation paths exhibit a random distribution and increase significantly when the illumination intensity increases from 0.8 to 1.4 AM, which is consistent with the macro J-V curves measurement shown in Fig.6.11 (a). The high resolution of the CAFM measurement is determined by the small tip dimension; however, the sharp shape of the tip may also cause an enhanced electric field between the tip and sample substrate and this effect can explain the "over bright" region in the CAFM measurement.





Fig.6.11 Photocurrent density vs. incident light intensity (a). In situ conductive AFM (CAFM) measurement of micro photocurrent distribution when incident light is 0.8 AM (b), 0.9 AM (c), 1.0 AM (d), 1.2 AM (e) and 1.4 AM (f).

6.5.4 Time dependence

Figure 6.12 (a) shows the photocurrent variation over time of the graphene/BFO/Pt photovoltaic heterojunction under AM 1.5 illumination intensity at zero bias. A stable

ON/OFF ratio confirms the repeatability in photovoltaic performance and illustrates the feasibility for use in practical applications. Moreover, it can be calculated from Fig.6.12(b)-(c) that the 10% to 90% relaxation times, namely, the rise time from OFF to ON state and the fall time from ON to OFF state, are small (0.06 s and 0.07 s, respectively), indicating an instantaneous response to illumination. Such photovoltaic properties suggest that the graphene/BFO/Pt photovoltaic heterojunction can be applied as a photosensitive detector; this will be described in the following discussion.



Fig.6.12 (a) Photocurrent vs. illumination time in the graphene/BFO/Pt photovoltaic heterojunction, zoomed-in versions provided for calculating (b) rise time and (c) fall time.

6.5.5 Minority carrier lifetime

The lifetime of photo-generated excess minority carriers is a crucial parameter in solar related designs, since it governs the carrier diffusion length (*L*) and thus the overall collection efficiency in such an application. A common practice, the photoconductivity decay method (μ -PCD), is employed and the decay of excess carriers excited by the pulsed light (200 ns in width) is examined using microwaves. A minority carrier lifetime distribution map within an area of 1.5×2.5 cm², and a corresponding histogram, are presented in Fig.6.13 (a)-(b). It is seen that the minority carrier lifetime has a random distribution pattern from 23 µs to 53 µs and a weighted average lifetime of 42.2 µs, which is larger than that of regular silicon material. The random distribution of the minority carrier lifetime to the BFO material achieved in this experiment, and the relatively large value indicates that the BFO material has the potential to provide a large carrier diffusion length and sound conversion efficiency.



Fig.6.13 Minority carrier lifetime mapping of the BFO crystal in a region of 1.5×2.5 cm² (a) and the corresponding distribution histogram (b).

6.5.6 External quantum efficiency

External quantum efficiency (EQE), an important parameter that quantitatively defines the conversion percentage of an incident photon into an electron-hole pair, is also investigated and plotted in Fig.6.14. The photo conversion efficiency of the graphene/BFO/Pt photovoltaic heterojunction over a wavelength range from 250 to 900 nm is presented. It shows a maximum harvest efficiency of 1.42% around 417 nm, corresponding to the band gap energy of the BFO material calculated above. The low EQE in other wavelength regions can be attributed to the poor excitons stimulation/dissociation and material absorption. As for most photographic films, the BFO thin film has EQE values of much less than 10%, indicating weak conversion efficiency.



Fig.6.14. External quantum efficiency (EQE) measurement of the graphene/BFO/Pt photovoltaic heterojunction.

6.5.7 Thermal modulation effect

Thermal properties, such as pyroelectricity, are of great interest in ferroelectrics. For this reason, we also study the impact of temperature on the photovoltaic properties of BFO. Due to the thermal stability issue with graphene sheets, carbon nanotubes (CNT) are employed to replace the graphene sheet as the transparent electrode. Since CNT possesses a work function of 4.8 eV, which is the same as that of the graphene sheet, and the two have similar electrical properties, this replacement will not change the band diagram structure of the photovoltaic heterojunction. All of the obtained theoretical models still apply in the new device structure [227].

Fig.6.15 (a) shows the comparison between *J-V* curves at different temperatures. It can be seen that J_{sc} increases from 2.2 to 3.3 μ A/cm², and V_{oc} decreases from 0.47 to 0.33 V, as the temperature increases from 313 to 363 K. A 3D curve, shown in Fig.6.15 (b), presents a clear depiction of this temperature dependence of *J-V*. To explain this thermal impact on the photovoltaic effect, Eq. (6.18) can be rewritten as:

$$j = A^* T^2 e^{-\frac{q\Phi_B}{K_B T}} (e^{\frac{q(V_F - V_{sub})}{K_B T}} - 1) - j_R \sim A^* T^2 e^{-\frac{q\Phi_B}{K_B T}} e^{\frac{q(V_F - V_{sub})}{K_B T}} - j_R,$$
(6.23)

where thermionic emissions dominate the current density, and A^* is the Richardson constant.

The short circuit current under heating can be obtained as:

$$j_{sc} = A^* T^2 e^{\frac{-q\Phi_B}{K_B T}} e^{\frac{-qV_{sub}}{K_B T}} - j_R .$$
(6.24)

To calculate the open circuit voltage (V_{oc}) ,

$$j_{sc} = A^* T^2 e^{-\frac{q \Phi_B}{K_B T}} e^{\frac{q (V_{oc} - V_{sub})}{K_B T}} - j_R = 0.$$
(6.25)

Therefore, Voc can be approximated as follows [227]:

$$V_{oc} = \frac{K_B T}{q} (\ln j_R - \ln A^* - 2\ln T) + V_{sub} + \Phi_B; \qquad (6.26)$$

and since $ln j_R - ln A^* - 2 ln T < 0$, V_{oc} decreases as T increases in the low temperature region.

It can be concluded from the above calculation that as the temperature increases the photocurrent increases correspondingly, resulting in a larger voltage drop over the resistance and thus less bias applied to the junction [227]. Such a temperature dependent junction bias is also illustrated in Fig.6.15 (c). Incorporating the junction bias variation into Eq. (6.4), the theoretical temperature dependence of the photocurrent density under different applied voltages is plotted in the inset of Fig.6.15 (d) and exhibits a reasonable consistency with the experiment, as shown in Fig.6.15 (b). Such agreement in the thermal effect analysis further confirms the validity of the model achieved in our work.





Fig.6.15. (a) J-V curves for different temperatures (313 to 373 K). (b) A 3D view of the temperature/voltage dependence of the photocurrent density. (c) Simulated temperature dependence of the junction bias. (d) Temperature dependence of the photocurrent density under different applied voltages (-1 to 1 V); in the bottom left inset is the simulated temperature dependence of J-V.

6.6 Conclusion

Research on the photovoltaic effect of multiferroic BFO is a new hot spot in the ferroelectric field. In this chapter, we demonstrated an enhancement in the photovoltaic performance of a polycrystalline BFO thin film with graphene as the top electrode. The short circuit current density (J_{sc}) and open circuit voltage (V_{oc}) of the heterojunction were measured to be 61 μ A/cm² and 0.52 V, respectively, values which are much higher than those reported for polycrystalline BFO with indium tin oxide (ITO) as the top electrode. A theoretical band diagram model and an equivalent electrical model, considering the ferroelectric polarization, interface states, and energy band bending effect, were constructed to describe the carrier transportation behaviour. A detailed photovoltaic characterization of the graphene/BFO/Pt heterojunction was performed. Different photovoltaic parameters, including dark/light properties, illumination intensity dependence, time dependence, minority carrier lifetime, external quantum efficiency, and

the thermal modulation effect, were investigated experimentally and theoretically. Our work indicates that by introducing graphene as a replacement for the ITO material, the photovoltaic performance of BFO has been improved significantly, making the graphene/polycrystalline BFO/Pt heterojunction a promising candidate for next generation photovoltaic-related applications.

Chapter 7

Photovoltaic Performance Enhancement and Applications

7.1 Introduction

In the previous chapter, we examined photovoltaic-related parameters of the graphene/BFO/Pt photovoltaic heterojunction, and demonstrated the promising properties and performance of BFO. In this chapter, we will further our research on enhancing the performance and photovoltaic applications. Although the graphene/BFO/Pt photovoltaic heterojunction demonstrates superior properties compared with such devices reported in the literature, there is still considerable work to be done in optimizing it before it can be applied commercially. Two different enhancement routines, namely, a chemical routine and a physical routine, will be demonstrated in this chapter, we will further our research by attempting to develop two interesting applications based on our graphene/BFO/Pt photovoltaic heterojunction. More specifically, Section 7.2.1 discusses HNO₃ treatment and the corresponding photovoltaic enhancement of the graphene/BFO/Pt, with comparison between experimental results and theoretical

calculations. Section 7.2.2 provides a study on the improvement obtained using the physical routine. The quantum dots (QDs) sensitization process will be examined and explained, and three different natural mechanisms will be illustrated. In Section 7.2.3, a comparison between the chemical approach and the physical routine will be provided, and the appropriate enhancement method will be demonstrated in a real application. In Section 7.3, we will apply our graphene/BFO/Pt photovoltaic heterojunction in the optical and electrical fields by building and demonstrating the functionality of both a photo detector and a tunable switch. Finally, this chapter is summarized and concluded in Section 7.4.

7.2 Performance enhancement

To improve the photovoltaic performance of the graphene/BFO/Pt heterojunction, chemical treatment and physical filling/sensitizing are employed as two independent, effective methods. The application of these techniques will be discussed in detail in the following subsections.

7.2.1 Chemical enhancement

We perform the chemical treatment by immersing the graphene/BFO/Pt cell in 65% HNO₃ vapor for various time durations (1-10 min). Significant short circuit photocurrent increases can be observed with different HNO₃ treatment times, namely from 61 μ A/cm² to 8.67 mA/cm² (~150 fold) after HNO₃ treatment for 8 min, with the current staying constant at immersion times above this, as shown in Fig.7.1. A comparison between *J-V*

curves before and after HNO₃ treatment is also presented, as shown in Fig.7.2, indicating no significant variation in the shape of the J-V curves following the HNO₃ treatment.



Fig.7.1 Photocurrent density vs. HNO₃ treatment time.



Fig.7.2 Comparison of photocurrent density before treatment and after treatment of different durations.

This unexpected enhancement in photocurrent can be attributed to three factors. The first and principal factor is the variation in the graphene work function ($\Delta \Phi_{GS}$) induced by HNO₃. S. Bae *et al.* reported that the graphene work function decreases by 0.1 eV

during HNO₃ treatment [220]. As discussed in Section 6.4, the photocurrent density term is proportional to $e^{-q\Phi_B/K_BT}$, as indicated in the calculation below. The current density ratio with and without HNO₃ treatment is expressed as:

$$j_{after} / j_{before} \sim e^{-q\Delta\Phi_B/K_BT} \sim 144;$$
(7.1)

which exhibits a good agreement with our experimental results. Second, the sheet resistance of the graphene top electrode can also be affected by HNO₃ treatment. As explained by S. Bae *et al.* [220], the electrons in the graphene sheet can be withdrawn due to the strong oxidation property of HNO₃ and the graphene sheet can thus be regarded as p-doped during the HNO₃ treatment. The p-doping during the redox process will increase the carrier concentration in the graphene sheet can reduce the sheet resistance according to the following expression:

$$\rho = \frac{1}{e(n\mu_n + p\mu_p)},\tag{7.2}$$

where ρ is the resistivity and μ is the mobility of the graphene sheet. The graphene sheet resistance for different HNO₃ treatment times is shown in Fig.7.3, and is in agreement with our analysis [204,228]. The third factor in the photocurrent enhancement is that the impurities and remanent graphene/BFO interface state can also be removed during the redox process thus improving the electrical properties of the contact [208].



Fig.7.3 Graphene sheet resistance for different HNO₃ treatment times.

7.2.2 Physical enhancement

On the other hand, we perform the physical filling routine by dipping CdSe QDs (2.5 mg/mL, exciton peak at 530 nm) in the graphene/BFO/Pt heterojunction. A high resolution TEM image, shown in Fig.7.4, demonstrates the random distribution of the CdSe QDs nanocrystallite. The inset of Fig.7.4 provides a colour photograph of the CdSe QDs solution. The short circuit photocurrent demonstrate a ~5 fold increase, namely from $61 \,\mu\text{A/cm}^2$ to 0.32 mA/cm², after CdSe QDs filling, as presented in Fig.7.5.



Fig.7.4 High resolution TEM image of CdSe QDs, exhibiting a random nanocrystallite distribution; the inset is a colour photograph of the CdSe QDs solution.



Fig.7.5. Photocurrent density variation before and after QDs filling/sensitizing.

Unlike the variation in the graphene work function caused by the chemical treatment, the photovoltaic improvement seen here can be attributed to the enhancement in the photon absorption and exciton transfer process. Since the CdSe QDs possess a small band gap (~ 1.70 eV) [229] and wide absorption band, the introduction of CdSe QDs to graphene/BFO/Pt will help absorb photons with energy less than the BFO band gap. The usage of CdSe QDs is therefore equivalent to adding an intermediate energy level to the graphene/BFO/Pt heterojunction band diagram and helps to harvest the incident photons with lower energy, and enlarge the absorption band of the BFO material, as illustrated in Fig.7.6.



Fig.7.6 BFO absorption variation before and after QDs sensitization.

As an electron supplier and transporter, QDs can provide an ultra-high electron injection rate of $\sim 10^{10}$ s⁻¹ into the BFO crystal [230], and correspondingly the holes are scavenged by a redox coupling process, as depicted schematically in Fig.7.7. Such a high exciton transportation rate will minimize the possibility of recombination and thus increase the photovoltaic performance. On the other hand, the graphene electrode with a large surface area, high aspect ratio, and high carrier mobility, also plays a role as an electron donor to the QDs in the carrier transportation and collection process. Furthermore, a multiple exciton generation (MEG) effect reported in QDs can also contribute to this photovoltaic enhancement [231,232]. With QDs, more than one electron-hole pair can be stimulated by one "high energy" incident photon [233,234], resulting in conversion quantum efficiency greater than 100%. As reported by R. J. Ellingson and R. D. Schaller *et al.* [232,235], three electron-hole pairs can be stimulated by a photon for which the energy is four times that of the QDs band gap, and the number of excitons can reach up to seven if the photon energy increases to eight times that of the

QDs band gap. Such unique properties of QDs can redouble the photo generated carriers under the same illumination and thus increases the conversion efficiency in an application.



Fig.7.7 Schematic illustration of the redox and electron transfer process with QDs filling/sensitizing.

7.2.3 Comparison of chemical and physical enhancements

The chemical and physical routines both have their advantages and drawbacks in terms of improving the photovoltaic performance of the graphene/BFO/Pt heterojunction. Both routines are easy to implement and can provide obvious enhancement in the photocurrent. HNO₃ treatment is economical and can offer a large improvement in photocurrent (~150 fold); however, the strong oxidizability may damage not only the graphene electrode but also the adjacent electrical components in an integrated application. On the other hand, due to the redox nature of the chemical treatment, the improved photocurrent could degrade over long-term operation, resulting in instability in an application. The method using inorganic QDs filling/sensitizing is damage-free to the solar cell and can provide long-term functionality and stability. Also, as an "artificial atom", the band gap of the

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QDs can be modulated by tuning the QDs size, providing more flexibility for optimization and compatibility. Nevertheless, QDs are expensive and the photovoltaic performance is not greatly enhanced. In practice, a combination of chemical treatment and physical filling could provide an optimized solution for improving the photovoltaic properties of the graphene/BFO/Pt heterojunction.

7.3 Photovoltaic heterojunction applicationsTo test the practical applications, we apply our graphene/BFO/Pt photovoltaic heterojunction in the optical and electrical fields with the development of a photosensitive detector and a small electrical signal extractor.

7.3.1 Optical application: Photosensitive detector

As an interesting photovoltaic application, the graphene/BFO/Pt heterojunction is used as a photosensitive detector to drive a photochromic film. Fig.7.8 shows the schematic illustration of the test bench. In the test scenario, one graphene/BFO/Pt unit drives a liquid crystal polymer film; the film has transparency that is controlled by an external voltage. By modulating the incident light onto the graphene/BFO/Pt unit, the output photocurrent can be adjusted correspondingly. A current-mode amplifier module is employed to reduce the noise from the previous stage and is used to drive the photochromic film. A pre-written *McGill University* pattern is put behind the photochromic film [204].



Fig.7.8 Schematic test bench of photochromic film using the graphene/BFO/Pt photovoltaic heterojunction as a photosensitive detector.

It can be seen in Fig.7.9 (a) that the polymer film is opaque without illumination, since the dark current does not provide enough drive and therefore the pattern *McGill University* is not visible. However, by gradually increasing the light intensity, the photocurrent generated by the unit can be powerful enough to turn the polymer film transparent and the characters behind the screen are then observed, as shown in Fig.7.9 (b).



Fig.7.9 Transparency of the photochromic screen under dark (a) and illumination (b) conditions.

7.3.2 Electrical application: Tunable switch

Our graphene/BFO/Pt photovoltaic heterojunction can be used as a bidirectional tunable switch. In the dark *J-V* curve, as shown in Fig.7.10, it can be seen that the graphene/BFO/Pt heterojunction exhibits a bidirectional shoot-through characteristic with a rectifying window of 3.13 V. Large signals beyond the threshold voltages (-1.49 and +1.64 V) can pass through the switch while others will be rectified.



Fig.7.10 Dark/light photocurrent density and corresponding rectifying window of the graphene/BFO/Pt photovoltaic heterojunction.

Such a bidirectional switchable property can be attributed to the intrinsic ferroelectric nature of the BFO material. The rectifying window can be modulated by illumination or by heating; it changes from 3.13 to 1.98 V by applying illumination, as shown in Fig.7.10. Experiments are performed to confirm this bidirectional switchable property. Fig.7.11(a) shows the application test bench and Fig.7.11 (b)-(c) show the output current with rectangular pulse signals with different amplitudes (3 and 0.5 V, peak value). A clear rectifying effect can be found in the 0.5 V input pattern (Fig.7.11(c)), while a good conduction property can be observed with the 3 V signal (Fig.7.11 (b), the graded rise-

falling-edge is due to the charging-discharging effect caused by the junction capacitance). Moreover, a sweep in voltage from -3 to 3 V with increments of 0.1 V and time duration of 100 ms is applied to the heterojunction. A good rectifying response is also found (Fig.7.11(d)), indicating a rectifying effect in both digital and analog applications. The simple device structure (sandwich structure), easy fabrication process (sol-gel), tunable rectifying window (illumination and heat), and easy integration are the major advantages of the graphene/BFO/Pt-based bidirectional switch compared with traditional bidirectional switches composed using different circuit elements.






Fig.7.11 (a) Test bench of the graphene/BFO/Pt heterojunction operated as a bidirectional tunable switch. Output current with rectangular pulse signals with different amplitudes (b) 3 V and (c) 0.5 V. (d) Time domain test result for a sweep in voltage from -3 to 3 V.



Fig.7.12 Schematic diagram of the "small signal extractor" application based on graphene/BFO/Pt.

This type of structure can be applied as a small signal extractor, as shown schematically in Fig.7.12. Complex signal inputs will be divided into two channels. One channel will pass through the graphene/BFO/Pt heterojunction and the small signal will be eliminated. Then, by subtraction with the original signal in the other channel, the small

signal will be separated from the large signal. Such a small signal extractor is desirable in fields where the signal to noise ratio is fairly low.

7.4 Conclusion

In this chapter, we advanced our photovoltaic investigation of the graphene/BFO/Pt heterojunction and studied the performance enhancement and optimization processes. To start with, we investigated the chemical enhancement effect. By introducing HNO₃ to the photovoltaic heterojunction, a ~150 fold improvement in photocurrent was observed in our study. This dramatic enhancement effect was then explained in detail using our theoretical model built in Chapter 6. A physical enhancement approach, CdSe QDs sensitization and filling, was used in the graphene/BFO/Pt heterojunction, and the corresponding performance enhancement was reported experimentally and theoretically. As a conclusion, the advantages and disadvantages of both chemical and physical routines were compared. In the second part of this chapter, we applied our graphene/BFO/Pt photovoltaic unit in the electrical and optical fields. A photosensitive detector and a tunable switch were proposed and implemented in our study.

Chapter 8

Conclusion

erroelectric materials have attracted significant research interest due to their unique electrical, optical, dielectric, piezoelectric, and photovoltaic properties. The coupling of such properties provides extra degrees of freedom in many technologically demanding applications, for instance, non-volatile ferroelectric random access memory (FeRAM), optical waveguides and modulators, high-K mediums, piezoelectric sensors and varactors, and photovoltaic devices. As an important application format, ferroelectric thin films have been extensively investigated since the late 1960s, when silicon integration processes and thin film deposition technologies began to boom. Research regarding theoretical ferroelectric principles, materials engineering, and fabrication technologies is always active in ferroelectric related fields. The research presented in this thesis provides a comprehensive investigation, including theoretical principles, fabrication technology, performance optimization, and electrical/optical application of two novel ferroelectric materials, namely, Nd-doped bismuth titanate (BNdT) and bismuth ferrite (BFO). In this chapter, we provide a summary of the work presented in this thesis. We also reiterate the central ideas and research methodologies associated with this work. Finally, we suggest directions for future work and other research avenues that may be pursued.

8.1 Summary

In Chapter 1, we provided motivation for the research presented in this thesis, and briefly introduced ferroelectric based electrical, optical, and photovoltaic applications. By detailing the current problem statement in the three major ferroelectric application domains, we outlined the research objectives that demarcate the course of this work. A section listing the original contributions of this thesis was supplied, followed by a full thesis overview.

Chapter 2 provided the background necessary for understanding ferroelectric research and applications. We started the review with a description of the ferroelectric mechanism, fabrication technologies, and the development of ferroelectric materials. We then introduced current state of the art research in the ferroelectric based electrical, optical, and photovoltaic domains.

In Chapter 3, we presented fabrication and characterization of the ferroelectric material BNdT. Starting with the precursor preparation, we studied the sol-gel and spinning coating processes for the BNdT material. Different fabrication parameters were analyzed in order to optimize the ferroelectric properties of the BNdT material. Microstructure properties such as XRD, Raman scattering, SEM, AFM, TEM, etc., were also investigated. Different ferroelectric performance characteristics, such as remnant polarization, fatigue endurance, and leakage density were provided in detail. In the latter part of this chapter, material engineering was applied to fabricate BNdT materials with

different elemental constituents, and the corresponding variation in properties was therein reported.

Based on our studies up to this point, we furthered our research into the optical characterization of BNdT in Chapter 4, and demonstrated the first systematic investigation of BNdT optical properties. With different fabrication parameters and elemental constituents, optical parameters such as optical transmittance, refractive index, extinction coefficient, and optical band gap energy were examined and their correlation with different fabrication parameters and the microstructure were investigated both experimentally and theoretically.

Chapter 5 presented the ferroelectric characterization of a multiferroic BFO material. Due to the intrinsic low conductivity at room temperature, the ferroelectric performance of the pure BFO material has never been reported. Based on the content discussed in Chapters 2 and 3, we employed the BNdT ferroelectric thin film as a seeding layer for the BFO/BNdT multilayer heterojunction, and we report the room temperature ferroelectric measurement of this pure BFO ferroelectric for the first time. A theoretical analysis was conducted to describe the phenomenon of ferroelectric enhancement, and a ferroelectric inducing effect was presented and discussed.

In Chapter 6, photovoltaic research on the multiferroic BFO material was presented as an advanced topic of investigation on BFO ferroelectrics. By introducing a graphene nano transparent electrode, we reported enhanced photovoltaic performance of the BFO material in a graphene/polycrystalline BFO/Pt heterojunction structure for the first time. The remarkable electrical and optical properties of the graphene sheet, including ballistic electronic transport, ultra high carrier mobility, high conductivity and transparency, result in a superior BFO photovoltaic performance which is much improved compared to results reported in the literature. A theoretical model considering the ferroelectric polarization, interface states, and energy band bending effect, were proposed to describe the BFO ferroelectric photovoltaic effect and carrier transport behaviour for the first time. Important photovoltaic parameters, such as conversion efficiency, illumination intensity response, ON/OFF characteristics, minority carrier lifetime, and external quantum efficiency (EQE), were investigated experimentally and theoretically.

Chapter 7 investigated optimization of the existing photovoltaic effect in the graphene/polycrystalline BFO/Pt heterojunction. HNO₃ treatment and CdSe quantum dots (QDs) filling/sensitizing, as two independent chemical and physical routines, were processed and compared. The photocurrent density demonstrated a significant improvement of ~150 fold after HNO₃ treatment, while a considerable enhancement of ~5 fold was seen with QDs filling/sensitizing. Finally, a photosensitive detector and a tunable switch were proposed as two interesting applications of the BFO photovoltaic effect.

8.2 Research methodologies

The work presented in this thesis was conducted at different academic institutions. More specifically, work from Chapters 3 to 5 was executed at McGill University, Université de Montréal, and Institut National de la recherche scientifique (INRS), whereas work from Chapters 6 and 7 was conducted at both McGill University and Tsinghua University. Detailed specification targets were established as part of the workflow. Fig.8.1 summarizes the research methodologies for this work.



Fig.8.1 Methodologies of the research.

8.3 Future research avenues

Although the objectives of this research have been fulfilled, there are still other research opportunities left to be investigated. Below, we propose directions for future research that could follow from the work presented in this thesis.

(1) Preparation of the BNdT material

As a novel ferroelectric material, BNdT has attracted much interest since its discovery. However, to the best of our knowledge, all of the research has been conducted based on sol-gel derived BNdT thin films; a physical routine for preparing the BNdT material has never been reported. According to common practice, a ferroelectric thin film derived using a physical routine will possess better ferroelectric phase and thus better performance in a ferroelectric application. Epitaxial growth, for instance, may be a good practice, since it can help minimize the grain boundaries existing in polycrystalline phase, and thus reduces the light scattering in optical applications. Meanwhile, due to its unique 3D deposition feature, the MOCVD routine may also be a useful way of preparing the BNdT material, especially in some 3D MEMS related applications.

(2) Optical application of the BNdT material

Few research reports have been published on the topic of optical applications of BNdT material; most of the existing research has focused on electrical related applications. The content presented in this thesis provides a valuable advancement in the study of BNdT in the optical domain. Optical waveguides, modulators, and switches would be interesting applications that could be investigated in the near future.

(3) Thick film technology in ferroelectric optical MEMS

As discussed in this thesis, the ferroelectric based actuator is a promising candidate in

today's optical MEMS domain. However, the thickness of the ferroelectric film is an important fabrication issue to consider in the design and application. Ferroelectric thin films, as applied in electrical applications such as FeRAM, cannot provide sufficient driving force for scanning mirrors. For example, for the PZT material, a thickness of more than 1 µm is required to achieve sufficient force to actuate the mirrors. Many fabrication processes such as screen printing sol-gel, hydrothermal, and gas deposition have been investigated in attempts to improve the thickness of the as-prepared PZT film. However, very few of these methods have met the high deposition rate, low process temperature, large area coverage, and cost requirements. Many approaches to increase the deposition rate of the ferroelectric thick film in optical MEMS applications are still being researched.

(4) The operating principle of ferroelectric EO devices

Due to the complex nature of the frequency response of the EO effect in ferroelectric materials, the operating principle of ferroelectric EO devices is not well understood, and no explicit models describing the dynamic EO response have been demonstrated. To further establish the use of ferroelectric materials in high-bandwidth applications, it is necessary to first determine an accurate model for the ferroelectric dynamic EO response. Recently, domain reorientation has been proven to be a primary mechanism responsible for the transient, nonlinear optical response of ferroelectric materials at steady state. However, the simultaneous response of the ferroelectric EO effect has not yet been reported, and related studies are necessary to further develop ferroelectric EO research.

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