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2 **Vitrification a versatile method to modulate properties of myrcene-based rubbers**

3
4 Farhad Asempour ^a, Milan Maric ^{a,b*}

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6 ^a Department of Chemical Engineering, McGill University, 3610 University St, Montreal, H3A
7 0C5, Quebec, Canada

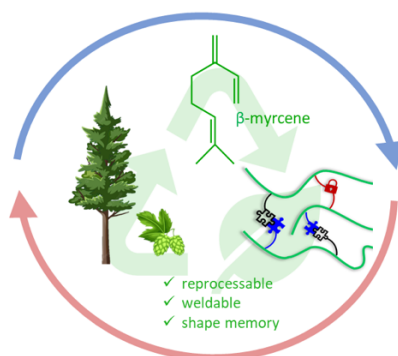
8 ^b McGill Institute of Advanced Materials (MIAM), Quebec Centre for Advanced Materials
9 (CQMF / QCAM), Canada

10 * Corresponding author

11 E-mail address: milan.maric@mcgill.ca

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14 **Keywords:** bio-based elastomer, recyclable, terpene, vinylogous urethane, dynamic cross-linking,
15 shape memory, nitroxide mediated polymerization

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19 **Graphical abstract**



1 **Abstract**

2 We report bio-derived vitrimeric rubbers with weldability and excellent reprocessability.
3 Reversible deactivation radical copolymerization of the commercially available terpene-based β -
4 myrcene with 10 to 30 mol% (2-acetoacetoxy)ethyl methacrylate (AAEMA) afforded linear
5 prepolymers which were cross-linked in a single step treatment with difunctional amine, the
6 vegetable oil-derived Priamine 1075, or trifunctional amine tris(2-aminoethyl)amine (TREN).
7 Decoupling the networks' backbone structure and cross-linkers led to high tunability of the
8 vitrimers' final mechanical and rheological properties using prepolymer composition, molecular
9 weight, nature and concentration of cross-linker and cross-linking density. Glass transition
10 temperature (T_g) of the vitrimers ranged between -49 to -5 °C while the average elongation and
11 stress at break ranged from ~83% and 0.18 MPa to ~30% and 1.68 MPa respectively from the
12 lowest, 0.12 mol/L, to the highest, 0.98 mol/L, cross-linking densities. Characteristic features of
13 dynamic vinylogous urethane-vitrimers were confirmed over at least 3 reprocessing cycles by
14 grounding and hot pressing at 110 °C. No appreciable change in the ATR-FTIR spectra, T_g ,
15 decomposition temperatures, tensile properties and storage modulus were observed due to the
16 reprocessing. Furthermore, incorporation of 5 mol% epoxy-based glycidyl methacrylate into the
17 prepolymer led to the formation of a network with dual static and dynamic cross-links. Compared
18 to the counterpart network with solely dynamic cross-links, the addition of static cross-links
19 decreased creep by 75% and imparted shape memory effects. This work shows that combining
20 vitrimer chemistry with myrcene is a facile and inexpensive, yet highly versatile method to not
21 only modulate and compensate for the poorer mechanical properties of brush-like terpene-based
22 elastomers but also provides a potential platform for recyclable bio-based rubbers with more
23 sophisticated functionalities.

1 **1. Introduction**

2 Global warming and plastic waste pollution are considered planetary threats ¹. As a result, there is
3 a growing interest in shifting from petroleum-based single-use polymers towards renewably
4 sourced plastics with improved recyclability ^{2,3}. In this work, we are particularly focusing on the
5 development of “greener” alternatives for thermosetting elastomers. Given the massive size of the
6 synthetic rubber industry, with the current estimation of 15 to 20 million metric tons (MMT) per
7 year, even small improvements can have significant environmental benefits ^{4,5}.

8 Thermosets and elastomers are an irreplaceable category of polymers with substantial advantages
9 associated with their mechanical, thermal, and chemical resistant properties ⁶. However, due to
10 their cross-linked molecular structure, they are commonly difficult to (re)process and recycle ^{7,8}.

11 This issue has historically drawn a lot of attention from the polymer community. In the past two
12 decades, covalent adaptable networks (CANs) exhibiting reversible covalent chemistry have
13 appeared to offer a possible solution ^{9–12}. However, CANs can undergo depolymerization under
14 certain conditions and temperatures, limiting their applications ⁵. This has led to the development
15 of vitrimers, first reported in 2011, as a new category of polymeric materials bridging the gap
16 between thermosets and thermoplastics ^{5,13,14}. Vitrimers are permanently cross-linked networks
17 with thermally induced “associative” dynamic covalent bonds ^{15,16}. This provides them with a
18 unique ability to behave like thermosets at service temperatures but can change topology and be
19 reprocessed without decreasing connectivity and dissolution at elevated temperatures ^{6,17}. Several
20 catalyst-free chemistries such as exchanges of silyl ethers ^{18,19}, imines ^{20,21}, vinylogous urethanes
21 ^{6,22,23}, disulfides ^{5,24}, dioxaborolane metathesis ^{17,25–27}, hydroxy urethanes ²⁸ and metathesis of
22 cyclic acetals ²⁹ have been reported, showing great potential for malleability, shape memory, and
23 weldability ^{30–34}. Despite these advantageous properties, it has been commonly reported that

1 vitrimers undergo substantially higher creep compared to their static thermosetting counterparts
2 ^{6,35}. Improving the dimensional stability of vitrimers is still an evolving area of research. It has
3 been shown that a vitrimer's molecular architecture greatly influences its malleability and
4 rheological properties ³⁶⁻³⁸.

5 In addition to reprocessability and recyclability, renewability plays a key role in the development
6 of more sustainable polymeric materials ³⁹. Aside from natural rubber, various bio-based platforms
7 such as itaconic acids, vegetable oils, lactides, norbornenes, and terpenes have shown much
8 potential to produce rubbers ^{39,40}. Terpenes are particularly promising candidates as they can
9 undergo radical polymerization with comparatively higher efficiencies ⁴⁰⁻⁴². Terpenes are made
10 from highly abundant forestry feedstocks and are composed essentially of isoprenic motifs.
11 Specifically, β -Myrcene (Myr) is a readily available acyclic monoterpene with a conjugated diene
12 structure⁴³. Myr can be isolated from pine, hops, bay leaves, lemongrass, celery, nutmeg, and
13 rosemary ^{44,45}. Myr is industrially produced by pyrolysis of β -pinene, a major constituent of natural
14 turpentine oil ⁴⁵. Similar to other 1,3-dienes, such as butadiene and isoprene, poly(Myr) also forms
15 low glass transition temperature (T_g) (~ -75 °C) rubbery polymers ⁴⁶. In addition to renewability,
16 an advantage of Myr over butadiene and isoprene is its lower volatility with a boiling point of 167
17 °C, meaning that Myr does not require pressurized equipment to handle ⁴⁷. However, the longer
18 pendent side chain in poly(Myr) results in a higher entanglement molecular weight of ~ 18 kg/mol
19 compared to that of poly(butadiene) and poly(isoprene) with ~ 3 and ~ 6 kg/mol respectively ^{46,48}.
20 This in general can result in lower tensile strength, elongation, and toughness of poly(Myr),
21 potentially limiting its applications ^{43,49}. Although some in-depth studies involving various
22 polymerization techniques and properties of poly(Myr) have been reported, thorough
23 investigations on the applications of poly(Myr)-based elastomers in the rubber industry are

1 generally lacking in the literature ^{48,50,51}. Some works have investigated applications of vulcanized
2 poly(Myrr) as well as Myrr-based thermoplastic elastomers with styrene and isobornyl methacrylate
3 (IBOMA)^{47,52–55}. Bhowmick’s and Gong’s groups have also reported Myrr-based CANs using
4 Diels-Alder chemistry via Myrr copolymerizations with furan-based monomers. The resulting
5 elastomers exhibited self-healing and shape memory properties ^{56,57}.

6 Recently several works have reported promising results combining renewability and recyclability
7 via vitrimer chemistry to produce elastomers ⁵⁸. Kolsch et al. synthesized poly(itaconate)
8 elastomers with catalytic transesterification ⁵⁹. Feng et al. prepared photothermally induced self-
9 healable and shape memory epoxidized natural rubber-based elastomers using catalytic
10 transesterification ⁶⁰. Liu et al. reported the development of a cross-linker with triple dynamic
11 covalent bonds (boroxine, disulfide bond, imine bond) for the vitrification of epoxidized natural
12 rubber, imparting self-healing and recyclability ⁶¹.

13 In this study, we report a facile method to produce thermally reprocessable bio-derived vitrimeric
14 rubbers based on catalyst-free vinylogous urethane exchanges. Well-defined copolymers of
15 inexpensive and commercially available Myrr with a monomer containing a reactive β -ketoester
16 moiety, 2-acetoacetoxy)ethyl methacrylate (AAEMA), were synthesized using nitroxide mediated
17 polymerization (NMP). Two different cross-linkers, Priamine 1075 (referred to simply as Priamine
18 hereafter), a long-chain dimer diamine with 100% bio-based carbon content, as well as tris(2-
19 aminoethyl)amine (TREN), a smaller triamine molecule, were utilized to tailor cross-linking
20 density. Thermomechanical tests showed that the resulting vitrimers had excellent reprocessability
21 after three cycles of grounding and hot pressing. Moreover, to suppress creep and eventually
22 impart shape memory effects, terpolymers of Myrr, AAEMA, and glycidyl methacrylate (GMA),
23 the latter containing an epoxy moiety, were synthesized. Upon reactions with amines, a dual static

1 and dynamic network was formed. The use of different prepolymer compositions, cross-linkers,
2 and the addition of the low number of static cross-links provided a versatile toolbox to tune the
3 final mechanical and rheological properties of the vitrimers.

4

5 **2. Experimental**

6 **2.1. Materials**

7 All chemicals were of reagent grade and used as received unless otherwise stated. β -Myrcene
8 (Myr, Sigma-Aldrich, $\geq 90\%$), (2-acetoacetoxy)ethyl methacrylate (AAEMA, TCI, 95%), glycidyl
9 methacrylate (GMA, Sigma-Aldrich, 97%) were purified by passing through columns of basic
10 alumina (Al_2O_3 , Brockmann, Type I, Sigma-Aldrich) mixed with 5 wt% calcium hydride (90-95%,
11 Sigma-Aldrich) and stored in a refrigerator under a head of nitrogen until needed. Priamine 1075
12 (Priamine) was procured from Cargill and tris(2-aminoethyl)amine (TREN, 97%) was purchased
13 from Alfa Aesar. Butylamine (99%) was purchased from Sigma-Aldrich. Tetrahydrofuran (THF,
14 HPLC grade), toluene ($>99\%$), chloroform ($>99\%$), N,N- dimethylformamide (DMF, $>99\%$),
15 acetone ($>99\%$), reagent alcohol (anhydrous ethanol 90% v/v; methanol 5% v/v; 2-Propanol 5%
16 v/v), methanol ($>99\%$) were purchased from Fisher Scientific. Deuterated chloroform (CDCl_3 ,
17 $\geq 99\%$) was purchased from Cambridge Isotopes Laboratory for ^1H NMR analyses.

18 BlocBuilderTM (BB, also known as MAMA-SG1, is the alkoxyamine for NMP, and SG1 is the
19 free nitroxide, see Figure S1 for more details) was obtained from Arkema. 2-Methyl-2-[N-tert-
20 butyl-N-(1-diethoxyphosphoryl-2,2-dimethylpropyl)-aminoxy]-N-propionyloxy-succinimide
21 (NHS-BB, also known as NHS-BlocBuilder) was synthesized according to the previous literature
22 ⁶². N,N'-dicyclohexylcarbodiimide (DCC), N-hydroxysuccinimide (NHS) were procured from
23 Sigma Aldrich.

24

1 2.2. Polymer synthesis

2 We synthesized three different statistical copolymers of Myr with either 10, 20, or 30 mol%
3 AAEMA content with similar molecular weights. NMP with BlocBuilder, an SG1-based
4 alkoxyamine, was used to initiate and control the synthesis of well-defined prepolymers. All
5 polymerizations were performed in bulk. Table 1 summarizes the copolymerization formulae and
6 reaction conditions for prepolymers. As an example, for the synthesis of MyrAA-20 prepolymer,
7 Myr (56.45 g, 414.3 mmol), AAEMA (22.2 g, 103.6 mmol), BlocBuilder (1.2 g, 3.145mmol), and
8 a magnetic stir bar were added to a 250 mL three-neck round-bottom glass flask. The reactor was
9 equipped with an overhead reflux condenser connected to a chiller (Fisher Scientific Isotemp
10 3016D) at 2 °C. The reaction solution was sparged with high-purity N₂ gas for 20-25 minutes prior
11 to being heated at 125 °C for 8h using a heating mantle and a feedback temperature controller.
12 Samples were periodically taken for ¹H NMR and GPC analyses. Afterward, the reaction was
13 stopped by lowering the temperature, and the obtained viscous solution was three times
14 (re)precipitated into a mixture of ethanol/methanol (70/30 v/v%) from THF. It should be noted
15 that, the (re)precipitation and work up resulted in some polymer loss. Finally, the polymer was
16 dried under a reduced pressure at 60 °C overnight, yielding 39.1 g of a yellow-colored viscous
17 liquid. The overall monomer conversion from ¹H NMR was 88.2%, see Supporting Information
18 section S2, and from gel permeation chromatography (GPC), the number average molecular
19 weight (M_n) was 12,800 g/mol with the dispersity (\mathcal{D}) of 1.49 relative to PMMA standards.

20 We also studied the effects of physical molecular entanglements on the rheological properties of
21 vitrimers. To do so, we synthesized a prepolymer with a molecular weight higher than the
22 entanglement molecular weight (M_e) of poly(Myrr) homopolymer, MyrAA-30-Long, by increasing
23 the theoretical target molecular weight to 60 000 g/mol at 100% monomer conversion.

1 Furthermore, to incorporate static cross-links into the vitrimeric network, we prepared a
 2 terpolymer of Myr with 20 mol% AAEMA and 5 mol% GMA. For the synthesis of the GMA-
 3 bearing prepolymer, a different initiator with an SG1-based alkoxyamine initiator bearing an N-
 4 succinimidyl ester group was synthesized (NHS-BlocBuilder) and utilized according to the
 5 literature⁶³.

6 The prepolymers are coded as MyrAA-xx, where xx refers to the AAEMA mol% in the initial
 7 monomer mixture composition. The high molecular weight polymer was coded as MyrAA-30-
 8 Long, and the copolymer with 5 mol% GMA content was named MyrAA-20-GMA-5.

9
 10 **Table 1.** Myrcene/ AAEMA/ GMA copolymerization formulae and synthesis conditions

prepolymer code ^a	[Alkoxyamine] ₀ (M) ^c	[Myr] ₀ (M) ^d	[AAEMA] ₀ (M)	[GMA] ₀ (M)	$M_{n, target}$ ^e (g/mol)	T (°C)	time (h)
MyrAA-10 ^a	0.033	5.19	0.58	—	25,000	125	8.5
MyrAA-20 ^a	0.035	4.56	1.21	—	25,000	125	8
MyrAA-30 ^a	0.036	3.82	1.79	—	25,000	125	6
MyrAA-30-Long ^b	0.015	3.83	1.79	—	60,000	125	8
MyrAA-20-GMA-5	0.033	4.32	1.15	0.29	25,000	125	6

11
 12 ^a Experimental identification of copolymers: MyrAA-xx, where xx referees to the initial molar
 13 ratio of AAEMA

14 ^b Long refers to prepolymer with higher target number average molecular weight (M_n)

15 ^c Molar concentration of BlocBuilder, or NHS-BlocBuilder in case of MyrAA-20-GMA-5

16 ^d Initial monomer molar concentration in the feed

17 ^e Target M_n at 100% conversion
 18

19 2.3. Formation of vitrimers and (re)processing

20 Vitrification of a prepolymer started with dissolving it in THF, 40% (w/v), followed by the addition
 21 of either Priamine or TREN and stirring until gelation. The resulting gel was left overnight at room
 22 temperature in a fume hood and was further cured and dried at $75 \pm 10^\circ\text{C}$ under reduced pressure
 23 in a vacuum oven for 8-12 h. The resulting vitrimer was ground up and hot pressed (Carver Manual
 24 Hydraulic Press with Watlow temperature controllers), while sandwiched between two Teflon

1 plates, at 110 ± 5 °C under 6 ± 1 metric tons for 50 ± 5 min yielding a yellow and transparent
2 shaped material. See Supporting Information and Figure S3 for each step. To further explore the
3 effects of cross-linking density, two different ratios of β -ketoester : amine were studied; 1:1 and
4 0.7:1. Vitrified polymers are coded as “MyrAA-xx-P/T-yy” where xx is the rounded molar ratio
5 of the AAEMA, P/T shows the type of cross-linker, T for TREN or P for Priamine, and yy indicates
6 the molar ratio of β -ketoesters from AAEMA in the co/terpolymer to NH_2 from the cross-linker.
7 As an example, *MyrAA-20-T-0.7* represents a vitrified polymer with 20 mol% AAEMA which is
8 cross-linked with TREN with a 0.7:1 ratio of β -ketoesters to NH_2 .

9

10 **2.4.Characterization**

11 **Nuclear Magnetic Resonance (NMR) Spectroscopy**

12 ^1H NMR spectra were recorded on a Bruker AVIIIHD 500 MHz Spectrometer using 16 scans with
13 CDCl_3 at room temperature.

14 **Gel Permeation Chromatography (GPC)**

15 The number average molecular weight (M_n) and dispersity ($D = M_w / M_n$) of the polymers
16 synthesized were estimated using GPC (Waters, Breeze System) in THF (HPLC) at 40 °C and a
17 flow rate of 0.3 mL/min. The GPC system was equipped with a guard column, a differential
18 refractive index (RI 2414) detector and three Styragel HR columns (with a molecular weight
19 measurement range of 10^2 to 5×10^3 g/mol for HR1, 5×10^2 to 2×10^4 g/mol for HR2 and 5×10^3 to
20 6×10^5 g/mol for HR4). Poly(methyl methacrylate) (PMMA) (Varian) standards were used for
21 calibration of molecular weights ranging from 875 to 1,677,000 g/mol.

22 **FT-IR Spectroscopy**

23 Infrared spectra were collected on a Thermo Scientific Nicolet™ iS50 FTIR Spectrometer
24 equipped with diamond attenuated total reflectance (ATR) accessory using 32 scans.

1 **Differential Scanning Calorimetry (DSC)**

2 DSC experiments were collected on a Discovery 2500 TA Instruments equipped with an
3 autosampler and refrigerated cooling system (RSC 90) using aluminum hermetic pin-hole pans.
4 Calibrations for temperature and heat flow were carried out using indium and benzoic acid
5 standards. Temperature ramp experiments (cool/heat/cool/heat) were run from -90 to 30 °C under
6 nitrogen with heating rate of 15 °C/min and cooling rate of 10 °C/min with 3-min isotherms at
7 each extreme. Experimental data were recorded and analyzed using TA instrument TRIOS
8 software. The reported T_g were calculated using the curve inflection and only the second heating
9 run was considered to remove any thermal history.

10 **Thermal Gravimetric Analysis (TGA)**

11 To study the thermal stability of the polymers, a TA Instrument's Discovery TGA 5500 with
12 autosampler and platinum pans were used. All experiments were done under a nitrogen flow. The
13 samples were heated to 100 °C for 30 min isotherms prior to each run to remove any moisture or
14 residual solvent. Ramp experiments were performed with a heating rate of 15 °C/min until 650 °C.
15 Isothermal experiments were done from room temperature up to 110 °C and remained at the
16 temperature for a 6 h total run time.

17

18 **Tensile Analysis Testing**

19 Tests were performed on a universal Shimadzu Easy Test system with a 500 N load cell and a
20 crosshead speed of 10 mm/min. Dog-bone shaped tensile specimen similar to ASTM D638 type
21 V (overall length of 60 mm and respective neck thickness and width of approximately 2 and 3mm)
22 were prepared using a Carver hot-press as described previously²³. Reported results are the average
23 of at least 3 specimens.

1 **Dynamic Mechanical Analysis (DMA) and Rheology**

2 All tests were done using an Anton Paar MCR 302. DMA tests were conducted using a solid
3 rectangular fixture (SFR 12). Rectangular-shaped samples (60mm length, 10mm width, and 2mm
4 thickness) were heated from room temperature to 130 °C with an average rate of 5 °C/min and at
5 a frequency of 1 Hz. Rheological tests were done with a 25 mm parallel plates geometry. Strain
6 sweep tests were carried out at 100-130 °C to determine the linear viscoelastic region (LVR) at 1
7 Hz. Stress relaxation experiments were conducted at 0.1 % strain at the desired temperatures.
8 Creep recovery experiments were performed at 1000 Pa for 300 s followed by 0 Pa for 600 s, for
9 a total experiment time of 900 s.

10 **Gel fraction and swelling tests**

11 Gel fraction was obtained by soaking the networks in excess amount of a desired solvent for 72
12 hours at room temperature. Next, the swelled samples were filtered, dabbed with delicate task
13 wipes to remove any excess solvent, and immediately weighed to find the samples' swelling ratio.
14 This was followed by drying the samples in a vacuum oven at reduced pressure and 60 °C for a
15 day, and finally weighing them. Gel fraction was calculated using m_2 / m_0 where m_0 is the original
16 mass of the sample and m_2 is the mass of dried sample after swelling.

17

18 **3. Results and discussion**

19 **3.1. prepolymer synthesis and characterization**

20 We anticipated that the thermomechanical properties of the final vitrimers would be dictated by
21 those of the linear reactive precursors. Therefore, we commenced our studies by synthesizing
22 statistical copolymers of Myr with AAEMA, which provides the functionality for amine-
23 crosslinking. NMP with BlocBuilder was used to control the molecular weight of the prepolymers
24 and minimize possible side reactions and cross-linking of Myr during the polymerization.

1 Copolymerizations of Myr using reversible-deactivation radical polymerization (RDRP) have
2 been reported^{40,42,64}. For example, Pablo-Morales et al. and Hilschman et al. utilized reversible
3 addition–fragmentation chain-transfer (RAFT) for copolymerization of Myr with GMA and
4 styrene respectively^{65,66}. Métafiot et al. showed effective copolymerization of Myr with
5 methacrylates such as IBOMA and GMA with highly regioregular microstructure using
6 NMP^{47,52,67}. Herein, NMP was adopted since it does not rely on sulfur-based chain transfer agents
7 or any metallic ligands^{68–70}. This is particularly important since the thiocarbonylthio chain transfer
8 agent moieties in RAFT are prone to rapid aminolysis upon treatment with primary amines and
9 therefore chain end modification is required before further processing^{23,34}.

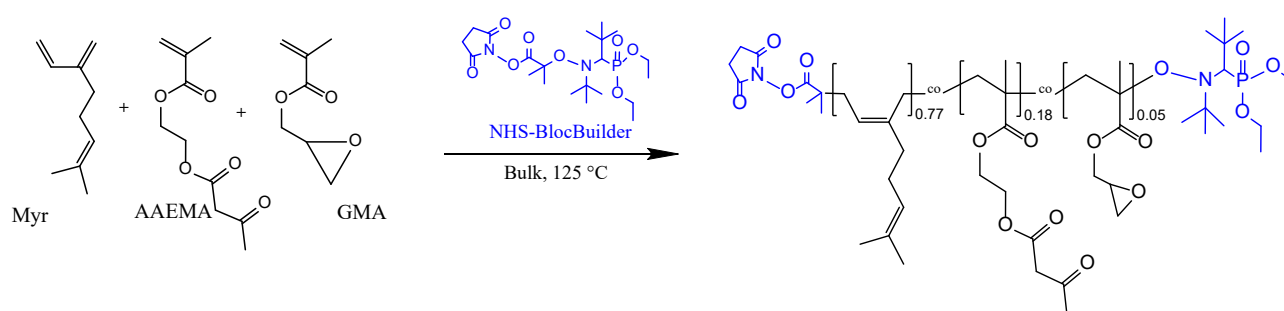
10 Three different prepolymers with initial AAEMA feed ratios of 10, 20 and 30 mol% were prepared
11 to investigate the effects of cross-linking density. See Figure 1 and S1 for the synthetic route used
12 to prepare these copolymers. Table 2 summarizes the overall monomer conversion, molecular and
13 thermal characterization of all synthesized prepolymers. Characterization by GPC showed that the
14 M_n of the MyrAA-10, 20 and 30 were predictable, ranging from 11.8 to 12.8 kg/mol with relatively
15 low dispersities (D) of 1.38 to 1.51. It should be mentioned that some deviation from the theoretical
16 M_n was observed which indicates divergence from the ideal persistent radical effect and the
17 possibility of chain transfer and/or termination reactions^{68,71}. Additionally, all M_n s reported were
18 relative to PMMA standards, which may introduce some error as the copolymers were largely
19 Myr-based in composition. Figure 2 illustrates representative kinetic plots and molecular weight
20 characterizations of MyrAA-10. From the ¹H NMR analyses, a pseudo-first-order linear monomer
21 conversion over time was observed. Reasonable overall monomer conversion of 76 to 89% for
22 Myr, and >95% for AAEMA were achieved. See Figures S4 and S5 for representative ¹H NMR
23 spectra, calculations of conversion, and Figure S6 for GPC traces. The observed linear trend of

1 chain growth combined with the low \bar{D} suggest that the possible side reactions and chain
2 terminations were largely suppressed^{68,72}. Figure S7 shows the ratio of unreacted AAEMA to Myr
3 monomers as a function of the polymerization time of MyrAA-10. A decrease in the reactants'
4 composition ratio from 0.11 to 0.01 over time suggests some compositional drift in the
5 prepolymers. Further investigation on the reactivity ratios and compositional drift of Myr and
6 AAEMA is underway and will be addressed separately. Via ¹H NMR, the microstructure of the
7 incorporated Myr was also determined. Myr can be polymerized into 3 different regioisomers: 1,4-
8 , 3,4- and 1,2- vinyl addition^{47,53}. All prepolymers had high regioregularity with >90% of the 1,
9 4-addition structure, which agrees with the literature^{49,53,65}.

10 In the second part of our study, we aimed to suppress creep in the vitrimers using two strategies:
11 incorporating physical chain entanglements or adding chemically static cross-links. To achieve the
12 first strategy, we synthesized a statistical prepolymer of Myr and AAEMA with M_n of 22 kg/mol
13 (coded as MyrAA-30-Long) which is slightly higher than the critical entanglement molecular
14 weight (M_e) of poly(Myrr) homopolymer ($M_e \sim 18$ kg/mol)^{46,73}. Figure S8 shows the GPC traces of
15 all prepolymers. A clear shift towards higher molecular weights was observed for MyrAA-30-
16 Long.

17 Moreover, we incorporated GMA in MyrAA-20-GMA-5 prepolymer, as seen in Figure 1. The
18 epoxy group in GMA can react with amines and generate secondary chemically static cross-links.
19 For the synthesis of the GMA-based prepolymer we used NHS-BlocBuilder instead of neat
20 BlocBuilder. This was to avoid side reactions between the epoxy group and carboxylic acid groups
21 from BlocBuilder^{63,67}. Interestingly, MyrAA-20-GMA-5 had a comparatively lower \bar{D} of 1.29.
22 This can be attributed to a higher dissociation rate and slightly lower activation energy of NHS-
23 BlocBuilder, compared to BlocBuilder, which mimics the use of additional controlling SG1,

1 thereby providing more efficient control^{62,67}. Incorporation of epoxy groups was confirmed by ¹H
 2 NMR, Figure S5.
 3 From the DSC traces, T_g of the prepolymers systematically increased from -63 °C to -49 °C by
 4 increasing the AAEMA and GMA content; see Figure S9 for the DSC experiments. The measured
 5 T_g s are in good agreement with the estimates from the Flory-Fox equation⁷⁴, see Table S1 for the
 6 details.



10 **Figure 1.** Statistical copolymerization of MyrAA-20-GMA-5 with NHS-BlocBuilder. A
 11 controlled radical polymerization was achieved using NMP.

12
13 **Table 2.** Molecular and thermal characterizations for various synthesized prepolymers

code	X (%) ^a	M_n (g/mol) ^b	\bar{D} ^b	F_{Myr} ^c	1,4 addition	F_{AAEMA}	F_{GMA}	T_g (°C) ^d
MyrAA-10	70.0%	11,800	1.38	90%	93.5%	10%	—	-63
MyrAA-20	88.2%	12,750	1.49	82%	89.6%	18%	—	-62
MyrAA-30	92.6%	12,650	1.51	69%	93.6%	31%	—	-53
MyrAA-30-Long	90.2%	22,060	1.45	70%	92.3%	30%	—	-54
MyrAA-20-GMA-5	79.5%	13,860	1.29	77%	92.4%	18%	5%	-49

14

15 ^a Overall monomer conversion determined by ¹H NMR

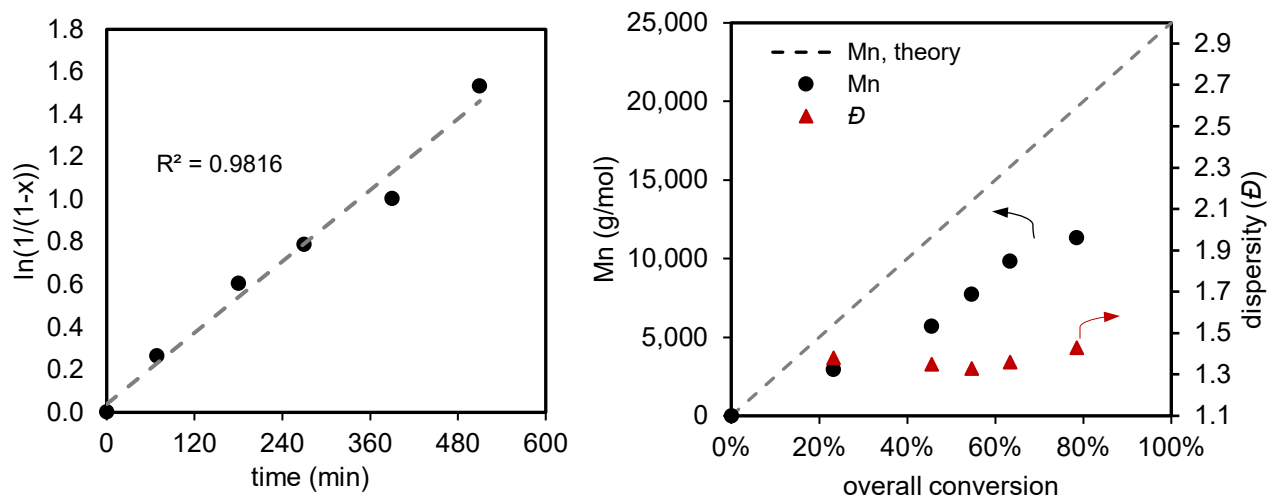
16 ^b Number average molecular weight (M_n) and dispersity (\bar{D}) from GPC relative to PMMA standard
 17 in THF at 40 °C

18 ^c Molar fraction of monomers in the final polymer determined by ¹H NMR

19 ^d Percentage of 1,4 addition microstructure in poly(Myrr)

20 ^e Determined by DSC

1



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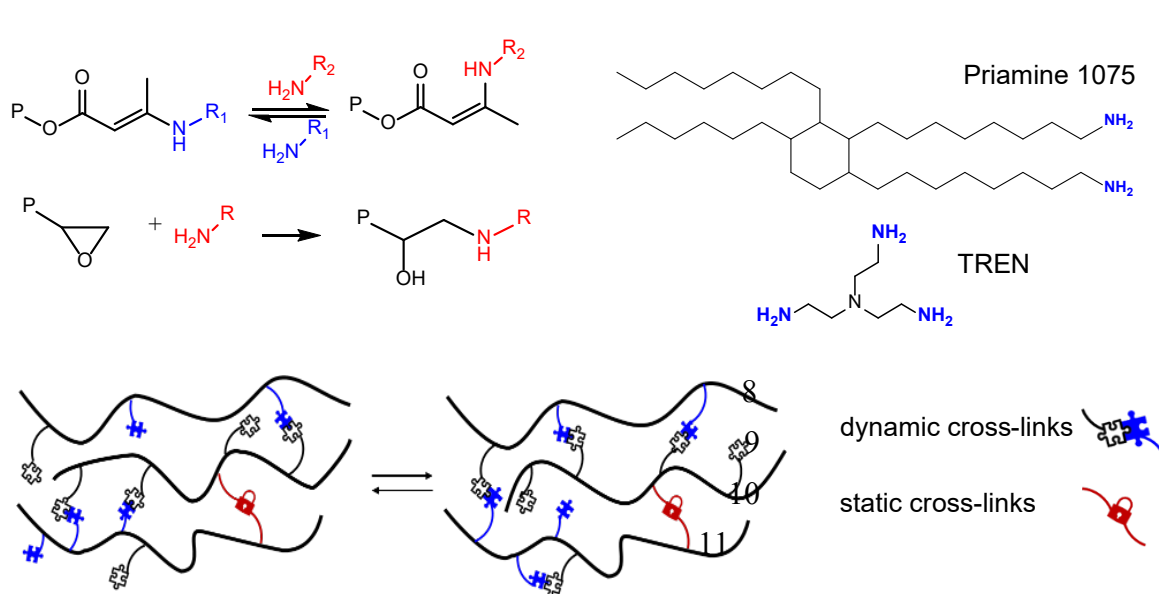
3 **Figure 2.** Representative polymerization data of MyrAA-10 prepolymer: left) linearized overall
 4 monomer conversion versus time and right) evolution of M_n and D against overall monomer
 5 conversion.

6

7 3.2. Vitriimer network synthesis and characterization

8 Once the prepolymers were prepared, vitrification was performed by simple solution casting, as
 9 seen in Figure S3. Two different cross-linkers were used. TREN, a small trifunctional molecule
 10 and Priamine, a difunctional vegetable oil-based molecule with relatively longer arms, are shown
 11 in Figure 3. Due to the associative nature of transamination, a stoichiometric imbalance is required
 12 to have an effective cross-linking exchange^{13,23,34,75}. However, the effects of cross-linking ratio on
 13 the rheological properties and dimensional stability of vitrimers have generally been limited^{6,34,}
 14 ^{38,76}. Therefore, we prepared networks with two different ratios of amine to β -ketoester for each
 15 cross-linking system to test for sensitivity. We were able to study the mechanical and rheological
 16 properties of the resulting vitrimers over a wide range of cross-linking densities by decoupling the
 17 structure and composition of the prepolymers from the nature and ratio of the cross-linkers.

18



12
13 **Figure 3.** Cross-linking of MyrAA-20-GMA-5 prepolymer with Priamine or TREN. Both
14 dynamic and static cross-links are present, enabling exchange and incorporation of shape memory
15 behaviour.

16
17 **3.3. Swelling test**

18 Due to the associative nature of the reversible cross-links in vitrimers, the networks do not dissolve
19 in solvents but swell^{17,37,77,78}. Indeed, this was evident for all synthesized vitrimers. The results
20 of swelling tests for various networks and solvents are summarized in Table 3. A compromise
21 between the gel content and swelling ratio was observed. Swelling ratio increased with looser
22 networks by shifting from TREN to Priamine. Expectedly, MyrAA-30-T-1, with the tightest
23 network, had the lowest swelling ratio while MyrAA-10-P-0.7 exhibited the highest one, as it had
24 the lowest β -ketoester concentration and higher free amine chain ends (β -ketoester/ $\text{NH}_2 = 0.7$).
25 Also, MyrAA-20-GMA-5-P-0.7 showed an intermediate value of cross-linking density between
26 MyrAA-20-P-0.7 and MyrAA-30-P-0.7 as expected.

1 **Table 3.** Swelling results of various vitrimers in toluene and gel content of MyrAA-20-T-0.7 in THF

Vitrimer	MyrAA-30 -T-1	MyrAA-30 -T-0.7	MyrAA-30 -P-1	MyrAA-30 -P-0.7	MyrAA-20 -P-0.7	MyrAA-10 -P-0.7	MyrAA-20-GMA-5 -P-0.7
Gel Content*	95%	95%	95%	93%	91%	87%	96%
Swelling ratio*	202%	235%	242%	261%	361%	692%	294%
Solvent	THF	Toluene	Chloroform	DMF	Methanol		
Gel Content**	92%	89%	91%	93%	93%		

2 * in toluene

3 ** Tests done with MyrAA-20-T-0.7

4

5 The cross-link densities (ν_e) of equilibrated swollen networks were estimated using the Flory-

6 Rehner equation (eq 1):

$$7 \quad \nu_e = -\frac{\ln(1-V_r) + V_r + \chi_{12} V_r^2}{V_s \left(V_r^{\frac{1}{3}} - \frac{V_r}{2} \right)} \quad (\text{eq 1})$$

8 in which V_s is the molar volume of solvent (106.5 cm³/mol for toluene⁷⁹) and V_r is the volume

9 fraction of polymer network in the swollen sample, calculated using equation 2)^{80,81}. χ_{12} is the

10 Flory-Huggins polymer-solvent interaction parameter and is estimated using the Flory-Hildebrand

11 equation (eq. 3)⁸¹.

$$12 \quad V_r = \frac{\frac{m_2}{\rho_2}}{\frac{m_1}{\rho_1} + \frac{m_2}{\rho_2}} \quad (\text{eq 2})$$

$$13 \quad \chi_{12} = \frac{V_s}{RT} (\delta_s - \delta_p)^2 \quad (\text{eq 3})$$

14

15 Here, m_1 and m_2 are the mass of the swollen and vacuum dried samples and δ_s and δ_p are the

16 solubility parameters of the solvent and polymer^{55,82}. δ_p of different prepolymers were either taken

17 from the literature or estimated using the group contribution method of Hoftyzer and van Krevelen

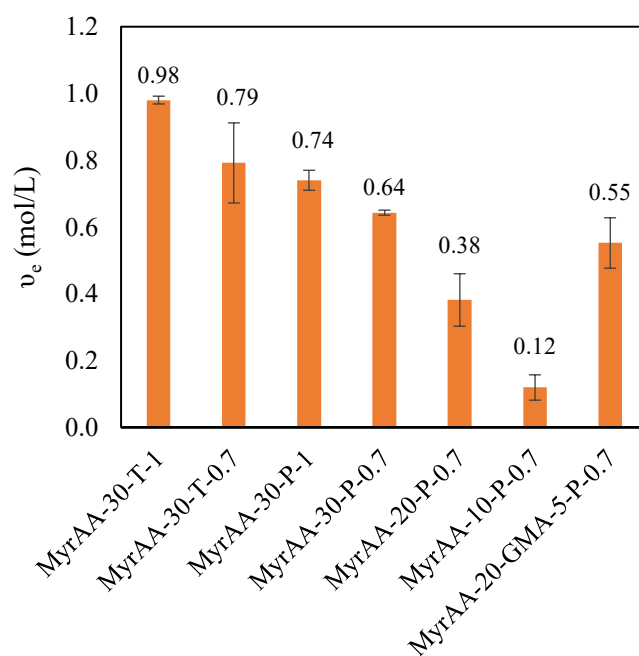
18 with a weighted average of different comonomers using the volume fraction^{67,83}. See section S5 in

19 the Supporting Information for the details of calculations. Figure 4 compares the cross-linking

20 density of the various networks studied ranging between the two extremes. As expected, the

21 sample with highest AAEMA content and a balanced β -ketoester : amine ratio exhibited the

1 highest cross-linking density of 0.98 mol/L. In contrast, MyrAA-10-P-0.7 which had the lowest
2 AAEMA content and was cross-linked with excess Priamine expectedly showed lowest cross-
3 linking density of 0.12 mol/L. This trend correlates with the results from the DSC analyses and the
4 shift in the T_g s of the vitrimers discussed in section 2.4.



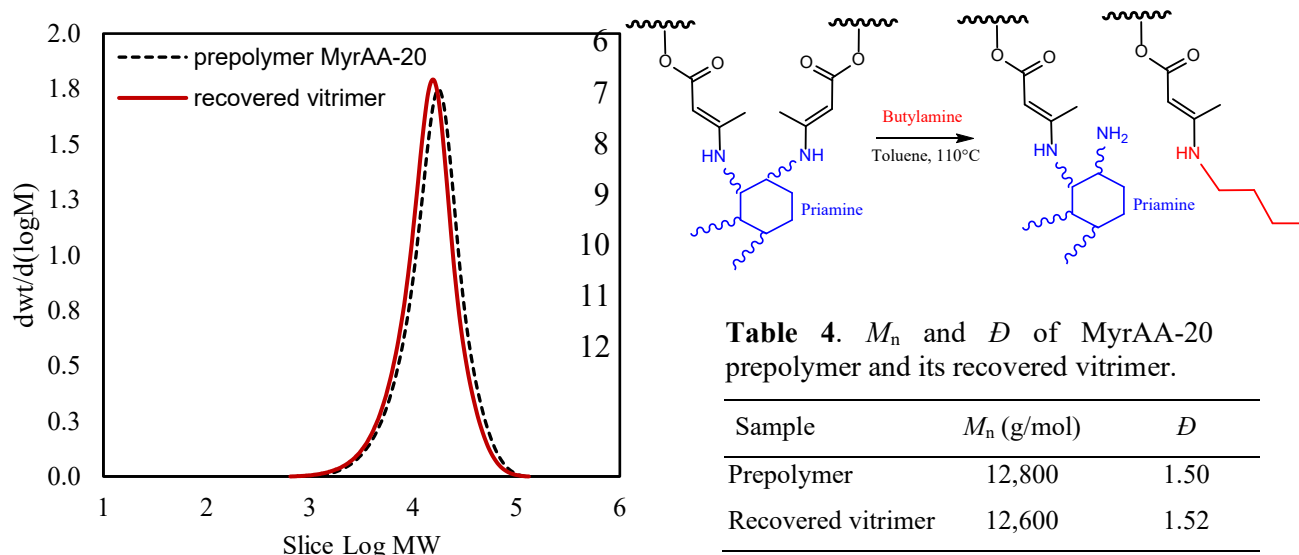
5
6 **Figure 4.** Comparisons of the cross-link density of various networks from highest to lowest,
7 calculated using the Flory-Rehner equation and swelling tests in toluene. A monotonic rise in
8 cross-linking density was observed with increasing AAEMA content and balancing the
9 stoichiometric cross-linking ratio.

10
11

12 **Network disintegration and polymer recovery**

13 Considering the dynamic nature of transamination in vinylogous urethanes, we hypothesized that
14 by adding an excess amount of a monofunctional amine, the network can be disintegrated, and the
15 prepolymer be chemically recovered^{23,84}. Thus, MyrAA-20-P-0.7 with toluene and excess
16 butylamine were added to a vial and sealed. Interestingly, the network did not dissolve after 24hr
17 at room temperature; however, once the vial was placed in an oven at 110 ± 5 °C the vitrimer was

1 fully dissolved in a few hours. Figure 5 and Table 4 compare the GPC traces and molecular weights
 2 of MyrAA-20 prepolymer and MyrAA-20-P-0.7 after disintegration and chemical recovery. These
 3 results confirm that the vitrimer processing, shaping, and chemical recovery of the prepolymer did
 4 not significantly degrade the polymer backbone.

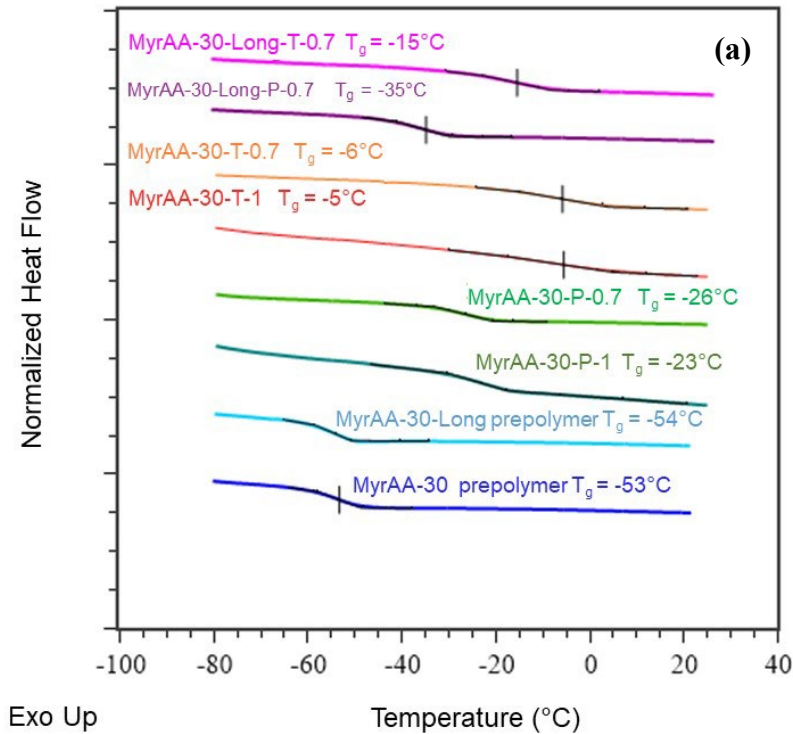


18 The DSC traces of the MyrAA-30 prepolymer and its associated vitrimers are shown in Figure 6.a.
 19 A clear shift towards higher T_g s was observed after the network formation. Vitrimers cross-linked
 20 with TREN exhibited T_g s that were about 20 °C higher than those cross-linked with Priamine. This
 21 can be attributed to the higher cross-linking density of the TREN-based networks. However, it
 22 appears that changing the β -ketoester : amine ratios did not have a significant impact on the T_g s.
 23 Similar shift towards higher T_g s was observed for vitrified MyrAA-30-Long. Interestingly,
 24 although prepolymers of both MyrAA-30 and MyrAA-30-Long had similar T_g s, vitrified MyrAA-
 25 30-Long -T-0.7 had a T_g that was about 10 °C lower than that of the vitrified MyrAA-30-T-0.7.

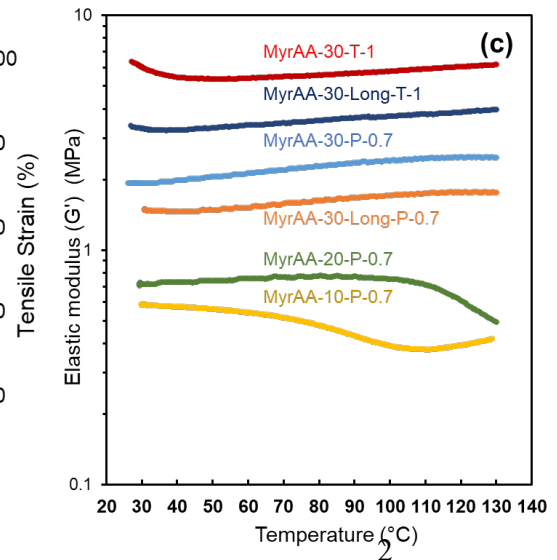
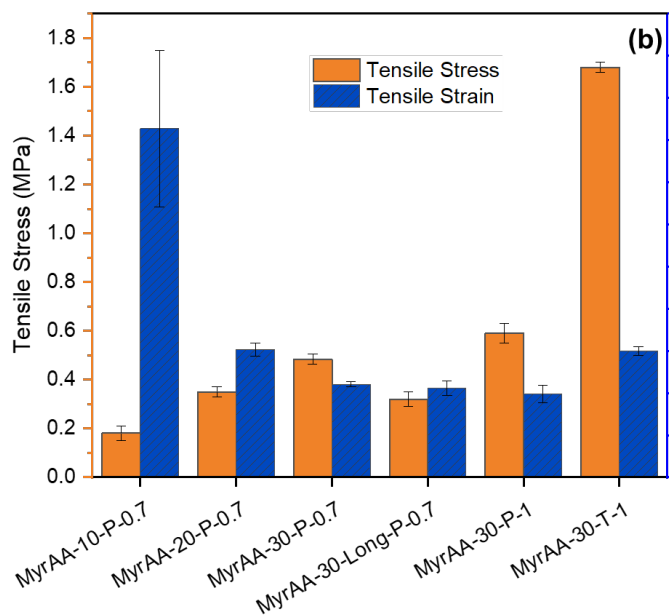
1 One possible explanation for this is that there may have been a compositional drift in the
2 prepolymers during the synthesis, resulting in the formation of longer Myr-rich sequences in the
3 chains of MyrAA-30-Long, as seen in section 3.1 and Figure S7. Determination of reactivity ratios
4 for this system is underway to verify if compositional drift is significant.

5
6 Figure 6.b illustrates the results of tensile tests performed with the various vitrimers. The tensile
7 strength at break of the vitrimers systematically increased by increasing the AAEMA content in
8 the copolymer. For samples cross-linked with excess difunctional amine (P-0.7), an increase in
9 tensile strength from MyrAA-10-P-0.7 with 0.18 ± 0.03 MPa to MyrAA-30-P-0.7 with $0.48 \pm$
10 0.03 MPa was seen. Simultaneously, the opposite trend was observed for samples' elongation at
11 break, as it decreased from $82.7 \pm 18.6\%$ for MyrAA-10-P-0.7 to $22.5 \pm 0.5\%$ for MyrAA-20-P-0.7.
12 In addition, The maximum tensile strength of 1.68 ± 0.02 MPa was observed for MyrAA-30-T-1.
13 From Figure S19, it is evident that replacing the diamine cross-linker with the triamine one,
14 resulted in the formation of stiffer materials in case of MyrAA-20-P-0.7 and MyrAA-20-T-0.7. A
15 similar trend was observed by DMTA with a systematic increase in modulus from MyrAA-10-P-
16 .07 to MyrAA-30-T-1. The tensile data closely follow the results of the swelling tests and cross-
17 linking density calculations. These findings show that vitrification can be used as an effective tool
18 to modulate the mechanical properties of terpene-based rubbers.

19



1



3

4 **Figure 6. a)** DSC traces of MyrAA-30 and MyrAA-30-Long prepolymer and their networks cross-
 5 linked with two ratios of TREN and Priamine; vitrification increased the glass transition
 6 temperature; **b)** Tensile data of various prepolymers cross-linked with Priamine with 0.7 to 1, and
 7 TREN with 1:1 β -ketoester: amine ratios. Increasing the network cross-linking density
 8 systematically reduced the elongation at break and increased tensile strength; **c)** representative
 9 DMTA data, elastic modulus and rubbery plateau of the vitrimers increased with cross-linking
 10 concentration.

1 **3.5. Rheological properties**

2 **Stress-relaxation and creep**

3 The recyclability of vitrimers is directly influenced by the exchange rate of the dynamic bonds due
4 to their associative nature. The dynamic cross-link exchanges facilitate rearrangements in the
5 network topology, segmental healing, and reformation of a continuous material
6 macroscopically^{13,37}. We carried out stress-relaxation experiments to investigate the flow behavior
7 of the vitrimers and quantify the timescale of the conformational rearrangements. Figure 7
8 compares the normalized stress-relaxation spectra of various prepolymers vitrified with an excess
9 amount of Priamine, P-0.7, at 130 °C. Increasing the AAEMA content systematically slowed down
10 the stress-relaxation rate of the vitrimers which is in line with the networks' cross-linking density.
11 Networks with 10 and 20 mol% AAEMA content showed fast and complete relaxation. Moreover,
12 increasing the molecular weight of the prepolymer, in the case of MyrAA-30-Long-P, beyond the
13 M_e , further slowed down the stress relaxation which suggests some restrictions in conformational
14 rearrangements due to physical chain entanglements. Furthermore, addition of static cross-links
15 via epoxy groups i.e., MyrAA-20-GMA-5, resulted in a significant increase of stress relaxation
16 time with a portion of the stress never being fully relaxed after 1000 seconds.

17 Figure 8.a illustrates a typical normalized stress-relaxation i.e., $G(t)/G(0)$, curve for
18 MyrAA-30-T-0.7 in the temperature range of 90 to 130 °C. According to the single element
19 Maxwell viscoelastic model, $G(t)/G(0) = \exp(-t/\tau^*)$, the characteristic relaxation time (τ^*) is
20 identified at the time when the normalized relaxation modulus reaches the value of e^{-1} (≈ 0.37)⁸⁵.
21 However, with increasing cross-linking density some deviations from the ideal Maxwellian
22 behavior were observed. To capture these deviations, a stretched exponential decay model was

1 used according to equation 4. which permits the extraction of (τ^*) for samples that do not fully
2 relax past the e^{-1} point:

$$3 \quad \frac{G(t)}{G(0)} = e^{-\left(\frac{t}{\tau^*}\right)^\beta} \quad (\text{eq. 4})$$

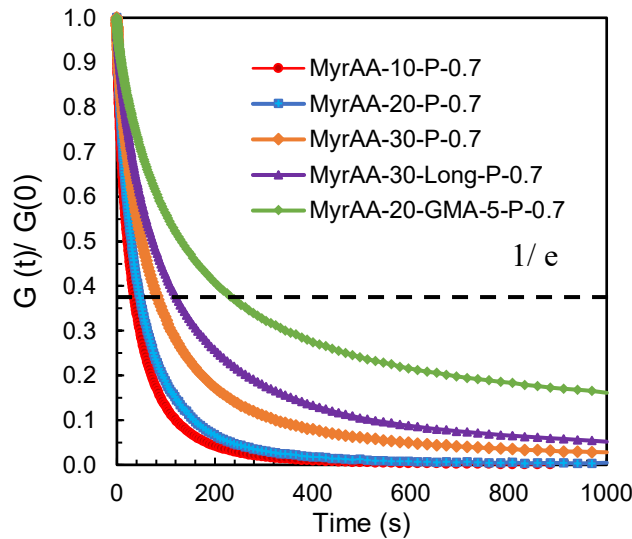
4 where, $G(t)$ and $G(0)$ are the relaxation moduli at time t and 0, τ^* is the characteristic relaxation
5 time and β ($0 < \beta \leq 1$) is a parameter related to the breadth of the relaxation distribution. For
6 MyrAA-30-T-0.7, β varies between 0.50 and 0.69 showing deviations from ideal Maxwellian
7 behavior^{6,16,85}. See Table S3 for detailed τ^* and β values obtained by curve-fitting. As suggested
8 by Leibler et al., since a chemical reaction is responsible for the dynamic exchanges in cross-
9 linking, an Arrhenius relationship can be used to model the gradual decrease of viscosity with
10 increasing temperature according to equation 5^{6,74}.

$$11 \quad \ln \tau^* = \frac{E_a}{RT} + \ln(\tau_0) \quad (\text{eq. 5})$$

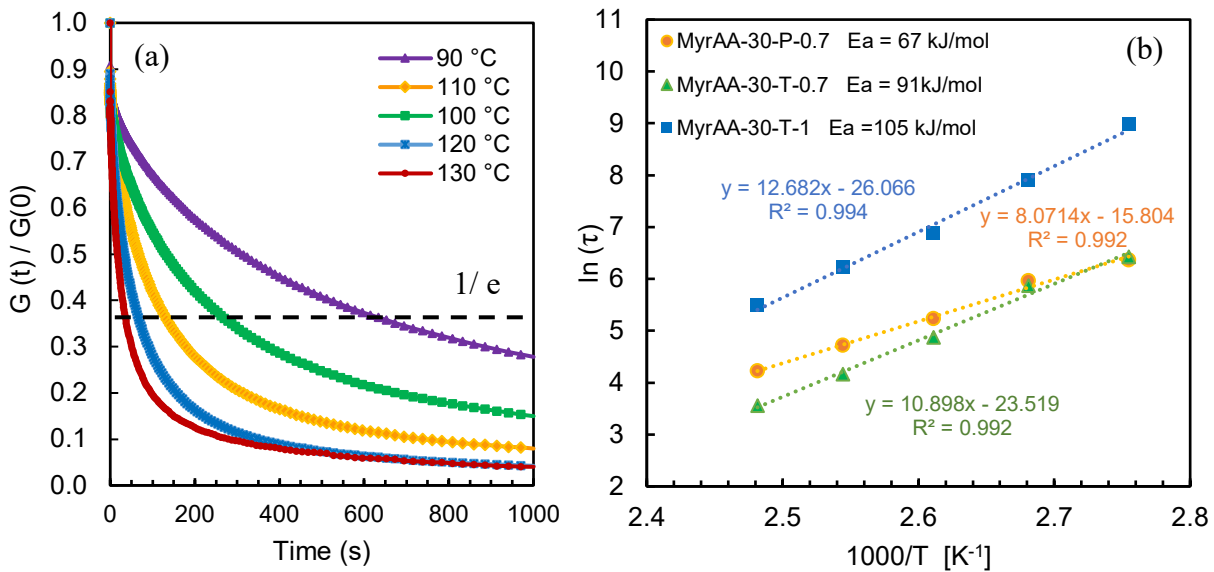
12 Here, E_a is the viscous flow activation energy, R is the universal gas constant, T is temperature,
13 and τ_0 is the Arrhenius pre-factor. The calculated E_a for MyrAA-30-P-0.7 and MyrAA-30-T-0.7
14 were 67 and 91 kJ/mol respectively, which is consistent with the literature; the observed increase
15 in the activation energy can be attributed to the different nature of the cross-linkers and the higher
16 T_g of the latter network^{6,34}. Figure 8.b compares the Arrhenius plots of MyrAA-30-T-0.7 (with
17 0.7:1 β -ketoester : NH_2 ratio) and MyrAA-30-T-1 (with 1:1 β -ketoester : NH_2 ratio). In the latter
18 case, decreasing the concentration of amine groups to a balanced stoichiometric ratio increased the
19 E_a to 105 kJ/mol. Typically, higher values of E_a indicate a higher energy barrier of bond exchange
20 which leads to a rapid decrease of viscosity upon increasing temperature. In contrast, vitrimers
21 with low E_a show less pronounced viscosity change with temperature alterations¹³. This trend
22 agrees with the observed flow behavior of MyrAA-30-P-0.7, MyrAA-30-T-0.7, and MyrAA-30-
23 T-1. A practical manifestation of this phenomenon can be utilized in the design of vitrimers with

1 enhanced dimensional stability at service temperatures and yet rapid viscosity decay with
2 increasing temperatures which enables their fast processability^{13,17,78}. Figure S17 compares the
3 Arrhenius plots of MyrAA-30-P-0.7 and MyrAA-30-Long-P-30; a similar trend was observed with
4 a slight increase of E_a value from 67 to 76 kJ/mol for the respective vitrimers.

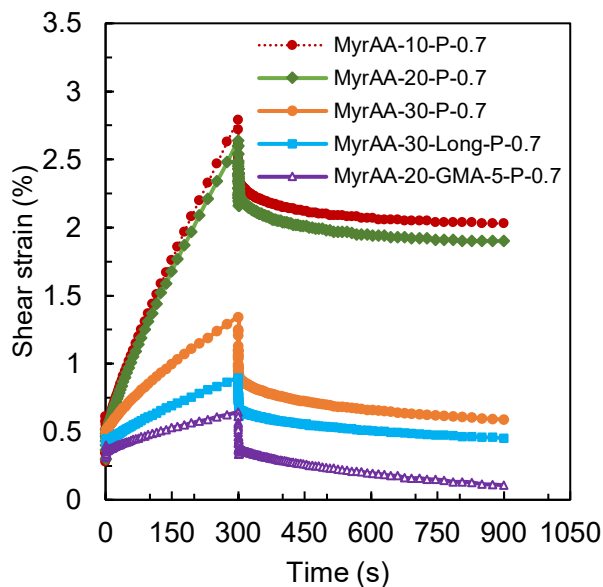
5 Figure 9 shows the results of creep-recovery experiments for 5 different prepolymers vitrified with
6 excess β -ketoester : amine ratio of 0.7:1. As the cross-linking density increased, the creep
7 systematically decreased. Networks with copolymer having 10 and 20 mol% AAEMA content
8 exhibited similar creep behavior with 2.8% and 2.6% shear strain at 300 s followed by some limited
9 strain recovery of 27% and 28%, respectively. Further increasing the AAEMA content in the
10 copolymer to 30 mol%, MyrAA-30-P-0.7, led to lower shear strain of 1.3% at 300 s which had
11 52% lower deformation compared to MyrAA-10-P-0.7. In addition, a higher creep recovery of
12 56% at 900 s was observed for MyrAA-30-P-0.7. At the 300 s point, the creep-recovery analysis
13 of the MyrAA-30-Long-P-0.7, with $M_n \geq M_e$, revealed a lower deformation of about 49%
14 compared to its counterpart, MyrAA-30-P-0.7, with a shorter backbone and $M_n < M_e$. Furthermore,
15 we studied the influence of additional static cross-links in MyrAA-20-GMA-5-P-0.7. The dual
16 cross-linked network showed the lowest deformation until 300 s combined with the highest creep
17 recovery of 83% at 900 s. The high creep recovery in MyrAA-20-GMA-5-P-0.7 indicates that less
18 permanent deformation had occurred in the sample. This can be credited to the presence of static
19 cross-links which restricts network strand deformation^{26,86}. The results of creep-recovery are in
20 good agreement with those of stress-relaxation tests, showing that dimensional stability of the
21 vitrimers can be tailored by cross-linking density, increasing primary chain length, and addition of
22 physical or chemical, static cross-links^{25,26,75,86}.



1
2 **Figure. 7** Comparison of stress-relaxation behavior of various pre-polymers vitrified with an
3 excess amount of Priamine (P-0.7) at 130 °C. Increasing AAEMA content and molecular weight
4 of prepolymer ($M_n > M_e$) as well as incorporation of static cross-links systematically increased the
5 relaxation time.



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18 **Figure 8. a)** Comparison of stress-relaxation behavior of MyrAA-30-T-0.7 from 90 to 130 °C. **b)**
19 Arrhenius relationship between relaxation time and temperature obtained from the stress relaxation
20 experiment of the MyrAA-30-T-1 (with 1:1 β -ketoester : NH_2) and MyrAA-30-T-0.7 (with 0.7 :
21 1 β -ketoester : NH_2) vitrimers using stretched exponential decay fit.



1
2 **Figure 9.** Creep-recovery data of various vitrimers cross-linked with excess Priamine (P-0.7).
3 Creep was decreased by increasing the cross-linking density (AAEMA content), increasing the M_n
4 of prepolymer ($>M_c$), and incorporating 5 mol% GMA to impart dual static and dynamic networks.

6 2.1. Recycling of vitrimers

7 Vitrimer reprocessability and ability to be remolded into new materials after curing is one of the
8 most important properties of such polymer networks. This phenomenon is a direct consequence of
9 the dynamic nature of the cross-links. Particularly, processability of vinylogous urethanes cured
10 with TREN and Priamine were well-established by others^{6,22,23,34,37}. Therefore, we mimicked
11 similar recyclability tests by cutting the processed MyrAA-20-T-0.7 into small pieces and re-
12 processing them via hot-pressing for 3 cycles. Figure 10 shows pictures of reprocessed and cut
13 MyrAA-20-T-0.7 samples. We performed the compression molding at a relatively low temperature
14 of 110 °C for 50 ± 5 min to minimize possible side reactions or degradation, and even though this
15 temperature is lower than the values reported in the literature, well-formed samples were achieved.
16 In addition, vitrified polymers showed high isothermal stability in a TGA test at 120 °C under
17 nitrogen flow for 6 h (see Figure S11).

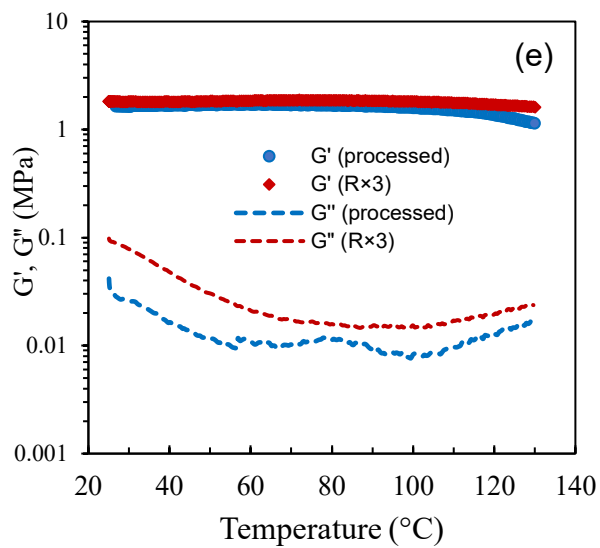
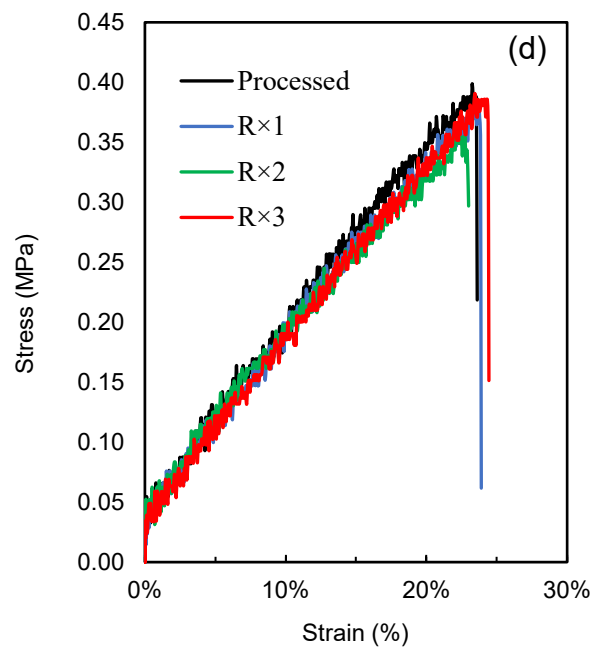
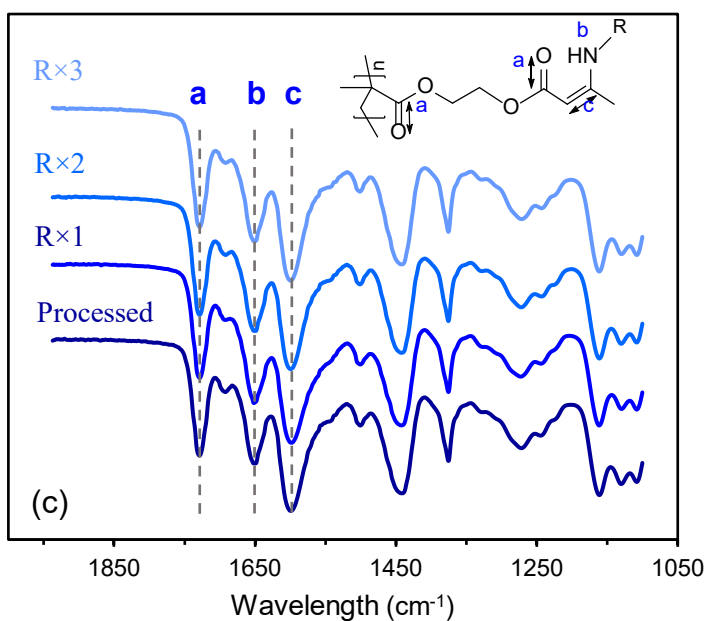
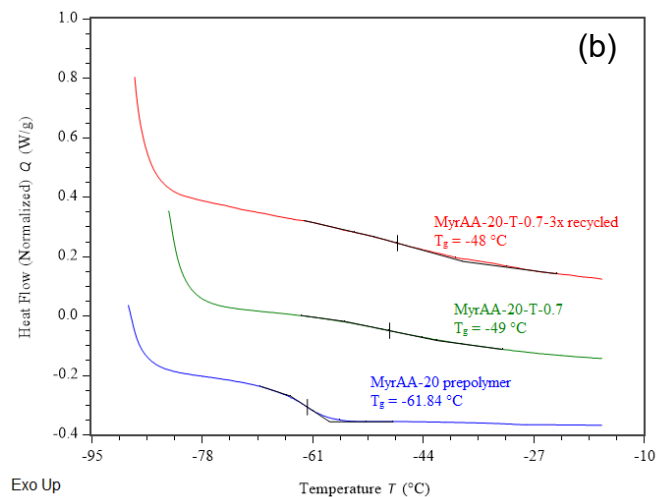
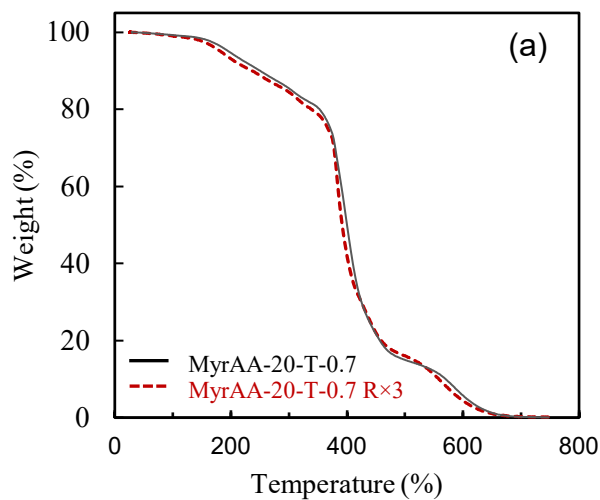
18 Figure 11 compares the thermomechanical and chemical properties of the original MyrAA-20-T-
19 0.7 and those of the same sample after 3 recycling processes. ATR-FTIR spectra of the sample
20 after each reprocessing cycle showed peaks attributed to the vinylogous urethanes at 1600 cm⁻¹,

1 indicating N-H bending, and 1655 cm^{-1} , indicating C=C stretching, were retained and no other
2 noticeable degradation was observed.
3 Thermal analyses by TGA and DSC shows that thermal properties of the vitrimer essentially stayed
4 intact after reprocessing. The onset degradation at $360\text{ }^{\circ}\text{C}$ with $T_{5\%} = 196\text{ }^{\circ}\text{C}$ and $T_g = -48 \pm 1\text{ }^{\circ}\text{C}$
5 was observed for the original and the recycled ($3\times$) samples. DMTA analyses showed that the
6 rubbery plateau was retained after $3\times$ reprocessing with elastic modulus (G') of $1.82 \pm 0.5\text{ MPa}$.
7 Most importantly, the tensile properties remained intact after each processing cycle. Figure 11.d
8 illustrates the stress-strain curves of the MyrAA-20-T-0.7 of the originally processed sample and
9 its three consecutive reprocessed ones. Table 5 summarizes the results of tensile tests of
10 reprocessed samples; respectively, average stress and elongation at break of 366 kPa and 21.7%
11 were recorded for the (re)processed samples.

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Figure 10. Reprocessing of poly(myrcene)-based vitrimers. Cured and processed samples were cut into small pieces and hot-pressed for 3 cycles.



1 **Figure 11.** Properties of reprocessed MyrAA-20-T-0.7 vitrimer after 3 cycles: a) TGA traces,
 2 thermal decomposition temperature with onset of 355 ± 5 °C did not change. b) DSC traces of
 3 MyrAA-20 prepolymer (blue line) with T_g of -61.8 °C, pristine processed Myr-AA-20-T-0.7
 4 vitrimer (green line), and Myr-AA-20-T-0.7 vitrimer after 3 reprocessing cycles (red line); T_g was
 5 retained at $\sim -48 \pm 1$ °C after vitrification and reprocessing. c) ATR-FTIR spectra, bands of N-H
 6 bending at 1600 cm^{-1} and C=C stretching at 1655 cm^{-1} corresponding to the vinylogous urethane
 7 cross-links retained. d) Stress-strain curves did not change e) Semi-logarithmic DMTA traces of
 8 originally processed vitrimer and after 3 reprocessing cycles (R×3), the rubbery plateau in elastic
 9 (G') and loss (G'') was retained.

10

11 **Table 5.** Tensile properties of reprocessed MyrAA-20-T-0.7

MyrAA-30-T-0.7	Stress at break (kPa)	Strain at break (%)	Young's Modulus (MPa)
Original Processed	375.7 ± 22.7	22.1 ± 0.8	1.53 ± 0.04
Reprocessed ×1	362.6 ± 29.0	22.6 ± 1.4	1.45 ± 0.02
Reprocessed ×2	348.3 ± 16.3	20.0 ± 2.1	1.54 ± 0.14
Reprocessed ×3	377.7 ± 52.4	22.3 ± 2.4	1.52 ± 0.09

12

13 An interesting consequence of dynamic cross-linking is the ability of different cured samples to
 14 be welded together without using significant pressure. Inspired by Liu et al., we performed a
 15 welding experiment by dabbing 2-3 drops of butylamine on top of two different rectangular
 16 samples each with a size and weight of about $1.5 \times 1 \times 0.1$ cm (length×width×thickness) and 0.15 g
 17 respectively⁸⁴. Afterwards, the samples were quickly combined and placed in an oven at 115 °C
 18 for 20 min. An empty NMR tube was placed on top of the samples to physically secure them, and
 19 no extra pressure was applied. The welded sample could resist up to 23.5 g, which is more than 60
 20 times its weight. Control samples without any butylamine could not resist any external weight after
 21 a similar welding procedure was applied. Thus, it appears that butylamine caused welding by either
 22 solvent welding via swelling of the surfaces and/or possible liberation of some functional groups
 23 on the vitrimers and promotion of transamination between the two surfaces which led to a
 24 relatively fast and effective welding.

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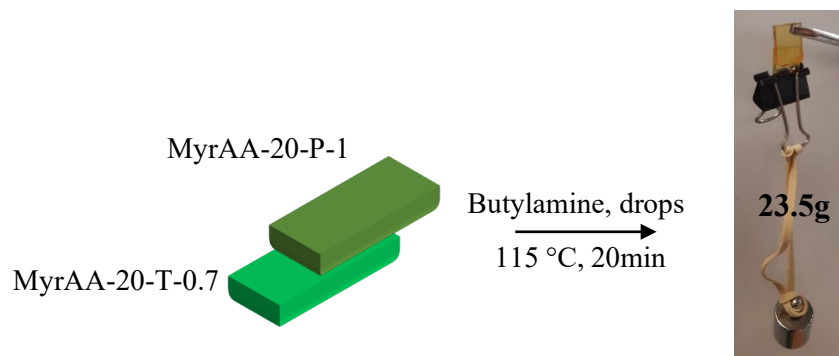
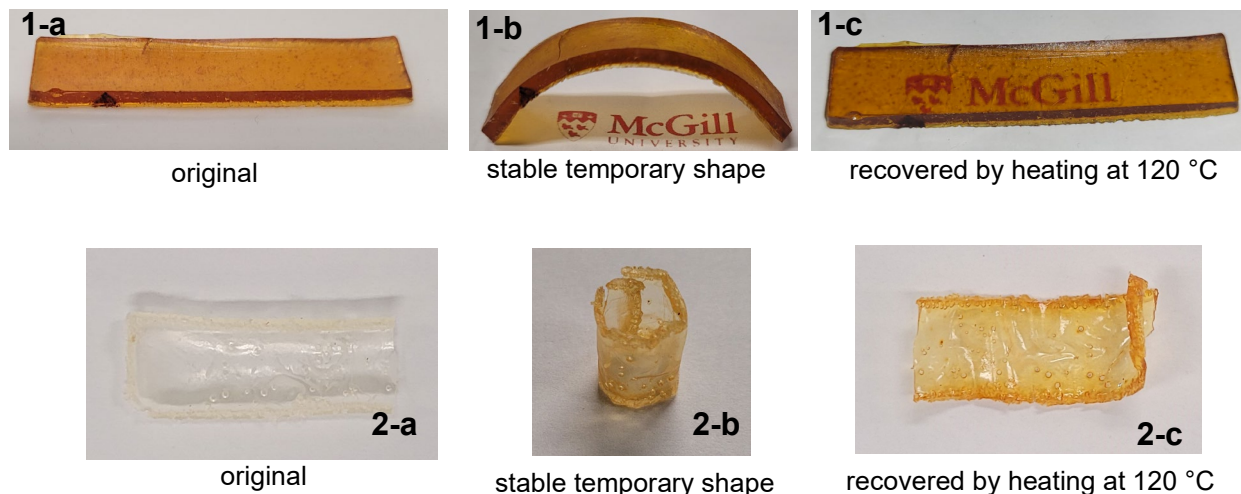


Figure 12. Welding of two different vitrimeric samples: MyrAA-20-P-1 and MyrAA20-T-0.7. Samples were dabbed with a few drops of butylamine at the interface and then heated for 20 min under no added pressure.

2.2. Shape memory

As mentioned in section 3.5, we originally synthesized the dual-functionalized MyrAA-20-GMA-5 prepolymer to impart both static and dynamic cross-links with the goal of reducing creep. Additionally, we hypothesized that shape memory effects can be seen in this material as static epoxy-amine cross-links can “memorize” the permanent shape of the vitrimer while the dynamic vinylogous urethane can retain the temporary shape. Therefore, we first vitrified the sample in a rectangular mold, i.e., the permanent shape. Afterwards, the sample was heated and carefully bent and reshaped, the temporary shape, and kept in an oven at 110 °C under vacuum for 1 h. This was followed by cooling of the sample under stress. The resulting sample’s shape, Figure 13.b, was temporarily stable, at least for 48 h, until it was heated again in an oven at 120 °C. The full shape recovery was achieved in about 4 h. While good shape fixity and shape recovery ratio was observed, the rate of shape recovery was slow. These results are in line with the observed slower stress-relaxation, Figure 7, and full creep-recovery, Figure 9, of MyrAA-20-GMA-5. Although a simple shape recovery is reported, this initial exploration combining shape recovery with dynamic

1 networks was very promising and more in-depth studies on exploring the interplay of the
2 chemistries to tailor recovery times are underway.



13 **Figure 13.** Shape memory effect of 2 different MyrAA-18-GMA-8-P-0.7 samples. a) original
14 shape was formed after vitrification as described in section 2.3 b) temporary shape was formed
15 after heating to 110 °C and cooling under stress; the shape was stable at room temperature for at
16 least 24hr c) recovery of the original shape by reheating to 120 °C for 4 h.

19 3. Conclusions

20 Development of elastomers from renewable feedstocks with enhanced recyclability is a step
21 forward towards a more sustainable rubber industry. We have demonstrated a straightforward
22 approach to synthesize bio-based vitrimers using commercially available and relatively
23 inexpensive myrcene with catalyst-free vinyllogous urethane chemistry for the first time. Statistical
24 prepolymers of Myr and AAEMA were prepared in a controlled fashion using NMP and afterwards
25 cross-linked with biobased Priamine or TREN via solution casting and compression molding. The
26 final mechanical and rheological properties of the networks could be effectively tailored by

1 changing the prepolymers' composition, molecular weight, and the nature and ratio of the cross-
2 linkers. The rubbery networks exhibited effective reprocessability by mechanical grinding and hot
3 pressing at 110 °C in less than 60 min for at least 3 cycles. ATR-FTIR confirmed retention of the
4 network while no change in the T_g , onset of decomposition, storage modulus as well as elongation
5 and stress at break was observed after reprocessing. Although vitrimer-like insolubility of the
6 networks in different solvents was confirmed, prepolymers could be chemically recovered by
7 addition of excess monofunctional amines at 110 °C without degradation, confirmed by GPC.
8 Also, Myr-based vitrimers could be welded to each other by using a few drops of n-butyl amine at
9 115 °C in 20 min. Increasing the prepolymer's molecular weight beyond its entanglement limit
10 ($M_n > M_e$) led to decreased creep. In addition, dual networks with static and dynamic cross-links
11 were formed by incorporation of 5 mol% epoxy-based GMA in the prepolymer. The resulting
12 network exhibited significant reduction in creep in addition to shape memory effects.
13 Adopting vitrimer chemistry is a versatile and yet simple tool in tailoring the thermomechanical
14 properties of poly(My) with excellent reprocessability. We envision that this approach can be
15 used as a platform to develop customized recyclable biobased elastomers with applications in
16 rubbers, smart materials, wearable electronics, to name but a few.

17

18 **4. Associated Information**

19 Synthetic route, photographs of vitrification steps, ^1H NMR of prepolymers, GPC traces, DSC,
20 calculation of solubility parameters, TGA, swelling tests, rheological data, ATR-FTIR spectra are
21 found in the Supporting Information.

22

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6 7 **6. References**

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