

Aggregation and Deposition of Engineered Nanomaterials in Aquatic Environments: Role of Physicochemical Interactions

A Critical Review revised and resubmitted to:
Environ. Sci. Technol.

June 2, 2010

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Abstract

The ever-increasing use of engineered nanomaterials will lead to heightened levels of these materials in the environment. The present review aims to provide a comprehensive overview of current knowledge regarding nanoparticle transport and aggregation in aquatic environments. Nanoparticle aggregation and deposition behavior will dictate particle transport potential and thus the environmental fate and potential ecotoxicological impacts of these materials. In this review, colloidal forces governing nanoparticle deposition and aggregation are outlined. Essential equations used to assess particle-particle and particle-surface interactions, along with Hamaker constants for specific nanoparticles and the attributes exclusive to nanoscale particle interactions are described. Theoretical and experimental approaches for evaluating nanoparticle aggregation and deposition are presented, and the major findings of laboratory studies examining these processes are also summarized. Finally, we describe some of the challenges encountered when attempting to quantify the transport of nanoparticles in aquatic environments.

Introduction

Featuring unique electronic, optical, thermal and photoactive properties, nanomaterials are ideal candidates for a multitude of current and potential industrial applications (1, 2). With the rising demand for such materials and an increase in their production, nanoparticle release into the environment is inevitable and exposure more likely. Once present in the biosphere, the novel particles may interact with humans and organisms in an unforeseen fashion (3). Thus, it is essential to elucidate the effects such materials can have on both human and environmental health as a result of exposure via different routes.

Exposure can occur at the production, consumption, and disposal stages of particle life (4, 5). Particles either enter the environment directly (e.g., due to unintentional release or for remediation purposes), or indirectly by way of waste incineration plants, sewage treatment plants, and landfills (4, 5). Once released, the particles will interact with each other and with their surrounding environments (be it in air, water or soil) (6, 7). While particle release occurs within all of these environments, the present review focuses on nanoparticle deposition and aggregation in aquatic systems.

When released into aquatic environments, nanoparticle behavior is dependent on particle-specific properties (e.g., size, shape, chemical composition, surface charge, and coating), particle state (free or matrix incorporated), the surrounding solution conditions (e.g., pH, ionic strength, ionic composition, natural organic matter content), and hydrodynamic conditions (1, 2). Such factors are important in determining whether particles aggregate with other particles or deposit onto various environmental surfaces (2). Recognizing which interactions particles experience under different conditions is essential in predicting their fate in the environment and thus likelihood of exposure.

Under conditions resulting in favorable (non-repulsive) particle-surface interactions, nanomaterials will be less likely to travel extensive distances (8). The opposite holds under unfavorable (repulsive) deposition conditions (8). Additionally, an understanding of particle-particle interactions is also imperative when considering particle transport, as aggregation greatly affects particle behavior in the natural environment (2). Changes in particle size and shape resulting from aggregation may significantly alter transport potential, as well as nanomaterial reactivity and toxicity (1). Whereas nanoparticle transport through aquatic environments is expected to be dominated by random

Brownian diffusion (9, 10), an increased particle size imparted by aggregation may result in particle-surface collisions due to gravitational sedimentation and interception (2, 9). In addition, nanoparticles may associate and aggregate with other naturally-occurring substances, such as organic matter, naturally occurring colloidal matter, and dissolved molecules (e.g. phosphates and sulfates) (1). Finally, nanoparticles may experience chemical transformations when suspended in natural aquatic environments, including oxidation/reduction, partial dissolution, hydrolysis, and biological degradation (1, 11). Whether such associations and transformations facilitate nanoparticle transport or augment nanoparticle deposition has not been well examined and will depend on the properties exhibited by the nanoparticles, other naturally-occurring materials and the environmental conditions.

Overall, it is essential to elucidate which physicochemical interactions govern particle-surface and particle-particle interactions under conditions representative of aquatic environments. While a great deal of work analyzing the behavior of micrometer-sized particles in various aquatic environments has been performed, limited data (and quantitative analysis) is available for nanosized particles, both in terms of aggregation (12-56) and deposition (15, 16, 20, 25, 44, 57-96). As a result, two key questions remain unanswered. First, how do specific particle and environmental properties affect deposition and aggregation? Second, are the current approaches and models used in quantifying colloidal interactions and transport applicable to nanomaterials?

This paper provides critical review and assessment of existing research and approaches examining the deposition and aggregation behavior of engineered nanomaterials in aquatic systems. First, colloidal forces central to nanoparticle deposition and aggregation, including traditional Derjaguin-Landau-Verwey-Overbeek (DLVO), non-DLVO, and nanoparticle-specific interactions are summarized. Next, theoretical and experimental approaches for evaluating nanoparticle aggregation and deposition under both favorable and unfavorable conditions are discussed. Finally, the challenges commonly faced when attempting to quantify the environmental transport of engineered nanoparticles are outlined.

Engineered Nanomaterials in Aquatic Systems: From “A”luminum to “Z”irconium

The presence of nanomaterials in the environment is not novel. Both fullerenes (C_{60}) and carbon nanotubes (CNTs) were discovered in 10,000-year-old polar ice cores (97). However, the current rise in anthropogenic nanomaterial production will result in heightened environmental levels of such products (4). Nanoparticle release into the biosphere will originate at both point sources (e.g., production sites, landfills, treatment plants) and nonpoint sources (e.g., release into the environment during use and consumption of nanomaterial-containing goods) (2, 4). Global production estimates for nanomaterials range from 350 and 500 tons/yr for CNTs and nano-silver (nAg), respectively, to 5,000 tons/yr for titanium dioxide (TiO_2) nanoparticles. Predicted environmental concentrations for these particle types have also been estimated, with soil concentration estimates ranging from 0.01 and 0.02 $\mu g/kg$ for CNTs and nAg , respectively, to 0.4 $\mu g/kg$ for $nTiO_2$ (4).

The intentional injection of nanoparticles into the subsurface for remediation purposes is an additional entry route into the environment (82). It has been demonstrated that nanoscale zero-valent iron ($nZVI$) can treat a variety of groundwater contaminants, including pesticides and chlorinated organic solvents (2). While a potentially excellent candidate for large-scale site remediation, the environmental transport, fate, and impact of such particles remains to be determined.

Anthropogenic nanomaterials consist of intentionally manufactured products (referred to as manufactured or engineered nanomaterials) and accidental byproducts resulting from wear, corrosion, waste, and combustion of bulk materials (5). A large variety of engineered organic (carbon-based) and inorganic (includes metallic, bimetallic, metal oxide, and semi-conductor based) particles are currently available. Table S1 in the Supporting Information presents a selection of commonly encountered nanomaterials and their key physicochemical characteristics. As can be noted in Table S1, current manufactured nanomaterials vary significantly in isoelectric point, shape, and composition, with particles containing elements ranging from Al to Zr. For a more extensive summary describing nanoparticles and their applications, refer to (1). Additionally (1, 4), the Woodrow Wilson International Center for Scholars has developed an extensive inventory of consumer products incorporating nanotechnology (<http://www.nanotechproject.org/>).

Colloidal Forces Governing Nanoparticle Deposition and Aggregation

Particle-particle interactions and particle-surface interactions play key roles in controlling the aggregation and deposition behavior of nanoparticles in aquatic environments. These interactions have traditionally been described by the DLVO theory of colloidal stability. However, non-DLVO forces such as steric, magnetic, and hydration forces can also play an important role in the aggregation and deposition of engineered nanomaterials.

Traditional Colloidal Interactions. The classical DLVO theory (98, 99) of colloidal stability describes the total interaction energy experienced by a nanoparticle when approaching another particle (in the case of aggregation) or a collector surface (in the case of deposition). According to the DLVO theory, the stability of nanoparticles suspended in an aqueous environment can be evaluated as the sum of van der Waals (VDW) and electrical double-layer (EDL) interactions. The resultant interaction energy (V_T), the sum of VDW and EDL interactions, determines the particle stability as the two surfaces approach one another.

VDW forces result from electrical and magnetic polarizations, yielding a varying electromagnetic field within the media and in the separation distance between the two surfaces. The evaluation of dispersion interactions proposed by Hamaker (100) is based on the assumption that the potential between two surfaces could be represented as the sum of the interactions between pairs of atoms located within the two surfaces (particle or collector). Equations to evaluate VDW interactions are presented in Table 1. In addition, the following relations are required to estimate the effect of an intervening medium “2” between two bodies of similar composition (“1”; eq 1) or of differing composition (“1” and “3”; eq. 2) in the case of deposition (8):

$$A_{121} = (A_{22}^{1/2} - A_{11}^{1/2})^2 \quad (1)$$

$$A_{123} = (A_{33}^{1/2} - A_{22}^{1/2})(A_{11}^{1/2} - A_{22}^{1/2}) \quad (2)$$

Here, A_{123} is the overall Hamaker interaction parameter for the deposition of a nanoparticle of composition “1” onto a surface of composition “3” when suspended in a medium “2”. In contrast, A_{121} is the overall Hamaker interaction parameter for the aggregation of two nanoparticles of composition “1” when suspended in a medium “2”. The Hamaker constants of “1”, “2”, and “3” in

vacuum — A_{11} , A_{22} , and A_{33} , respectively — are required for use in these equations. These are readily available for a variety of materials, e.g. (101, 102).

In aqueous environments, when particles approach each other (aggregation) or a surface (deposition), the overlap of the diffuse electric double layers results in electrostatic double layer interactions. Widely used equations for the most commonly encountered interaction geometries (i.e., two spherical particles or a spherical particle interacting with a planar surface) are presented in Table 1. These equations are based on the linear superposition approximation (LSA) method that applies for low surface potentials and symmetric electrolytes (103). The LSA is a useful compromise between the constant-charge approximation (CCA) and the constant-potential approximation (CPA), which are not likely to apply in practice.

Tables S2 and S3 provide a list of Hamaker constants corresponding to several common nanomaterials. When used with eq 4, the Hamaker constants presented in Table S2 serve in determining the VDW interactions between a particle and a collector surface (i.e., for deposition). The constants listed in Table S3 can be used with eq 7 to evaluate the VDW interaction between two particles (i.e., aggregation of particles). For the case where the Hamaker constant of a specific nanomaterial is not known, it may be evaluated using eqs 1 and 2.

Non-DLVO Interactions. Beyond the traditional colloidal interactions considered in the DLVO theory, a number of non-DLVO forces can also influence the stability of a nanoparticle suspension in aqueous environments. The most significant forces encountered by engineered nanomaterials in aqueous media include steric interactions, magnetic forces (for iron-based nanomaterials), and hydration forces.

Generalized expressions describing the extent of steric forces have been derived for particles with adsorbed layers of polymers or surfactants that might lead to steric repulsion. These expressions, also included in Table 1, are based on the Alexander-de Gennes theory (104, 105) that is used to evaluate the repulsive steric force and the Derjaguin approximation. Steric interactions can be particularly important for nanoparticles in natural and engineered aquatic environments, as most particles adsorb natural organic matter that is known to stabilize colloids (67, 83).

Certain nanomaterials, such as nano-sized iron, exhibit a magnetic dipole moment, even in the absence of an applied magnetic field (106). For these nanomaterials, the contribution of the magnetic force may dominate the total particle-particle interaction energy thereby leading to aggregation. Equation 9 represents the magnetic interaction energy between equally-sized particles of radius a_p (106):

$$V_M = -\frac{8\pi\epsilon_0 M^2 a_p^3}{9\left(\frac{h}{a_p} + 2\right)^3} \quad (9)$$

where all the variables are defined in the *Nomenclature* section.

Some nanoparticles may carry hydrophilic material or functional groups at their surface (e.g., proteins, polysaccharides) that can have significant amounts of bound water that may play a role in the interaction of such particles. The approach of two particles with hydrated surfaces will generally be hindered by an additional repulsive interaction. The range of this interaction is significant compared to the range of EDL repulsion and is expected to have an effect on nanoparticle stability, particularly at high ionic strength (107).

Unique Features of Interactions of Nanoscale Particles. Because of the small size of nanoparticles (less than 100 nm), their interaction with solid surfaces or other particles can be quite different than that of larger, micrometer-sized particles. These unique features of interaction of nanoscale particles can influence their transport, deposition, and aggregation in aquatic environments.

(a) **Greater influence of geochemical heterogeneities on deposition.** Geochemical heterogeneities are prevalent on mineral surfaces in subsurface aquatic environments (108, 109). Because of their small size, the interactions of nanomaterials in aquatic environments will be substantially influenced by patchwise geochemical heterogeneities (110). Such geochemical heterogeneities may be an important factor controlling the extent of nanoparticle transport in subsurface environments. The size of the patches relative to the size of the particles is an important factor. Nanoparticles may experience greater sensitivity to patch heterogeneity than micrometer-sized

particles because nanoparticles will interact with smaller patches. When the nanoparticles are smaller than the size of the patch heterogeneities, the particle deposition rate can be approximated by the patchwise heterogeneity model (108, 109). Similar arguments can be made regarding nanoparticle interaction with physical heterogeneities in the form of roughness.

(b) **Low energy barrier.** The kinetics of particle deposition and aggregation are dependent on the height of the energy barrier (8). Particles that overcome the energy barrier will deposit on a surface or aggregate with another particle in a deep primary energy minimum. The height of the energy barrier for deposition or aggregation is directly dependent on the size of the interacting particles, with smaller particles exhibiting much lower energy barriers (8, 62). Therefore, nanoparticles will deposit or aggregate more in primary minimum than micrometer-sized particles. It has been shown that nanoparticles that deposit in primary energy minima are less likely to be released from the surface following changes in solution chemistry, such as reduction of ionic strength or changes in solution pH (16).

(c) **Negligible secondary energy minimum.** At the ionic strength of typical natural waters, the interaction energy of particles greater than about 0.5 μm interacting with similarly charged particles or surfaces is characterized by a high energy barrier and a secondary energy minimum (91, 111). It has been shown that secondary energy minima play a critical role in the deposition and transport of particles greater than approximately 0.5 μm (69, 91). Such particles readily deposit in secondary minima, even under conditions where a significant energy barrier exists, resulting in reduced transport in subsurface environments. We also note that deposition or aggregation in secondary energy minima is reversible, as particles are released or disaggregate following reduction in ionic strength or increased hydrodynamic shear (91). Except for aggregation of *n*ZVI particles that have strong long-range attractive magnetic forces, or metallic nanoparticles with a large Hamaker (A_{121}) constant (Table S3), secondary energy minima are small for nanoparticles (sizes lower than 100 nm) at typical ionic strength of natural waters. Therefore, nanoparticles generally will not experience significant deposition or aggregation in secondary minima, and in the presence of an energy barrier will experience greater transport than micrometer-sized particles.

(d) **Interaction energy for very small nanoparticles or non-spherical particles.** The expressions summarized in Table 1 for the calculations of the various sphere-sphere and sphere-plate interaction energies are based on the classic Derjaguin approximation (8). The resulting expressions based on this approximation are valid for large particles and for very short separation distances, much smaller than the radius of the interacting particles. Accurate interaction energies for very small particles can be calculated based on the surface element integration (SEI) technique (112). This technique is particularly important for EDL interactions of small particles and low ionic strength, where $\kappa a_p < 1$ (κ is the inverse Debye length). The commonly used analytical expressions for EDL interactions (summarized in Table 1) are valid only for $\kappa a_p \gg 1$ (8). The surface element integration can also be applied to describe the interaction energies of non-spherical particles (113), which in principle can be extended to carbon nanotubes.

Quantitative Approaches to Evaluate Nanoparticle Aggregation

Three transport mechanisms govern the collision of particles during aggregation: Brownian diffusion (perikinetic aggregation), fluid motion (orthokinetic aggregation), and differential settling. For nanoparticles, Brownian diffusion is the predominant mechanism of aggregation with negligible contributions from fluid shear and sedimentation. The Smoluchowski result for the perikinetic aggregation rate constant (k_{ij}) for spherical nanoparticles is given by (8):

$$k_{ij} = \frac{2k_B T}{3\mu} \frac{(a_i + a_j)^2}{a_i a_j} \quad (10)$$

For nanoparticles of nearly equal size, the rate constant reduces to:

$$k_{ii} = \frac{8k_B T}{3\mu} \quad (11)$$

For nanoparticles in aqueous solutions at 25 °C, the rate constant for collision of nanoparticles, k_{ii} , is $1.23 \times 10^{-17} \text{ m}^3/\text{s}$.

Eqs 10 and 11 highlight two important features. First, for nanoparticles of equal size, the rate constant k_{ii} is independent of particle size. This surprising result is because increasing particle size leads to a lower diffusion coefficient but also to a larger collision radius, such that these two effects

cancel each other (8). The second important feature (eq 10) is that for particles of different size, the aggregation rate constant will always be greater than that for equal-size particles, which may be significant when small nanoparticles aggregate with much larger suspended particles in aquatic environments.

Unfavorable (Slow) Aggregation. Under unfavorable solution chemistry conditions, where repulsive interactions dominate, nanoparticle aggregation is “slow” or “reaction-limited”. Theoretical and experimental approaches to evaluate unfavorable aggregation are summarized briefly below.

(a) Theoretical approaches. The aggregation rate of nanomaterials decreases in the presence of repulsive interactions, such as electrostatic or steric repulsion. In this case, the fraction of successful collisions, α_a , often referred to as collision or attachment efficiency, needs to be incorporated into rate equations describing nanoparticle aggregation. When only EDL repulsion and VDW attraction are considered, the stability ratio, $W (=1/\alpha_a)$, for spherical nanoparticles of equal size is given by the Fuchs equation (114):

$$W = \frac{1}{\alpha_a} = 2 \int_0^{\infty} \frac{\exp(V_T / k_B T)}{(2a_p + h)^2} dh \quad (12)$$

A simple approximation of this equation is given by (8):

$$\alpha_a \approx 2\kappa a_p \exp\left(-\frac{V_{\max}}{k_B T}\right) \quad (13)$$

Because of the exponential dependence of α_a on V_{\max} , the equation predicts very low attachment efficiencies for energy barriers above a few $k_B T$. This equation also predicts that small changes in electrolyte concentration can have a dramatic effect on the rate of aggregation. Previous aggregation kinetics studies (e.g. (8), (115)) reveal that eq 12 markedly underpredicts the attachment efficiency of a wide range of colloidal particles, attributing the discrepancy to physical and chemical heterogeneities of particle surfaces as well as aggregation in secondary minima (116). Recent studies

with nC_{60} , however, demonstrated remarkable agreement between experimental results of aggregation kinetics and theoretical predictions (16, 18).

Note that the above analysis does not consider the role of hydrodynamic interactions. It is possible to incorporate the role of hydrodynamic interaction in the Fuchs' integral equation (8, 16). Such analysis has been successfully applied for the aggregation kinetics of nC_{60} by Chen and Elimelech (16, 18). Incorporation of hydrodynamic interaction in eq 12, however, has only a small effect on the attachment efficiency, α_a , reducing it by a factor of two or less.

We note that the theoretical approaches for nanoparticle aggregation (as well as nanoparticle deposition to be discussed later) are limited to spherical or, in practice, near-spherical nanoparticles. While these approaches are adequate for most engineered nanoparticles, a notable class of nanomaterials, namely carbon nanotubes (CNTs), cannot be treated with these approaches. CNTs have a very large aspect ratio (i.e., ratio of length to diameter), that often exceeds 1000. CNTs, particularly SWNTs, are also bundled and are not in the form of separate nanotubes in aquatic environments. The complex nature of CNTs precludes the use of useful theories to predict their aggregation (or deposition) behavior. Hence, experimental approaches, as those described below, are often used to describe their aggregation (or deposition) kinetics.

(b) Experimental approaches. Several methods are available to monitor the rate of aggregation of nanomaterials. Among these methods are dynamic light scattering (DLS), small angle light scattering (SALS), and fluorescence correlation spectroscopy (FCS).

Dynamic light scattering (DLS). DLS is the most common method to quantify the aggregation rate of nanomaterials. This technique is also known as photon correlation spectroscopy (PCS) or quasi-elastic light scattering (QELS). In this technique, the diffusion coefficient of aggregating nanoparticles is determined from the autocorrelation function obtained from the fluctuations of the scattered light intensity as a result of the Brownian motion of nanoparticles. The effective aggregate size is calculated from the diffusion coefficient using the Stokes-Einstein equation. DLS has been used to determine aggregation kinetics of a wide variety of nanomaterials (Table 2).

Small-angle light scattering (SALS). At very low scattering angles, the forward scattering intensity is proportional to the square of the particle/aggregate volume, and is independent of their shape or orientation. Although the form factor tends to be unity for all scattering angles for small nanoparticles, it varies significantly at high scattering angles for nanoparticle aggregate size of 100 nm or more (117). Therefore, SALS can be useful to derive absolute aggregation rate constants for nanomaterials.

Fluorescence correlation spectroscopy (FCS). In this approach, the particle/aggregate diffusion coefficient is determined for fluorescently-labeled particles passing through an optically-defined confocal volume. Temporal fluctuations in the measured fluorescence intensity are used to derive an autocorrelation curve which is related to the translational diffusion of the fluorophore through the confocal volume (118). FCS has been used to determine the diffusion coefficients and aggregation behavior of QDs, $n\text{TiO}_2$, and $n\text{ZnO}$ (43, 119).

Favorable (Fast) Aggregation. Under favorable solution chemistry conditions, in the absence of repulsive energy barriers, nanoparticle aggregation is “fast” or “diffusion-limited”. Theoretical and experimental approaches to evaluate favorable aggregation are briefly outlined below.

(a) Theoretical approaches. The transition from unfavorable to favorable aggregation occurs over a very narrow range of electrolyte concentration, at the salt concentration where the energy barrier for successful collision vanishes. This behavior can, in principle, be predicted from eq 12. The salt concentration corresponding to this transition is called the critical coagulation concentration (CCC). The magnitude of the CCC depends on the counterion valence (z), the nanoparticle zeta potential (ζ), and the Hamaker constant A_{121} according to (8):

$$CCC \propto \frac{1}{z^6 A_{121}^2} \tanh^4 \left(\frac{ze\zeta}{4k_B T} \right) \quad (14)$$

This equation shows that at large zeta potentials (i.e., $ze\zeta / 4k_B T \gg 1$), the CCC is proportional to z^{-6} . This relationship is known as the Schulze-Hardy rule. However, at low zeta potentials (i.e., $ze\zeta / 4k_B T \ll 1$), which is common for different engineered nanomaterials, the CCC is proportional

to z^{-2} . In practice, the CCC dependence on z for a wide range of nanomaterials should be in between z^{-6} to z^{-2} .

(b) Experimental approaches. The fast aggregation rate constant can be determined from any of the methods described earlier when carrying out aggregation experiments at high salt concentrations, above the CCC. Once the favorable aggregation rate is determined, the collision (attachment) efficiency, α_a , can be determined by normalizing the aggregation rate constant obtained at a given solution chemistry with the favorable aggregation rate constant. For instance, when using DLS, α_a can be obtained from the slopes of the initial change of the hydrodynamic radius with time (17, 120):

$$\alpha_a = \frac{\frac{1}{N_0} \left(\frac{da_h(t)}{dt} \right)_{t \rightarrow 0}}{\frac{1}{N_{0,fav}} \left(\frac{da_h(t)}{dt} \right)_{t \rightarrow 0,fav}} \quad (15)$$

where the subscript “*fav*” denotes favorable aggregation. This experimental approach can be used to determine the attachment efficiency of all types of nanomaterials, including non-spherical nanomaterials such as CNTs.

Quantitative Approaches to Evaluate Nanoparticle Deposition

The transport and deposition of nanoparticles in saturated granular porous media is generally governed by Brownian diffusion (68, 78), with negligible contributions from gravitational sedimentation and interception. The importance of Brownian diffusion increases with decreasing particle size, thereby increasing the number of collisions between nanoparticles and collector (e.g., aquifer grain) surfaces. Particle deposition onto a collector surface depends on a number of factors, including particle and grain sizes, particle and collector surface potentials, solution chemistry of the suspending medium, and the Hamaker constant of the particle-fluid-collector (8). In natural or engineered aquatic environments, the interactions between nanoparticles and collector surfaces—generally described by

the DLVO theory of colloidal stability— can either be attractive or repulsive. The particle attachment efficiency (α_d) is a parameter that relates the particle deposition rate measured under favorable conditions to that measured under unfavorable conditions (78):

$$\eta = \alpha_d \eta_0 \quad (16)$$

Unfavorable (Slow) Deposition. Analogous with aggregation, the dominating repulsive interactions encountered under unfavorable solution chemistries result in limited nanoparticle deposition. For deposition to occur under such conditions, sizable energy barriers between colloid and collector surfaces must be overcome. Theoretical and experimental approaches used to evaluate unfavorable deposition are summarized below.

(a) Theoretical approach. The most common approach in predicting nanoparticle deposition rates under unfavorable conditions is the interaction force boundary layer (IFBL) approximation (121, 122). In this approach, the region adjacent to a collector surface is divided into an inner layer (the IFBL) and an outer layer. The inner region thickness (δ_F) corresponds to that of the EDL, while the width of the outer region (δ_D) scales with the diffusion boundary layer. The IFBL approximation assumes that δ_D is far thicker than δ_F and that deposition of nanoparticles due to interception and gravitational sedimentation is negligible. Relevant IFBL equations are (8):

$$\eta = 4.0 A_s^{1/3} \left(\frac{D_\infty}{2a_c U} \right)^{2/3} \left(\frac{\beta}{1 + \beta} \right) S(\beta) \quad (17)$$

where β in the above equation is given by:

$$\beta = \frac{1}{3} (2)^{1/3} \Gamma \left(\frac{1}{3} \right) A_s^{-1/3} \left(\frac{D_\infty}{U a_c} \right)^{1/3} \left(\frac{K_F a_c}{D_\infty} \right) \quad (18)$$

Here, K_F is the pseudo-first order rate constant (8):

$$K_F = D_\infty \left\{ \int_0^{\delta_D} [g_1(H) \exp(V_T / k_B T) - 1] dy \right\}^{-1} \quad (19)$$

Similar to the analysis of unfavorable aggregation (eqs 12 and 13), the deposition rate is very sensitive to $V_T / k_B T$. Previous deposition kinetics studies indicate that eq 17 markedly underpredicts

the deposition rate for a wide range of colloidal particles and collector surfaces (8). This discrepancy is commonly attributed to chemical and physical heterogeneities of particle and collector surfaces as well as deposition in secondary minima.

(b) Experimental approaches. There exist two main experimental approaches to evaluate nanoparticle deposition rates onto collector surfaces in aqueous environments. The most commonly used approach is the laboratory-scale packed-bed column experiment (15, 61, 65, 78-80, 91). Another experimental technique that has recently been used to study nanoparticle deposition kinetics is the quartz crystal microbalance (QCM) (66, 85). Laboratory column studies are performed using columns packed with granular materials (e.g., glass beads, sand, or soil) and injecting the particles of interest at a known influent concentration, C_0 , for a time period t_0 . The particles are generally suspended in natural or artificial (model) solution chemistry of known composition. Particle retention in the packed-bed is evaluated by measuring the effluent particle concentration (C) as a function of time using techniques such as UV-visible and fluorescence spectrophotometry, or flow cytometry. The nanoparticle attachment efficiency is commonly evaluated using colloid filtration theory (CFT) (10):

$$\alpha_d = -\frac{2d_c}{3(1-\varepsilon)\eta_0 L} \ln(C/C_0) \quad (20)$$

The single-collector *contact* efficiency (η_0) in eq 20 is determined in the absence of external repulsive forces (favorable conditions) using the experimental or theoretical approaches described below.

Equation 20 is derived from a mass balance for a one-dimensional flow in a packed column when advection is the dominant mechanism of nanoparticle transport. This assumption is adequate for most laboratory column data with nanomaterials, including those described later in this paper. However, under conditions involving very low approach velocities (approximately less than 10^{-6} m/s), this equation is inadequate because transport of nanomaterials by dispersion dominates (123). Under these conditions, one needs to determine the nanoparticle deposition rate constant by fitting the breakthrough curve to the advection-dispersion equation with a first-order deposition rate constant (124). The attachment efficiency is then determined by normalizing the deposition rate constant with the favorable deposition rate constant determined from a similar experiment under favorable conditions or from theoretical approaches described below.

Alternatively, a pulse technique can be employed to explore the behavior of nanoparticles in packed-bed columns. Once the column has been equilibrated with electrolyte, a single-step injection pulse of nanomaterials of known mass or number concentration is introduced into the column. Assuming a semi-infinite column under clean-bed conditions, the particle concentration, $C(x,t)$, in the column at depth x and time t is given by the one-dimensional advection-dispersion equation (74, 108):

$$C(x,t) = n_o \frac{x}{2\sqrt{\pi t^3 D}} \exp(-k_d t) \exp\left[-\frac{(x-vt)^2}{4Dt}\right] \quad (21)$$

A nonlinear least-squares analysis can be employed to fit eq 21 to the breakthrough curves obtained subsequent to the pulse injection. Both k_d and D are obtained simultaneously with this analysis. Again, α_d is determined by normalizing this deposition rate constant with the favorable deposition rate constant determined from a similar experiment conducted under favorable conditions.

The QCM has recently been demonstrated to be useful in measuring the deposition kinetics of nanoparticles onto model collector surfaces (66, 85). In this technique, particle deposition occurs on a clean or functionalized silica-coated QCM crystal which is excited to oscillate at its fundamental resonance frequency. As particles deposit onto the crystal, the increase in mass (m) on the collector surface results in measurable decrease in the crystal's resonance frequency (f). For homogeneous, very thin, or quasi-rigid layers, the frequency shift of the oscillating crystal (Δf) is directly related to the increase in mass per unit area (Δm_f) by the Sauerbrey relation (125). As the frequency shift (Δf) is proportional to a change in mass (Δm_f) at the crystal surface, the rate of change of Δf is equivalent to the rate of mass change on the crystal surface (i.e., the rate of particle deposition or release). Hence, the nanoparticle deposition rate (r_d) can be determined by evaluating the initial slope in the Δf measurements (66) using:

$$r_d = \frac{d\Delta f}{dt} \quad (22)$$

When the QCM flow chamber is designed with a parallel-plate geometry, the Smoluchowski-Levich approximation can be used to evaluate the theoretical particle deposition rate (r_d^{SL}) in the absence of repulsive interactions:

$$r_d^{SL} = 0.538 \frac{D_\infty C_0}{a_p} \left(\frac{Pe h_c}{x} \right)^{1/3} \quad (23)$$

Two-dimensional microchannel structures have also been used to study nanoparticle deposition (68, 75). Photolithography and chemical etching are employed to construct porous microchannels. Particle suspensions of known concentration are injected into the 2-dimensional structure and the effluent concentration exiting the set-up can be determined using various detection methods. Additionally, pore clogging by large nanoparticle aggregates can be visualized by mounting the microchannels onto a microscope stage (68). Parallel-plate flow chambers can also be packed with collector grains, allowing for the visualization of particle deposition and pore clogging. While visualization of nanoparticles in such set-ups is challenging, the behavior of particle aggregates can sometimes be examined by mounting the set-up onto a microscope stage.

Favorable (Fast) Deposition. When deposition is favorable, the nanoparticle deposition rate approaches the mass-transport limited rate. In this case, α_d approaches unity, and $\eta = \eta_0$. Several theoretical and experimental approaches have been proposed to evaluate η_0 for nanoparticles and are described here.

(a) Theoretical approaches. The single-collector contact efficiency, η_0 , is a ratio between the total rate of particle-collector contacts and the rate at which particles flow towards a collector grain. Particle transport to the grain results from sedimentation, interception, and Brownian diffusion, with diffusion dominating for nanomaterials. The single-collector contact efficiency accounts for particle transport via interception (η_i), gravitational sedimentation (η_G), and Brownian diffusion (η_D) and can be determined by rigorously solving the convective-diffusion equation (9). Semiempirical correlation equations based on numerical solutions of the convective-diffusion equation have been developed (9, 126). A correlation equation developed by Tufenkji and Elimelech overcomes the limitations of previous approaches that are particularly important for nano-sized particles (9). Specifically, this equation considers the influence of hydrodynamic and VDW interactions on Brownian diffusion. Moreover, the impact of VDW forces on the transport of particles by gravitational sedimentation is also considered (9). This latter mechanism can be significant for nanoparticles of high density, such

as metal oxides. Hence, the single-collector contact efficiency for nanoparticle transport in saturated granular porous media under conditions favorable for deposition can be determined using (9):

$$\eta_o = 2.4A_s^{1/3}N_R^{-0.081}N_{Pe}^{-0.715}N_{vdW}^{0.052} + 0.55A_sN_R^{1.675}N_A^{0.125} + 0.22N_R^{-0.24}N_G^{1.11}N_{vdW}^{0.053} \quad (24)$$

The dimensionless parameters in eq 24 have all been defined elsewhere (9).

Equation 24 was derived from numerical simulations over a wide range of particle and porous media properties, covering particle diameters as small as 10 nm, approach velocities as low as 7×10^{-6} m/s, and particle densities as high as 1.8 g/cm^3 . The correlation equation slightly overestimates η_o for particle diameters smaller than about 30 nm, and the Smoluchowski-Levich approximation (8, 127) should be used for such small particles. This approximation yields predictions almost identical to those obtained from numerical solution of the complete convective-diffusion equation (9):

$$\eta_o = 4.04A_s^{1/3}N_{Pe}^{-2/3} \quad (25)$$

For very small nanoparticles (less than ~ 10 nm) and/or for unusually low approach velocities (on the order of 10^{-6} m/s or less), which are rarely encountered in practical applications, eqs 24 or 25 can yield η_o values greater than 1, which is physically questionable. Song and Elimelech (128) have analyzed this problem and indicated that η_o should not exceed 1. Similarly, at such unusually low approach velocities (on the order of 10^{-6} m/s or less) and for nanoparticles with high specific density (like metal oxide nanoparticles), η_o values greater than 1 can be obtained using eq 24. Here, again, the upper limit of η_o should be set to 1. We note, however, that such conditions of very low approach velocities are rarely encountered in the laboratory or field scale. Furthermore, under such low velocities the deposition rate is so high that the nanoparticles are practically immobile and there is no need to predict their transport.

(b) Experimental approaches. As with unfavorable deposition studies, experiments under favorable conditions can also be performed using packed-bed columns, the QCM, and micromodel flow-cells. Obtaining the favorable or transport-limited particle deposition rate can be beneficial when working with particles that undergo deposition and aggregation simultaneously. Under such conditions, the favorable deposition rate can be used to normalize observed deposition rates in efforts

to evaluate α_d (57). To obtain favorable deposition (and thus the favorable deposition rate), the colloid and collector surfaces must be oppositely charged. However, this is often not the case with model collector surfaces such as silica sand, as the isoelectric point (IEP) of silica is ~ 2 . Many engineered nanomaterials (e.g., $n\text{SiO}_2$, $n\text{TiO}_2$, QDs, $n\text{Au}$, fullerenes), also possess low IEPs (Table S1) and, hence, at environmentally relevant pHs, their deposition will be unfavorable. To create favorable conditions for deposition, the collector can be pretreated to create a positively charged surface (e.g., coating with a cationic polymer such as poly-L-lysine (PLL) or aminosilane surface modification) (108, 129). These surface treatments can be performed on various collector surfaces that might be used in QCM, packed columns, or micromodel flow-cells.

Current State of Knowledge on Nanoparticle Aggregation and Deposition

It can be expected that the most mobile nanomaterials will have the greatest impact on the environment, as they are most likely to contact potential receptors. In determining the mobility of any given particle, both aggregation and deposition must be considered. Aggregation and deposition are two closely related processes. The likelihood that either of these processes occurs depends on various interrelated factors. These include particle size and shape, particle and collector surface charges, and the surrounding pH and solution chemistry. An increase in size due to particle aggregation impacts particle mobility; hence, the time-scale of particle aggregation is an important consideration when conducting nanoparticle deposition studies. The information currently available in the literature on nanomaterial aggregation and deposition has been summarized and critically analyzed below.

Laboratory Studies Examining the Aggregation of Engineered Nanomaterials.

Table 2 presents a summary of studies involving aggregation of engineered nanomaterials in aquatic systems. This summary includes a wide range of nanomaterials, solution chemistries, and experimental techniques. Several of these studies present quantitative assessment of aggregation rates (16-18, 34, 43) and CCCs (16-18, 20, 24, 34, 54), while others present qualitative aggregation behavior (12, 36, 44).

CNT aggregation in aqueous solutions of inorganic electrolytes follows the classic Schulze-Hardy rule for colloidal stability (36). Multiwalled carbon nanotubes (MWNTs) have a negative electrophoretic mobility and are relatively stable at solution pH and electrolyte conditions typical of aquatic environments. Notably, the presence of natural organic matter markedly enhances the stability of MWNTs. Acidic functional groups, usually acquired via chemical treatment (24, 36, 53), increase the hydrophilicity of CNTs and substantially enhance their colloidal stability. A recent study demonstrated that clay minerals destabilize dispersed MWNTs in solution either by removal of surfactants from MWNT surfaces or by bridging between clay minerals and MWNTs by surfactant molecules (130). In contrast to MWNTs, studies on single-walled carbon nanotube (SWNT) aggregation are limited. SWNTs are highly bundled and are difficult to disperse even by sonication. However, once inter-tube VDW attraction is overcome, adsorption of surfactants, such as SDS, to SWNTs induces significant electrostatic repulsion to prevent SWNT re-aggregation (33). A recent study on SWNT aggregation kinetics has demonstrated that humic substances and biomacromolecules of relevance to biological media impart steric stabilization to SWNTs (131).

The early stages of aggregation of fullerene nanoparticles in the presence of both monovalent and divalent salts are consistent with the DLVO theory of colloidal stability (16-18). The presence of humic acid results in greater stability of nC_{60} suspensions as a result of steric repulsion (17). In identical polar solvents, the likelihood of aggregation among fullerene nanoparticles is $nC_{60} > nC_{70} > nC_{mix}$ (132). It was suggested that the original size and crystallographic face/lattice that control packing also play roles in aggregation in both polar solvents and aqueous solutions (19, 133). Labille et al. (134, 135) found that initially nC_{60} gradually become hydrophilic due to hydration and surface hydroxylation in the presence of water. It was hypothesized that this mechanism may be responsible for the gradual acquisition of titratable negative surface charge on the otherwise unfunctionalized fullerenes (134, 135). However, a recent study indicates that the mechanism of surface charge acquisition by nC_{60} is still not well understood (18).

Aggregation and stability of CNTs and nC_{60} depends on their surface properties, electrolyte concentration and type, and the specific adsorption mechanism of macromolecules, polymers, or surfactants. For example, humic and fulvic acid molecules adsorb onto MWNTs by π - π interactions

in which cross-linked aromatic networks on the molecules interact with aromatic rings on the MWNTs (28, 136). In fact, the sorption capacity and hence the stability of CNTs have been directly correlated to the aromatic content of NOM (136).

The presence of redox sensitive elements in nanoparticle structures may promote their dissolution and transformation. For example, oxidation of Fe in *n*ZVI produces a thin shell of hematite (Fe_2O_3) on the core of Fe^0 . The physicochemical properties of *n*ZVI with thick hematite shells are more likely similar to those of hematite particles. However, because *n*ZVI are often prepared with polymer and/or surfactant coatings, the properties of the Fe_2O_3 shell and Fe^0 core play a small role in the aggregation and deposition of *n*ZVI. The stability and aggregation behavior of *n*ZVI has been studied in the presence of different polymers and surfactants (51, 52, 54). Polymers and surfactants impart steric repulsive forces that oppose the long-range attractive magnetic forces between *n*ZVI particles. The properties of polymer-coated *n*ZVI are influenced by the chemical composition and structure of the polymer coating (137). Besides imparting a more negative surface charge due to sorption, surfactants such as poly(vinyl alcohol-co-vinyl acetate-co-itaconic acid), PV3A, also decrease the isoelectric point (53). These results collectively suggest that the properties of *n*ZVI are controlled by the characteristics of the surfactant or polymer added to achieve targeted application of *n*ZVI.

The stability curves in Figure 1 were prepared using the results of published experimental studies examining the aggregation kinetics of selected engineered nanomaterials under different solution conditions. Careful inspection of the data in Figure 1 reveals several interesting insights regarding nanoparticle aggregation behavior. Studies on *n*C₆₀ aggregation completed by Chen and Elimelech (18) show how different nanoparticle preparation methods can give rise to significantly differing nanoparticle surface properties and suspension stability (Fig. 1a). The data in Fig. 1a also show that the aggregation behavior of *n*C₆₀ particles can be comparable even across different laboratories (open square, triangles, and diamond). The solid symbols in Fig. 1a represent results obtained with the *n*C₆₀ derivatives PCBM ([6,6]-phenyl C₆₁-butyric acid methyl ester) and the corresponding butyl and octyl esters, PCBB and PCBO. When compared to *n*C₆₀, the derivatized nanomaterials exhibit considerably greater stability (14). Fig. 1b shows stability curves measured with MWNTs and oxidized MWNTs (O-MWNTs). The work of Smith et al (24) reveals linear

correlations between the CCC, total surface oxygen concentration (SOC), and surface charge of O-MWNTs. They also observed increased stability of O-MWNTs with increasing pH (square symbols, Fig. 1b). These studies suggest that although individual results may vary, aggregation of engineered nanomaterials, in general, follows the classical behavior of colloidal particles in aquatic systems. We note, for instance, clear trends of increasing values of the aggregation attachment efficiency with increasing solution ionic strength, to a maximum value of 1 when the CCC is reached.

Laboratory Studies Examining the Deposition of Engineered Nanomaterials. To date, laboratory studies examining the transport and deposition of engineered nanomaterials in aqueous environments have been performed using a variety of materials, including metallic, metal oxide, carbon-based, and semi-conductor based particles. These studies are summarized in Table 3, listing the type of experimental approach used in each study, as well as the solution chemistry, and collector and particle surface properties. The key findings of each study are also included. The summary presented suggests that it is not straightforward to draw conclusions from the transport studies performed thus far. Even when considering one type of particle, several factors complicate comparison between studies. These include variability in particle size and concentration, water chemistry (i.e., electrolyte species, ionic strength, and pH), flow velocity, and choice of collector surface. Moreover, given the importance of particle surface properties, direct comparisons between experiments involving bare and surface-modified nanoparticles are difficult to make.

Column studies are currently the most commonly used technique to elucidate nanoparticle deposition behavior. Experiments in columns packed with glass beads have indicated that SWNTs are mobile (78). Additionally, carboxylated SWNT transport in packed sand columns generally follows the behavior expected from DLVO theory, with straining limiting mobility at low ionic strength (73). A number of column studies have been performed to analyze the transport and retention of nC_{60} , employing glass beads, sand, and soil (15, 25, 59, 65, 79, 80, 93). At low ionic strength (3 mM), and in the presence of coarser sand ($d_{50}=335 \mu\text{m}$), nC_{60} elutes from packed sand columns with little retention. However, when finer sand ($d_{50}=125 \mu\text{m}$) and higher solution ionic strengths (30 mM) are encountered, a majority of the nanoparticles are retained (25). In packed soil columns, nC_{60} are

most mobile at higher flow velocities (11.4 and 3.8 m/day), with only limited nanoparticle mobility and extremely rapid deposition encountered at a lower flow velocity (0.38 m/day) representative of groundwater flow (59). Clearly, the choice of granular material, solution chemistry, and flow velocity all play major roles in nanoparticle deposition.

Packed column studies have demonstrated that the transport behavior of $n\text{C}_{60}$ particles is in good qualitative agreement with DLVO theory (25, 80). In addition to packed-bed column studies, the QCM has been employed to examine nanoparticle deposition onto and release from surfaces in aquatic environments (16, 57, 66, 85). QCM studies indicate that $n\text{C}_{60}$ deposition behavior is generally consistent with DLVO theory (16, 57).

Several studies have also reported the deposition behavior of inorganic nanoparticles (Table 3). Bare and surface-modified $n\text{Al}$ have demonstrated dissimilar deposition behaviors, even though the core material remains the same (61). Column studies with $n\text{ZVI}$ also indicate that surface modifications alter nanoparticle deposition behavior (138). A field study involving the injection of bimetallic (Fe/Pd) nanoparticles at a contaminated test site found particle behavior to be in general agreement with classical colloid transport concepts (64). QCM studies have established that the deposition behavior of bare and surface-modified $n\text{ZVI}$ onto silica surfaces is very different, with particles modified with amphiphilic triblock copolymer displaying significantly heightened mobility. QCM data obtained in this study correspond with column transport results (138). However, in these studies, surface-modified $n\text{ZVI}$ deposition was not in qualitative agreement with DLVO theory.

Several studies have examined the transport potential of $n\text{TiO}_2$ in saturated granular porous media (60, 78, 79). $n\text{TiO}_2$ retention in packed sand columns has been found to be high regardless of particle concentrations and flow velocities (60). Additionally, it appears that distinct transport processes likely occur at different column depths. Attempting to predict titania retention within packed sand columns utilizing an empirical kinetic transport model has indicated that existing models cannot predict $n\text{TiO}_2$ particle retention (60). $n\text{TiO}_2$ transport has been found to depend on both particle surface potential and particle aggregate size (68). Micromodel flow cell analysis of $n\text{TiO}_2$ transport and retention over a wide range of solution chemistries has been conducted (68). While the largest titania aggregate sizes are encountered at pH values closest to the pH_{zpc} , these aggregates have

been found to remain highly mobile. QCM deposition behavior of $n\text{TiO}_2$ onto silica was found to be in good qualitative agreement with DLVO theory (66). Working in a similar system with QD suspensions, heightened deposition is observed in the presence of divalent cations versus monovalent cations, with QD aggregation resulting in lowered deposition rate at higher ionic strength (85).

Although it is not straightforward to compare the results of deposition studies conducted with various engineered nanomaterials under dissimilar experimental conditions (e.g., solution chemistry, collector surfaces, and nanoparticle preparation methods), Figure 2 presents a direct comparison of data obtained in different laboratories with a wide range of nanomaterials. The deposition stability curves in Figure 2 show that nanoparticles of very dissimilar composition (e.g., $n\text{B}$ and sulfate modified latex (SML)) can exhibit comparable deposition behavior. It is interesting to note that much of the experimental data falls in a given region of the plot and exhibits an increase in α_d with increasing ionic strength. SWNTs (purple diamonds) generally experience greater retention in granular media, likely due to the influence of physical straining as discussed above. The black symbols in Fig. 2 represent data obtained using $n\text{ZVI}$ with differing surface modifications. These nanomaterials generally exhibit greater stability as a result of steric stabilization imparted by their polymer coatings. Similar to the conclusion drawn from inspection of Fig. 1, the data in Fig. 2 shows that the deposition of engineered nanomaterials also generally follows the classical behavior of colloids, with the exception of those particles that experience additional mechanisms such as steric stabilization or physical straining.

Challenges in Quantifying Nanoparticle Deposition and Aggregation in the Environment

Recent reviews and viewpoints have touched upon the challenges associated with characterizing nanomaterials in environmental settings. Many of these same challenges apply when considering nanoparticle aggregation and deposition in natural settings, given that in-depth particle characterization is required to fully understand particle mobility. Generally, difficulties arise due to a lack of analytical tools capable of characterizing and quantifying particles in complex environmental matrices. As a result, most deposition and aggregation studies have been conducted with simplified model laboratory systems. However, while providing important insights, particle behavior in model

laboratory systems might not be representative of that observed in far more complex natural environments.

Nanoparticle transport, persistence, and bioavailability in the environment are essential aspects to consider in assessing and managing risks (7). Factors such as microorganisms, naturally-occurring colloids and organic matter, biomacromolecules (e.g., proteins and polysaccharides), sunlight, and oxidants/reductants will complicate particle behavior in natural environments (1, 2), likely resulting in deviations from laboratory-scale experimental observations. Nanoparticles undergoing aggregation will sediment, thus becoming far less mobile. These aggregates may be ingested by organisms, potentially making their way into food chains (2). The impact that biota such as biofilms and invertebrates have on particle behavior remains unclear and must also be considered in natural settings (1).

Along with engineered nanoparticles, naturally occurring nanoparticles can also be found in the environment (7). Unintentional or incidental nanoparticles are a third source, and can originate from combustion, weathering, and oxidation processes among others (6, 7). When dealing with engineered, natural, and incidental nanoparticles simultaneously, establishing the source for any given particle is complicated (139). Additionally, background levels of certain elements, such as iron, in the environment may be significant (1). As a result, differentiating between the background elements and the engineered nanoparticles becomes a necessary and complicated task.

A majority of the aggregation and deposition studies conducted thus far have involved bare, non-functionalized nanomaterials. However, nanoparticles released into the environment may be either matrix bound or functionalized, thus altering their behavior (5). In the aim of understanding and predicting nanoparticle fate in aqueous environments, an in-depth characterization of particle surfaces following functionalization is necessary. A review describing the experimental methods available for analyzing nanoparticle surface chemistry and structure following intentional surface modification has been compiled (140). Regardless of prior characterization, additional particle modifications and chemical transformations can also occur upon release into the environment (2). For example, particles may undergo redox reactions or become coated with organic matter (7). Organic matter alters surface charge, thus affecting particle stability and aggregate size. Bridging due to the

adsorption of certain polymers onto particle surfaces can result in heightened aggregation. Both chemical and biological processes may result in inadvertent surface functionalization (6). On the other hand, such processes may wear down or alter existing surface functionality and particle coatings.

Environmental measurements are complex, with trace amounts of particles dispersed in a highly heterogeneous matrix. Currently, environmental nanomaterial concentrations, along with particle distribution and physicochemical data in natural settings, remain largely unavailable (1, 141). Analytical tools enabling the quantification of nanomaterials in multifaceted environmental matrices must be developed in order to better understand particle behavior. While techniques capable of identifying nanoparticles in sediments are available, they are incapable of quantifying the particles (6). Quantification will be further hindered by spatial and temporal variations in concentration (1). In the absence of appropriate tools, recent studies have modeled predicted environmental concentrations as a substitute (4, 141).

Along with information regarding particle concentration, additional properties such as the size distribution must be determined to fully comprehend the aggregation and deposition processes. A recent review by Tiede et al. (142) provides a detailed summary of the analytical tools currently available for nanoparticle characterization. While various characterization techniques can be employed, only a handful can deal with multifaceted environmental samples. Such samples present an assortment of elemental constituents and can potentially include multiple nanoparticle types. To further complicate matters, particles will likely be polydispersed in natural settings, making particle size determination more difficult. The nanoparticles encountered may also be in the dissolved, colloidal and particulate phases (1, 142).

Two key questions about nanoparticle aggregation and deposition were pointed out in the *Introduction* section of the manuscript; namely, “*How do specific particle and environmental properties affect deposition and aggregation?*”, and “*Are the current approaches and models used in quantifying colloidal interactions and transport applicable to nanomaterials?*”. This critical review begins to address these questions; however, it is evident that our current understanding of nanoparticle deposition and aggregation precludes a definitive unified answer. Although generalizations on the role of specific particle and environmental properties cannot yet be established, a comprehensive analysis of published

studies (Figures 1 and 2, and Tables 2 and 3) reveals that traditional DLVO theory can generally semi-quantitatively describe nanoparticle aggregation and deposition behavior. However, certain particle properties can lead to non-DLVO behavior; for instance, surface modifications such as polymer or surfactant coatings give rise to steric stabilization resulting in decreased nanomaterial deposition or aggregation. Moreover, unusual particle shapes, such as in the case of CNTs, can give rise to additional capture mechanisms (e.g., straining) which result in unpredicted nanomaterial transport patterns. Most common experimental and theoretical approaches used for evaluation of nanomaterial deposition and aggregation are applicable for spherical particles; however, we have noted above certain limitations for non-spherical or very small particles.

Acknowledgements

This research was supported by NSERC, McGill Engineering Doctoral Awards to ARP and IQP, the Canada Research Chairs Program, and the U.S. NSF under Research Grants CBET-0828795 and BES 0646247.

Nomenclature

Symbols

A	Hamaker constant
A_s	porosity-dependent parameter of Happel's model, $A_s = 2(1 - P^5)/w$
a_c	collector radius
a_h	hydrodynamic radius
a_i, a_p	particle radius, $i = 1, 2$
b	fluid envelope radius in Happel's model, $b = a_c(1 - \varepsilon)^{1/3}$
C	effluent particle concentration
C_0	influent particle concentration
C/C_0	normalized effluent particle concentration
$C(x,t)$	particle concentration at depth x and time t
D	hydrodynamic dispersion coefficient
D_∞	diffusion coefficient in an infinite medium, $D_\infty = k_B T / (6\pi\mu a_p)$
d_c	average collector grain diameter
e	electron charge, 1.602×10^{-19} C
F_{ST}	steric force
f	resonance frequency
$g_i(H)$	universal hydrodynamic function, $g_i(H) = 1/f_i(H)$
H	dimensionless separation distance, $H = h/a_p$
h	surface-to-surface separation distance
h_c	height of parallel-plate chamber
K_F	pseudo-first order rate constant
k_B	Boltzmann constant, 1.3805×10^{-23} J/K
k_d	particle deposition rate coefficient
k_{ij}	perikinetic aggregation rate constant between dissimilar-size particles

k_i	perikinetic aggregation rate constant between equal-size particles
L	bed depth
l	film thickness
M	magnetization
m	mass
N_0	initial particle number concentration
n_0	ratio of total injected particles to volumetric flow rate
P	ratio of a/b , $P = (1 - \varepsilon)^{-1/3}$
Pe	Péclet number, $Pe = 2Ua_p / D_\infty$
r	radial coordinate
r_d	particle deposition rate
$S(\beta)$	β function defined by Spielman and Friedlander (122)
s	distance between polymer chains on a surface
t	time
T	absolute temperature
U	approach (Darcy) velocity
v	fluid interstitial velocity, $v = U/\varepsilon$
V_{EDL}	electrical double-layer interaction energy
V_M	magnetic interaction energy
V_{ST}	steric interaction energy
V_{VDW}	van der Waals interaction energy
V_{\max}	energy barrier height
V_T	total interaction energy
w	porosity-dependent parameter, $w = 2 - 3P + 3P^5 - 2P^6$
W	stability ratio
x	distance from inlet (along flow)
y	boundary layer coordinate perpendicular to collector
z	counterion valence

Greek Symbols

α_a	aggregation attachment efficiency
α_d	deposition attachment efficiency
Γ_i	dimensionless surface potential for particle or collector, $\Gamma_i = \tanh\left[\frac{ze\psi_i}{4k_B T}\right]$
δ_D	diffusion boundary layer thickness
δ_F	electrical double-layer thickness
ε	porosity
ε_0	dielectric permittivity in vacuum, 8.85×10^{-12} F/m
ε_r	relative dielectric permittivity of solution
ζ	zeta potential
η	single-collector <i>removal</i> efficiency
η_0	overall single-collector <i>contact</i> efficiency
η_D	single-collector <i>contact</i> efficiency for transport by diffusion
η_G	single-collector <i>contact</i> efficiency for transport by gravity
η_I	single-collector <i>contact</i> efficiency for transport by interception
κ	inverse Debye length
λ	characteristic wavelength
μ	absolute viscosity of fluid
ψ	surface potential

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Table 1. Key Equations to Evaluate Particle-Particle and Particle-Surface Interactions

Interaction Geometry	Type of Interaction	Expression ^a	Ref
○ —	EDL	$V_{EDL} = 64\pi\epsilon_0\epsilon_r a_p (k_B T / ze)^2 \Gamma_1 \Gamma_2 \exp(-\kappa h)$ (3)	(103)
○ —	VDW	$V_{VDW} = \frac{A_{123} a_p}{6h(1+14h/\lambda)}$ (4)	(143)
○ —	STERIC ^b	$F_{ST}(h) = 2\pi a_p \left(\frac{k_B T}{s^3} \right) \left\{ \frac{8l}{5} \left[\left(\frac{2l}{h} \right)^{5/4} - 1 \right] + \frac{8l}{7} \left[\left(\frac{h}{2l} \right)^{7/4} - 1 \right] \right\}$ (5a) $V_{ST}(h) = - \int_{\infty}^h F_{ST}(h) dh$ (5b)	(144) (145)
○ — ○	EDL	$V_{EDL} = 64\pi \frac{a_1 a_2}{a_1 + a_2} \left(\frac{k_B T}{ze} \right)^2 \Gamma_1 \Gamma_2 \exp(-\kappa h)$ (6)	(103)
○ — ○	VDW	$V_{VDW} = - \frac{A_{121} a_1 a_2}{6h(a_1 + a_2)(1+14h/\lambda)}$ (7)	(143)
○ — ○	STERIC	$F_{ST}(h) = 2\pi \left(\frac{a_1 a_2}{a_1 + a_2} \right) \left(\frac{k_B T}{s^3} \right) \left\{ \frac{8l}{5} \left[\left(\frac{2l}{h} \right)^{5/4} - 1 \right] + \frac{8l}{7} \left[\left(\frac{h}{2l} \right)^{7/4} - 1 \right] \right\}$ (8a) $V_{ST}(h) = - \int_{\infty}^h F_{ST}(h) dh$ (8b)	(144) (145)

^aAll variables are defined in the *Nomenclature* section.

^bThis expression is for the case where both the particle and the surface are polymer-coated. For the case where only a single surface is polymer-coated, a factor of 2 is removed preceding each l term in eq. 5a.

Table 2. Summary of Laboratory Studies on Nanoparticle Aggregation

nanoparticle type	nominal size and concentration	experimental approach	solution chemistry	main findings and conclusions	references
nB	$d_{TEM} = 25$ nm $C = n/a$	DLS	20 - 1000 mM NaCl 0.2 - 20 mM $MgCl_2$ 0.2 - 10 mM $CaCl_2$ pH 5.6	Aggregation is similar to classical colloidal particles and follows DLVO theory	Liu et al. 2009
nC_{60} , nC_{70} and organic derivatives	$d = n/a$ $C = n/a$	DLS	10 mM NaCl, pH 4 - 10	Isoelectric point ~ 0 , nanoparticles stable at pH > 3.0; synthesis parameters control their stability and fate	Ma and Bouchard, 2009
nC_{60}	$d_{DLS} = 101.0$ nm 11.62 mg/L $d_{DLS} = 166.2$ nm 3.34 mg/L	time-resolved DLS	10 - 1000 mM KCl, pH = 5.5	nC_{60} prepared by prolonged stirring in water more stable than nC_{60} prepared by sonication in toluene; stability curves in agreement with DLVO theory	Chen and Elimelech, 2009
nC_{60} and organic derivatives	$d = n/a$ 0.22 - 2.42 mg/L	time-resolved DLS	25 - 1000 mM NaCl, pH = n/a	Presence of phenyl alkyl ester moieties increases colloidal stability	Bouchard et al. 2009
nC_{60}	$d_{DLS} = 92 \pm 0.3$ nm 1.0 - 2.7 mg/L	DLS	1-100 mM NaCl 1-100 mM $CaCl_2$ pH 7.0	Suspension stable at ≤ 1 mM ionic strength, regardless of electrolyte species, solution addition rate, or mixing sequence	Wang et al. 2008
nC_{60}	$d_{TEM} = 59.2 \pm 22.7$ nm 5.92 mg/L	time-resolved DLS TEM	90 - 650 mM NaCl $\pm 1 - 5$ mg/L HA 4 - 100 mM $MgCl_2 \pm 1$ mg/L HA 2.5 - 40 mM $CaCl_2 \pm 1$ mg/L HA pH 7.5 - 8.5	Aggregation kinetics consistent with DLVO theory; HA increases nC_{60} stability at low ionic strength due to steric repulsion; at > 10 mM $CaCl_2$, intermolecular bridging of HA macromolecules with Ca^{2+} results in increased light scattering and $\alpha > 1.0$	Chen and Elimelech, 2007
nC_{60}	$d_{TEM} = 59.2 \pm 22.7$ nm 5.92 mg/L	time-resolved DLS	60 - 350 mM NaCl 2.5 - 20 mM $CaCl_2$ pH 5.2	Stability ratios in good agreement with DLVO theory with reaction-limited and diffusion-limited aggregation zones clearly defined; CCCs at 120 and 4.8 mM for NaCl and $CaCl_2$, respectively	Chen and Elimelech, 2006
nC_{60} and nC_{70}	$d_{DLS} = 63$ nm $C = n/a$	DLS TEM	171 mM NaCl, pH = n/a	Monodisperse and polycrystalline nC_{60} clusters negatively charged and stable in pure water due to electrostatic repulsion; adding salt destabilizes cluster suspension	Deguchi et al. 2001
nC_{60}	$d_{TEM} = 7 - 36$ nm 130 mg/L	TEM	DI water, pH = n/a	nC_{60} nanoparticles form fractal clusters in hydrated state; size of individual clusters can be as low as 1 - 4 nm	Andrievsky et al. 1999
nC_{60}	$d \leq 200$ nm 80 - 140 mg/L	UV-Vis spectroscopy	0.005 - 85 mM NaCl 0.005 - 85 mM NH_4Cl 0.005 - 85 mM $CaCl_2$ 0.005 - 85 mM Na_2SO_4 0.005 - 85 mM $La(NO_3)_3$ pH 5 - 6	nC_{60} nanoparticles behave as typical colloidal particles and follow Schulze-Hardy rule	Mchedlov-Petrosyan et al. 1997

fullerols (C ₆₀ (OH) _n)	d _{TEM} = 100 - 250 nm 30 - 220 mg/L	UV-vis spectroscopy SEM TEM	0.1 - 500 mM Fe(NO ₃) ₃ , 500 mM each of Al(NO ₃) ₃ , CaCl ₂ , CoCl ₂ , CuCl ₂ , K ₂ MnO ₄ , Ag(NO ₃) and ZnCl ₂ pH 3 - 9	Fullerols react rapidly with metal to produce metal-fullerol cross-linked aggregates	Anderson and Barron, 2005
MWNTs	d _{TEM} = 0.6 ± 0.5 nm L = 0.1 - 5.8 mm 0.75 - 7.5 mg/L	Time-resolved DLS TEM AFM XPS	35 - 900 mM NaCl, pH 4, 6 and 8	Good correlation between CCC, total oxygen concentration, and MWNT surface charge	Smith et al. 2009
MWNTs	d _{TEM} = 0.6 ± 0.5 nm L = 0.1 - 5.8 mm < 3.0 mg/L	Time-resolved DLS	30 - 900 mM NaCl 30 - 200 mM Na ₂ SO ₄ 1 - 8 mM MgCl ₂ 0.7 - 6.2 mM CaCl ₂ pH 3 - 10	Oxidized MWNT CCC values consistent with electrostatic stabilization; surface charge correlates with pH-dependent MWNT colloidal stability variations	Smith et al. 2009
MWNTs	d _{TEM} < 10 - 100 nm L = 1 - 2 mm 100 - 200 mg/L	TEM UV-vis spectroscopy	1 - 20 mM Na + 25 mg/L TA 0.05 - 1.0 mM Mg + 25 mg/L TA 0.05 - 1.0 mM Ca + 25 mg/L TA 0 - 0.04 mM La + 25 mg/L TA pH 3 - 11	Aggregation rate independent of MWNT diameter; CCC values proportional to valence by an exponential factor of 5.5	Lin et al. 2009
MWNTs	d* = 140 ± 30 nm L = 7 ± 2 mm 50 - 500 mg/L	Thermal optical transmittance analyzer UV-vis spectroscopy	river water 1% SDS ± 10 - 100 mg/L NOM pH = n/a	MWNTs remain stable in presence of organic matter and river water; stability increases in presence of surfactant	Hyung et al. 2007
MWNTs	d _{TEM} = 17.6 ± 7.9 nm L = 1.5 ± 1.5 mm C = n/a	Time-resolved DLS	1 - 500 mM NaCl ± 5 mg/L HA 0.1 - 30 mM CaCl ₂ ± 5 mg/L HA 0.05 - 30 mM MgCl ₂ ± 5 mg/L HA pH 3 - 9	Electrostatic interactions control MWNT stability in electrolyte solutions; humic acid increases MWNT stability due to steric repulsion	Saleh et al. 2008
MWNTs	d = 10 - 30 nm L = 10 - 30 mm C = n/a	DLS	100 mg/L NOM, pH = n/a	Functionalization increases stability: (hydroxyl-modified > carboxyl-modified > bare)	Kennedy et al. 2008
MWNTs	d _{TEM} ~ 30 nm 50 mg/L	UV-vis spectroscopy	DI water 172 mM NaCl pH 0 - 12	COOH functionalized MWNTs stable at pH ≥ 4 as a result of carboxylic acid deprotonation to carboxylate anions	Shieh et al. 2007
SWNTs	d = n/a 100 mg/L	absorbance spectroscopy/photoluminescence	57.5 - 570 mM NaCl + 1% SDS 8.75 mM MgSO ₄ + 1% SDS 6.9 mM MgCl ₂ + 1% SDS 3.8 mM ErCl ₃ + 1% SDS pH = n/a	Once intertube van der Waals attraction overcome by sonication, SDS sorbed to SWNTs prevents reaggregation	Niyogi et al. 2007
SWNTs	d* = 1.2 nm < 600 mg/L	UV-vis spectroscopy	1-100 mM NaCl (-) mM KCl, MgCl ₂ , CaCl ₂ , LaCl ₃ , and CeCl ₃ pH = n/a	SWNTs treated with H ₂ SO ₄ /H ₂ O ₂ well-dispersed in water; CCC values follow Schulze-Hardy rule	Sano et al. 2001
SWNTs	d* = 0.9-1.4 nm	Time-resolved DLS	1-100 mM NaCl 0.1-10 mM CaCl ₂ pH 6 2.5mg/L (as TOC) of HA and biomacromolecules	HA and biomacromolecules (BSA, alginate, LB) impart steric stabilization; BSA had the most dramatic effect due to its globular molecular structure.	Saleh et al. 2010
QD	d* = 3.5 - 4.5 nm 680 mg/L	DLS	0 - 150 mM KCl 0 - 20 mM CaCl ₂ 0 - 20 mM MgCl ₂ 0 - 13.3 mM Al ₂ (SO ₄) ₃ pH 5, 8	QD stability controlled by ionic nature in solution; divalent and trivalent cations form strong complexes with QD capping ligands/functional groups, bridging QDs or neutralizing their surface charges	Zhang et al. 2008

QD	d* = 3.5 nm 100 mg/L	DLS Microscopy	DI water, pH 3 - 12	Decrease in pH causes surface ligands/functional group detachment; surface protonation promotes QD aggregation	Zhang et al. 2008
QD	d = n/a 0.37-0.67 mM (Cd)	FCS	1-100 mM Na ₂ HPO ₄ + 0.2-20 mM KH ₂ PO ₄ + 0.3-27 mM KCl + 1.4-1370 mM NaCl pH = 7.4 - 9.0	Aggregation rate depends on QD size (small QDs aggregate quickly); above 'photoactivation critical concentration', aggregation and subsequent photoactivation rapid under laser irradiation	Dong et al. 2007
nAg	d _{TEM} = 1 - 3 nm C = n/a	UV-vis spectroscopy TEM	0-800 mM Ba ²⁺ 0-800 mM Ca ²⁺ 0-20 mM each of Zn ²⁺ , Cr ³⁺ , Cu ²⁺ , Pb ²⁺ pH= 9.3	Change in position of absorption spectra during cation induced aggregation useful in identifying interaction mechanism between Ag nanoparticles and electrophilic transition metal cations or less polarizable alkaline metals	Liu et al. 2003
nAg	d _{DLS} = 23 - 42 nm 0.26 -7.0 x 10 ⁹ particles/L	DLS UV-vis spectroscopy	10-1000 mM NaCl 200 mM NaCl + 0.005-0.1% hydroxy-ethylcellulose pH = n/a	Fractal dimensions increase with time in reaction limited aggregation regime but not in diffusion limited aggregation regime	Trinh et al. 2009
nZVI	d = n/a 1 mg/L	photography spectroscopy	1.2 mM NaHCO ₃ ± 20 - 200 mg/L NOM, pH 7.1	NOM sorption onto nZVI results in reduced sticking coefficient and enhanced stability	Johnson et al. 2009
nZVI	d _{DLS} = ≤ 200 nm 154 mg/L	DLS	≤ 500 mM NaCl ± ≤1 g/L guar gum ≤10 mM CaCl ₂ ± ≤1 g/L guar gum pH 7.0	At high salt concentrations (500 mM NaCl and 3 mM CaCl ₂), guar gum stabilizes ZVI	Tirafferri et al. 2008
nZVI	d _{TEM} = 10 - 80 nm 3000 mg/L	DLS	1 mM NaHCO ₃ ± 5 - 1000 mg/L polystyrene sulfonate 1 mM NaHCO ₃ ± 5 - 1000 mg/L CMC 1 mM NaHCO ₃ ± 5 - 1000 mg/L PA pH 9.5 - 10.5	Larger ZVI particles unstable due to strong attractive magnetic forces	Phenrat et al. 2008
nZVI	d _{DLS} = 15.2 - 3000 nm C = n/a	DLS	≤200 mM NaCl ≤10 mM CaCl ₂ pH = n/a	High cation concentrations promote aggregation of stable ZVI particles	He and Zhao, 2007
nZVI	d _{TEM} = 10 - 80 nm 3000 mg/L	DLS optical microscopy	1 mM NaHCO ₃ , pH 7.4	Aggregation rapid; increased aggregation with increasing saturation magnetization (magnetic moment)	Phenrat et al. 2007
nTiO ₂	d _{RG} = 6 - 7 nm 3000 - 10000 mg/L	absorption spectroscopy	500 - 2000 mM KCl, pH 0 - 2.0	Aggregation slow at pH 0.1 - 2.0; aggregate structure depends on ionic strength and medium pH	Pavlova-Verevkina et al. 2009
nTiO ₂	d* = 5 nm 1 mg/L	FCS	5 - 100 mM NaNO ₃ ± 0.2 - 5 mg/L FA pH 2 - 8	Rapid aggregation in vicinity of pH _{ZPC} ; adsorbed FA increases nanoparticle stability due to increased steric repulsion	Domingos et al. 2009
nTiO ₂	d* = 4 - 6 nm 80 - 83 mg/L	DLS	4.5 - 16.5 mM NaCl 12.8 mM CaCl ₂ pH 4.8 - 8.2	Aggregation rate significantly higher in CaCl ₂ than in NaCl	French et al. 2009
nTiO ₂	d* = 35 nm 2000 mg/L (40mg/g of soil)	DLS	50 g/L diluted soil solution pH 6.15 - 8.58	In soil solution, high ionic strength and low DOC result in heightened aggregation rates	Fang et al. 2008
nTiO ₂	d* = 5, 32 nm 2 - 200 mg/L	DLS	20 mM NaCl ± 0.1 - 2.2 mM organic acids, pH 2 - 6.5	Aggregation occurs at all pH values; finer particles aggregate faster than larger particles	Pettibone et al. 2008
nTiO ₂	d = n/a 30 mg/L	DLS	0.01- 10 mM KCl 1 mM each LiCl, KBr, CsCl, LiF pH 2 - 12	Hydrated ion radius determines extent of adsorption; isoelectric point changes due to ion adsorption	Tkachenko et al. 2006
nTiO ₂	d* = 7 - 20 nm C = n/a	fractal dimension measurement	DI water pH = n/a	Diffusion-limited aggregation results in fractal-like aggregates	Tseng and Lin, 2003

Table 3. Summary of Laboratory Studies on Nanoparticle Deposition

nanoparticle type	deposition system	particle size and concentration	collector surfaces	solution chemistry	main findings and conclusions	references
<i>n</i> Al	packed column H: 16 cm, D: 1.5 cm	$d^* = 100$ nm large 1-10 μ m agglomerates 50 mg/L	quartz sand $d_{50} = n/a$	0.01M NaCl, pH 4, 7	Greater mobility at pH 4; Aluminum oxide coated particles more prone to leaching; leach most at pH 7	Doshi et al. 2008
alumoxane	packed column H: 9.25 cm, D: 2.5 cm	$d_{DLS} = 74$ nm 0 - 10 mg/L	glass beads d = 300 - 425 μ m ($d_{50} = 355$ μ m)	0.01 M NaCl, pH 7	High mobility; approximately 80% passage	Lecoanet et al. 2004
<i>n</i> B	packed column H: 15 cm, D: 1.5 cm	$d^* = 10 - 20$ nm $d_{TEM} = 25$ nm 50 mg/L	quartz sand d = 212 - 270 μ m ($d_{50} = 250$ μ m)	0.01 - 0.4 M NaCl, pH 5.6	Attachment efficiency increases with increasing IS up until 0.2 M	Liu et al. 2009
<i>n</i> CeO ₂	model wastewater treatment plant (biological treatment only)	$d_{DCL,TEM} = 20 - 50$ nm 100 mg/L \pm dispersing agents	fresh, stabilized clearing sludge 1.5 - 2.5 g/L dry content	<i>n</i> CeO ₂ , synthetic wastewater and drinking water mixed into aeration chamber, pH 8 - 8.5	Significant portion of <i>n</i> CeO ₂ present as large aggregates, bound to bacteria; high unagglomerated <i>n</i> CeO ₂ levels	Limbach et al. 2008
<i>n</i> CuO	2-D flow cell Length: 11.3 cm	$d^* = 118 - 637$ nm $d_{DLS} = 372$ nm 9 mg/L \pm SDS	etched glass d = 0.87 mm	0.01 M NaCl, pH 7	<i>n</i> CuO aggregates form within porous medium; velocity affects aggregate deposition density and location; SDS enhances particle elution	Jeong & Kim, 2009
ferroxane	packed column H: 9.25 cm, D: 2.5 cm	$d_{DLS} = 303$ nm 0 - 10 mg/L	glass beads d = 300 - 425 μ m ($d_{50} = 355$ μ m)	0.01 M NaCl, pH 7	Least mobile of 8 nanoparticles tested in study; mobility appears to decrease with time	Lecoanet et al. 2004
<i>n</i> C ₆₀	packed column H: 9.25 cm, D: 2.5 cm	$d_{DLS,TEM} = 20, 135, 168$ nm 0 - 10 mg/L	glass beads $d_{50} = 355$ μ m	0.001, 0.1 M NaCl, pH 7	Increased deposition with increasing IS; repulsive interactions between EDLs key to <i>n</i> C ₆₀ stability in suspension	Brant et al. 2005
<i>n</i> C ₆₀	QCM	$d_{DLS} = 50.5$ nm 5.8 mg/L	silica surface (bare or coated)	10 - 100 mM NaCl, pH 5.5 0.3 - 3 mM CaCl ₂ , pH 5.5	Behavior consistent with DLVO theory; humic acid and alginate decrease deposition rate due to steric repulsion	Chen and Elimelech, 2008
<i>n</i> C ₆₀	QCM-D	$d_{DLS} = 55.7$ nm ~ 3 mg/L	silica surface	1 - 300 mM NaCl, pH 5.2 0.1 - 1.0 mM CaCl ₂ , pH 5.2	Above CCC, rate of deposition decreases as a result of concurrent <i>n</i> C ₆₀ aggregation	Chen and Elimelech, 2006
<i>n</i> C ₆₀	packed column H: 5 cm, D: 0.9 cm	$d_{TEM} \sim 100$ nm 48 mg/L	lula soil (92% sand, 6% silt, 2% clay) $d_{50} \sim 250$ μ m	0.02M (NaCl + NaN ₃), pH 6.7 - 7.2	<i>n</i> C ₆₀ particles most mobile at higher velocities; column ripening possibly observed at low velocity	Cheng et al. 2005
<i>n</i> C ₆₀	packed column H: 10 cm, D: 2.65 cm	TTA/ <i>n</i> C ₆₀ : $d_{DLS} = 92$ nm 1.26 mg/L THF/ <i>n</i> C ₆₀ : $d_{DLS} = 111$ nm 2.34 mg/L	glass beads $d_{50} = 360$ μ m	0.01 - 0.6 M NaCl \pm TA, alginate, pH 6.5 - 7.5 other electrolytes considered	Increased deposition with increasing IS and decreasing velocity; transport affected by preparation method	Espinasse et al. 2007
<i>n</i> C ₆₀	packed column H: 4.3 cm, D: 1.6 cm	$d_{DLS} = 101$ nm 65 \pm 5 μ g (pulse injection)	natural soil (58% sand, 29% clay, 13% silt) d = 420 - 1000 μ m	KCl or CaCl ₂ (selected IS to compare with SWNT studies), pH 5.6 - 5.8	Compared to SWNT transport in soil packed columns, fullerene deposition more sensitive to IS; exhibits lower deposition rates	Jaisi & Elimelech, 2009
<i>n</i> C ₆₀	packed column H: 9.25 cm, D: 2.5 cm	$d_{DLS} = 168$ nm 0 - 10 mg/L (step function)	glass beads d = 300 - 425 μ m ($d_{50} = 355$ μ m)	0.01 M NaCl, pH 7	Fullerenes experience greater retention than fullerols and SWNTs	Lecoanet et al. 2004
<i>n</i> C ₆₀	packed column H: 9.25 cm, D: 2.5 cm	$d_{DLS} = 168$ nm 10 mg/L	glass beads d = 300 - 425 μ m ($d_{50} = 355$ μ m)	0.01 M NaCl, pH 7	Higher velocities alter break-through curve appearance but do not result in increased elution	Lecoanet & Wiesner, 2004
<i>n</i> C ₆₀	packed column H: 15 cm, D: 2.5 cm	$d_{DLS} = 120$ nm 3 mg/L	Ottawa sand (4 fraction sizes) $d_{50} = 125, 165, 355, 710$ μ m	3.065 mM (CaCl ₂ + NaHCO ₃), pH 7	Transport behavior not in agreement with DLVO; primary minimum deposition attributed to surface charge heterogeneities	Li et al. 2008

nC_{60}	packed column H: 15 cm, D: 2.5 cm	$d_{DLS} = 95$ nm 1-3 mg/L	Ottawa sand $d_{50} = 360$ μ m glass beads $d_{50} = 360$ μ m	1 mM $CaCl_2$, pH 7	Transport and deposition behavior consistent with batch retention data and DLVO theory	Wang et al. 2008
nC_{60}	packed column H: 15 cm, D: 2.5 cm	$d_{DLS} = 92$ nm (stock) 3 mg/L	quartz sand $d_{50} = 125, 335$ μ m	3, 30 mM NaCl, pH 7 3, 30 mM $CaCl_2$, pH 7	Little nC_{60} retention observed in coarser sand at low IS; > 95% retention at high IS with finer sand (regardless of electrolyte)	Wang et al. 2008
fullerols $C_{60}(OH)_n$	packed column H: 10 cm, D: 2.65 cm	$d_{DLS} = 120$ nm 18 mg/L	glass beads $d_{50} = 360$ μ m	0.01 - 1 M NaCl, pH 6.5 - 7.5	Increased deposition with increasing IS	Espinasse et al. 2007
fullerols $C_{60}(OH)_n$	packed column H: 9.25 cm, D: 2.5 cm	$d^* = 1.2$ nm 0 - 10 mg/L (step function)	glass beads $d = 300 - 425$ μ m ($d_{50} = 355$ μ m)	0.01 M NaCl, pH 7	Fullerols have little affinity for porous media	Lecoanet et al. 2004
fullerols $C_{60}(OH)_n$	packed column H: 9.25 cm, D: 2.5 cm	$d^* = 1.2$ nm 10 mg/L	glass beads $d = 300 - 425$ μ m ($d_{50} = 355$ μ m)	0.01 M NaCl, pH 7	Extremely low attachment levels; 99% passage achieved at both flow velocities	Lecoanet & Wiesner, 2004
Pd- $nZVI$	subsurface delivery test site 4.5 x 3.0 m, 6 m deep	$d_{SEM} = 100 - 200$ nm 1.7 kg nanoparticles injected	aquifer hydraulic conductivity = 0.2 cm/s groundwater present = 14.1 m ³	groundwater: pH 4.6 - 5.2 prior to injection pH 5.1 - 7.7 post injection	Pd- $nZVI$ behavior in line with classical colloid transport concepts and reactions in porous media	Elliot & Zhang, 2001
Pd- $nZVI$	packed column H: 3.4 cm, D: 1 cm	bare particles: form dendritic flocs (TEM) CMC-stabilized particles: $d_{TEM} = 4.3$ nm $d_{DLS} = 17.2$ nm 1 g/L	soil (84% sand, 10% silt, 6% clay) $d = n/a$	particle suspensions, pH 6.8, 8.3 DI water to elute retained particles	CMC-stabilized particles well dispersed in soil; ~ 98% of stabilized Fe-Pd collected from eluent (no irreversible binding)	He et al. 2007
$nZVI$	packed column H: < 100 cm, D: 1.6 cm	$d_{TEM} = 50 - 100$ nm 5 mg/mL	Ottawa sand $d = 160 \pm 45$ μ m	PAA + PSS + bentonite clay mixtures, pH = n/a	Particle elution dependent on electrolyte composition but not on total [poly(anion)]; higher PSS and lower PAA and clay concentrations result in highest elution	Hydutsky et al. 2007
$nZVI$	packed column H: 10 cm, D: 2.5 cm H: 50 cm, D: 6 cm	bare: $d_{SEM} = 10 - 160$ nm surfactant stabilized: $d_{TEM} = 2 - 10$ nm 1 g/L	glass beads sand (unbaked and baked) all collector types: $d = 425-600$ μ m	0.01 M NaCl (\pm surfactant), pH 7	Adding surfactant, breakthrough occurs earlier in column packed with glass beads; $nZVI$ is immobile in absence of surfactant	Kanel et al. 2007
$nZVI$	2-D physical model L*: 50 cm, W: 2 cm, H: 28.5 cm	size = n/a 4 g/L	silica beads $d_{50} = 1,100 \pm 100$ μ m	freshwater steady-state flow pH = n/a	Nonstabilized $nZVI$ not transported; PAA- $nZVI$ transported with negligible retardation; transport influenced by density gradients	Kanel et al. 2008
$nZVI$	packed column H: 25.5 cm, D: 1.1 cm	3 particle fractions: bimodal size distributions (DLS) 0.03 - 6 g/L	quartz sand $d_{50} = 300$ μ m	10 mM (NaCl + $NaHCO_3$), pH 8	At 0.03 g/L concentration, all modified $nZVI$ particles mobile; at higher concentrations, larger particles with higher Fe ⁰ content experience heightened deposition	Phenrat et al. 2009
$nZVI$	packed column + QCM-D H: 61.3 cm, D: 1.1 cm	bare: $d_{DLS} = 146$ nm Triblock co-polym mod.: $d_{DLS} = 212$ nm PA mod.: $d_{DLS} = 66$ nm SDBS mod.: $d_{DLS} = 190$ nm 30 mg/L	quartz sand $d_{50} = 300$ μ m	1 - 1000 mM NaCl, pH 7.7 0.1 - 50 mM $CaCl_2$, pH 7.7	Bare $nZVI$ was immobile, while both PA and SDBS-modified particles mobile at lower IS; Triblock co-polymer-modified particles have greatest mobility	Saleh et al. 2008
$nZVI$	packed column H: 13 cm, D: 1.2 cm	carbon stabilized iron $d_{TEM} = 30 - 100$ nm 5 mg/mL	Ottawa sand $d = 200 - 700$ μ m 3 soil types loam, sandy loam, clay loam	Nanopure water, pH 6.7	All collector types retain unsupported $nZVI$; supported particle retention highest in loam and sandy loam ($\geq 80\%$); elution decreases with time	Schrick et al. 2004
$nZVI$	packed column V: 10 mL (in 50 mL buret)	bare: $d^* = 30 - 70$ nm Fe-silica: $d_{TEM} = 358 \pm 249$ nm 3 g/L	Ottawa sand $d \geq 300$ μ m	DI water pH = n/a	Bare $nZVI$ trapped in top portion of column; ~70% of Fe-silica particles reach bottom of column and elute	Zhan et al. 2008

$nZVI$	horizontal capillary tube H: 3 cm, D: 0.15-0.18 cm	bare: $d^* = 30 - 70$ nm Fe-silica: $d_{TEM} = 358 \pm 249$ nm 3 g/L	Ottawa sand $d \geq 300$ μ m	DI water pH = n/a	Bare $nZVI$ aggregates accumulate at inlet; Fe-silica particles form small clusters and distribute uniformly throughout capillary	Zhan et al. 2008
polystyrene latex (sulfate-modified)	packed column H: 20 cm, D: n/a	$d^* = 46$ nm 1 - 4 mg/L	glass beads $d = 200, 400$ μ m	3 - 300 mM KCl, pH = 6.7 13 - 800 mM (CaCl ₂ + KCl), pH = 6.7	Deposition rates increase with increasing IS until 0.1M KCl and 0.01M CaCl ₂ (above which deposition rates drop off again)	Elimelech & O'Melia, 1990
polystyrene latex	packed column H: 15, 20 cm, D: n/a	$d^* = 46$ nm 0.5 ppm	glass beads $d = 200, 400$ μ m	3 - 300 mM KCl, pH 6.7	Deposition rates increase with increasing IS	Elimelech & O'Melia, 1990
polystyrene latex (sulfate-modified)	packed column H: 25 cm, D: 2.5 cm	$d^* = d_{DLS} = 98$ nm 1 mg/L	glass beads $d = 200$ μ m	0 - 500 mM NaCl \pm 1 mg C/L SRHA, pH 7.2	Increased particle deposition with increasing IS; particles depositing at lower IS more prone to reentrainment; reduction in particle deposition and enhanced reentrainment in presence of SRHA	Franchi & O'Melia, 2003
polystyrene latex (sulfate modified)	packed column H: 20 cm, D: 2.5 cm	$d^* = 72$ nm 1 mg/L	glass beads $d = 400$ μ m	0.01 M NaClO ₄ , pH 10	Latex particles exhibit little affinity for glass beads	Hahn et al. 2004
polystyrene latex	packed column H: 20 cm, D: 10 cm	$d^* = 53$ nm 1 mL pulse injection, C = n/a	Munich gravel $d = 250$ μ m Sengenthal sand $d = 100$ μ m	1, 10 mM NaCl, pH = n/a 1, 10 mM CaCl ₂ , pH = n/a	Deposition in agreement with DLVO theory; particle elution increases with decreasing IS; removal efficiency in sand more affected by IS, impact of counterion valence more apparent in gravel	Huber et al. 2000
polystyrene latex (sulfate-modified)	packed column H: 15 - 16.5 cm, D: 1 cm	$d^* = 50$ nm C = n/a	quartz sand $d_{50} = 256$ μ m	1 - 100 mM KCl \pm 5.0 mg/L SRHA, pH 5.7	Increase in IS results in increased attachment; addition of SRHA decreases attachment	Pelley & Tufenkji, 2008
polystyrene latex (carboxyl-modified)	packed column H: 20 cm, D: 5.4 cm	$d^* = 20$ nm pulse injection, C = n/a	dune sand (3 preparations) washing: none, dH ₂ O, acid $d_{50} = 0.31 - 0.32$ mm	3 - 4 mM artificial rainwater, pH 7 - 8	Colloid retention greater in unwashed (natural) sand than in washed types	Shani et al. 2008
polystyrene latex (carboxyl-modified)	packed column H: 10 cm, D: 3.8 cm	$d^* = 30, 66$ nm 10 mg/L	glass beads (3 fraction sizes) $d = 88 - 125$ μ m, $d_{50} = 110$ μ m $d = 180 - 250$ μ m, $d_{50} = 220$ μ m $d = 590 - 840$ μ m, $d_{50} = 720$ μ m	DI water 0.2 M NaCl, pH 10	Using DI water, 100% nanoparticle elution observed; addition of DI water to columns run using NaCl releases colloids deposited in secondary minima	Shen et al. 2008
polystyrene latex (carboxyl-modified)	packed column H: 12.6 cm, D: 1.6 cm	$d^* = 63$ nm $3.6 \times 10^8 - 3.6 \times 10^9$ particles/mL	glass beads $d_{50} = 330$ μ m	20 - 200 mM KCl, pH 8, 11	Increasing IS results in a marked increase in retention	Tufenkji & Elimelech, 2005
chloromethyl latex (sulfate-modified)	packed column H: 10 cm, D: 4.5 cm saturated and unsaturated conditions	$d^* = 20, 100$ nm 100 mg/L	quartz sand $d = 300 - 355$ μ m	1 mM (NaCl + NaHCO ₃), pH 7.5	Transport is size dependent under saturated and unsaturated conditions; colloid retention sensitive to saturation	Zhuang et al. 2005
QDs	QCM-D	$d^* = 10$ nm $d_{DLS} = 45 - 100$ nm 0.96 mg/mL	silica surface	1 - 300 mM KCl, pH 5, 7 17 mM CaCl ₂ , pH 5	3 - Heightened QD deposition in presence of Ca ²⁺ (vs K ⁺) and at pH 5 (vs pH 7)	Quevedo & Tufenkji, 2009
$nSiO_2$	packed column H: 9.25 cm, D: 2.5 cm	2 particle sizes type 1: $d_{DLS} = 57$ nm, $d^* = 47$ nm type 2: $d_{DLS} = 135$ nm, $d^* = 103$ nm 0 - 10 mg/L	glass beads 300 - 425 μ m ($d_{50} = 355$ μ m)	0.01 M NaCl, pH 7	Smaller silica particles very mobile with low affinity for collector; heightened retention with larger particles	Lecoanet et al. 2004
$nSiO_2$	packed column H: 9.25 cm, D: 2.5 cm	$d_{DLS} = 57$ nm 10 mg/L	glass beads 300 - 425 μ m ($d_{50} = 355$ μ m)	0.01 M NaCl, pH 7	Very low retention; flow rate has no significant impact on silica removal	Lecoanet & Wiesner, 2004
SWNTs	packed column H: 6.3 cm, D: 1.6 cm	$d_{RS} = 0.9 - 1.6$ nm 87 mg/L	quartz sand $d = 225 - 300$ μ m ($d_{50} = 263$ μ m) (bare and silanized)	0.1 - 55 mM KCl \pm 5 mg/L SRHA, pH 7.0 10 mM (KCl + CaCl ₂) \pm 5 mg/L SRHA, pH 7.0	Results consistent with DLVO theory; SWNT straining restricts mobility at low IS	Jaisi et al. 2008

SWNTs	packed column H: 4.3 cm, D: 1.6 cm	$d_{DLS} = 244$ nm 7 - 125 μg (pulse injection)	soil (58% sand, 29% clay, 13% silt) $d = 0.42 - 1.0$ nm	0.1 - 100 mM KCl, pH 5.6 - 5.8 0.03 - 10 mM CaCl_2 , pH 5.6 - 5.8	High retention with little change above 0.3 mM KCl or 0.1 mM CaCl_2 ; physical straining plays important role in SWNT deposition	Jaisi & Elimelech, 2009
SWNTs	packed column H: 9.25 cm, D: 2.5 cm	$d^* = 0.7 - 1.1$ nm L = 80 - 200 nm $d_{DLS} = 21$ nm 0 - 10 mg/L	glass beads 300 - 425 μm ($d_{50} = 355$ μm)	0.01 M NaCl, pH 7	SWNTs show little affinity for porous media	Lecoanet et al. 2004
SWNTs	packed column H: 9.25 cm, D: 2.5 cm	$d^* = 0.7 - 1.1$ nm L = 80 - 200 nm $d_{DLS} = 21$ nm 10 mg/L	glass beads 300 - 425 μm ($d_{50} = 355$ μm)	0.01 M NaCl, pH 7	Extremely low attachment; increased velocity alters breakthrough curve appearance	Lecoanet & Wiesner, 2004
MWNTs	packed column H: 10 cm, D: 5 cm	$d_{TEM} = 7 - 70$ nm $L_{SEM} = 100$ nm - 2 μm , avg. 407 nm 100 mg/L	quartz sand $d_{50} = 476$ μm glass beads $d = 425 - 500$ μm	10 mM solution ($\text{NaHCO}_3 + \text{Na}_2\text{CO}_3 + \text{NaBr}$ or NaCl), pH 10 0.1 mM NaOH solution, pH 10	Breakthrough at 43, 21 and 4.0 m/d similar, with time-dependent C/Co; particle mobility likely enhanced beyond critical pore water velocity	Xueying et al. 2009
SWNTs & MWNTs	packed column H: 15 cm, D: 2.5 cm	SWNTs: $d^* = 1.4$ nm MWNTs: $d^* = 35 \pm 10$ nm C = n/a	quartz sand $d_{50} = 350$ μm	0.01 - 10 mM KCl 0.01 - 10 mM CaCl_2 pH = n/a	Filtration of MWNTs higher than SWNTs; straining insignificant	Wang et al. 2008
nTiO ₂	soil cell H: 1.27 cm, D: 2.54 cm	$d^* = 21$ nm $d_{DLS} = 123.2 \pm 7.6$ nm 25 mg/L	glass beads $d = 500$ μm	0.2 mM NaCl, pH 10	Considers unsaturated nTiO ₂ transport; increased retention with decreasing saturation and slower drainage rates	Chen et al. 2008
nTiO ₂	packed column H: 30 cm, D: 15 cm	$d_{AFM} < 0.1$ μm 50, 75, 100 mg/L	quartz sand $d_{50} = 20$ μm	0.01 M NaCl, pH = 4.5	Very high particle retention; existing models limited in ability to predict nTiO ₂ behavior	Choy et al. 2008
nTiO ₂	pyrex wafers (2-D microchannel model) L*: 7.0 cm, W: 3.0 cm, H: 87 - 92 μm	$d_{XRD} = 5 - 12$ nm d_{DLS} depends on pH 0.07 - 0.14 g/L	pyrex $d = 700$ μm	hydrolysis synthesis solution, pH 1 - 12	Suspended nanoparticle aggregates very mobile; lower mobility seen at pH 3 and 7 (aggregates settle at pH 7)	Guzman et al. 2006
nTiO ₂	packed column H: 10 cm, D: 2.5 cm	$d_{50} = 35$ nm 2 g/L	12 surface soil types $d_{50} = 30 - 132$ μm	0.15 - 4.95 mM soil suspensions, pH 6.2 - 8.6	nTiO ₂ most mobile in soil solutions with smaller grain diameters and lower IS; heightened retention with increasing clay content and salinity	Fang et al. 2009
nTiO ₂	QCM-D	$d^* = 5$ nm $d_{DLS} = 350 - 750$ nm; $d_{FCS} = 7 - 189$ nm $d_{AFM} = 30$ nm $d_{TEM} \sim 30$ nm with larger aggregates 10 mg/L	silica surface	1 - 100 mM NaNO_3 , pH 3, 5, 9	Strong attractive electrostatic interactions between silica and nTiO ₂ at pH 3, 5 and at low IS; generally good agreement with DLVO theory	Fatissou et al. 2009
nTiO ₂	packed column H: 10 cm, D: 1.1 cm	$d^* = 10$ nm bare: $d_{TEM} = 14 \pm 1$ nm CMC-modified: $d_{TEM} = 15 \pm 1$ nm d_{DLS} varies with solution chemistry 20 mg/L	quartz sand $d_{50} = 290$ μm \pm aluminum or iron hydroxide coating	ultrapure water 1, 30 mM NaCl, pH 5.5 - 7.6 30 mM CaCl_2 , pH = 7.1	CMC coating greatly enhances mobility (bare nTiO ₂ is immobile)	Sung et al. 2009
nTiO ₂	packed column H: 9.25 cm, D: 2.5 cm	$d^* = 40$ nm $d_{DLS} = 198$ nm 0 - 10 mg/L	glass beads 300 - 425 μm ($d_{50} = 355$ μm)	0.01 M NaCl, pH 7	nTiO ₂ exhibits greater retention than alumoxane but more mobile than ferroxane; mobility slightly increasing with time	Lecoanet et al. 2004
nTiO ₂	packed column H: 9.25 cm, D: 2.5 cm	$d^* = 40$ nm $d_{DLS} = 198$ nm 10 mg/L	glass beads 300 - 425 μm ($d_{50} = 355$ μm)	0.01 M NaCl, pH 7	Decreased nTiO ₂ retention at faster flow velocity	Lecoanet & Wiesner, 2004
nTiO ₂	packed column H: 100 cm, D: 1.27 cm	$d^* = 40 - 60$ nm (before functionalization) Injected as ~ 60 wt% aqueous slurry	quartz sand 20 - 30 mesh	~ 60 wt% TiO ₂ aqueous slurry + 2% ammonium carboxylate, pH = n/a	Functionalized nTiO ₂ distributed uniformly throughout column, Cu-EDA functionalized nTiO ₂ candidate for groundwater treatment	Mattigod et al. 2005

Figure 1. Representative aggregation stability curves for selected engineered nanomaterials: (a) nC_{60} and nC_{60} derivatives PCBM ([6,6]-phenyl C_{61} -butyric acid methyl ester) and the corresponding butyl and octyl esters, PCBB and PCBO, and (b) MWNTs and surface oxidized MWNTs with varying surface oxygen concentration (SOC). Experimental data adapted from (14, 16-18, 23, 24, 34).

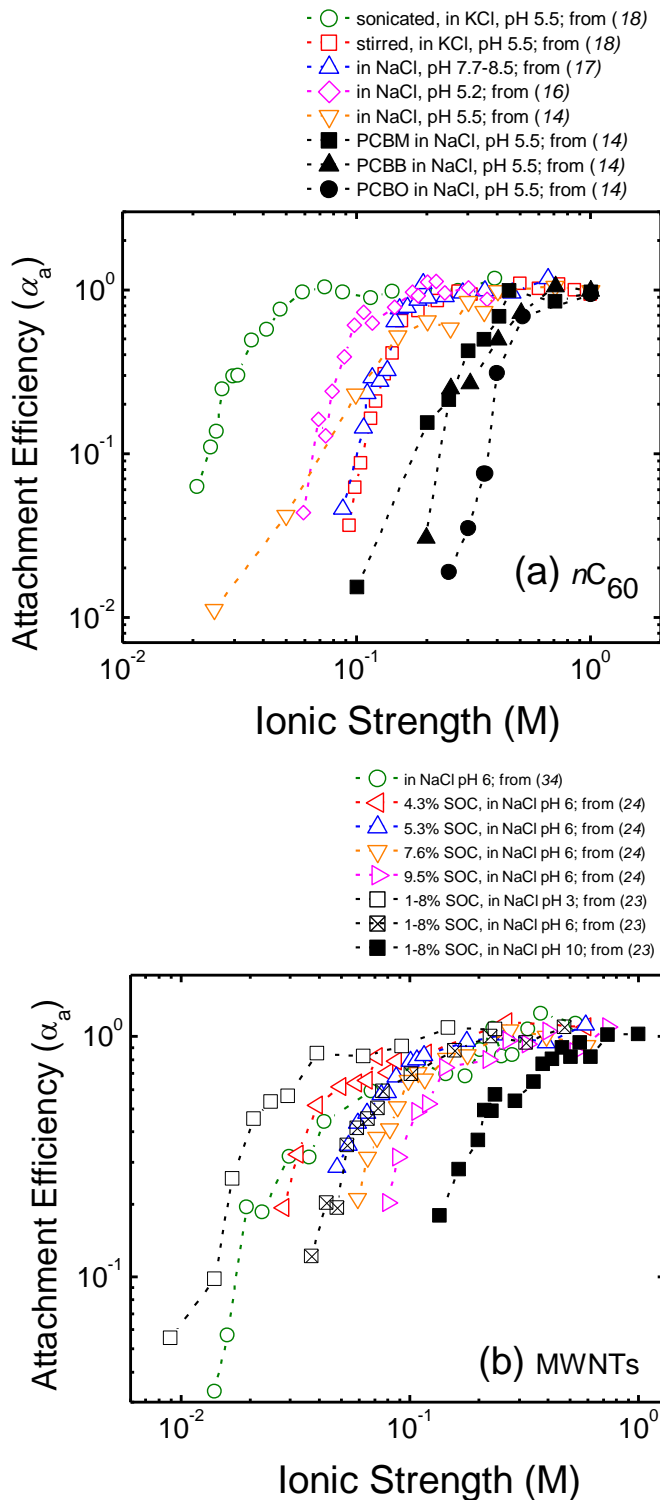
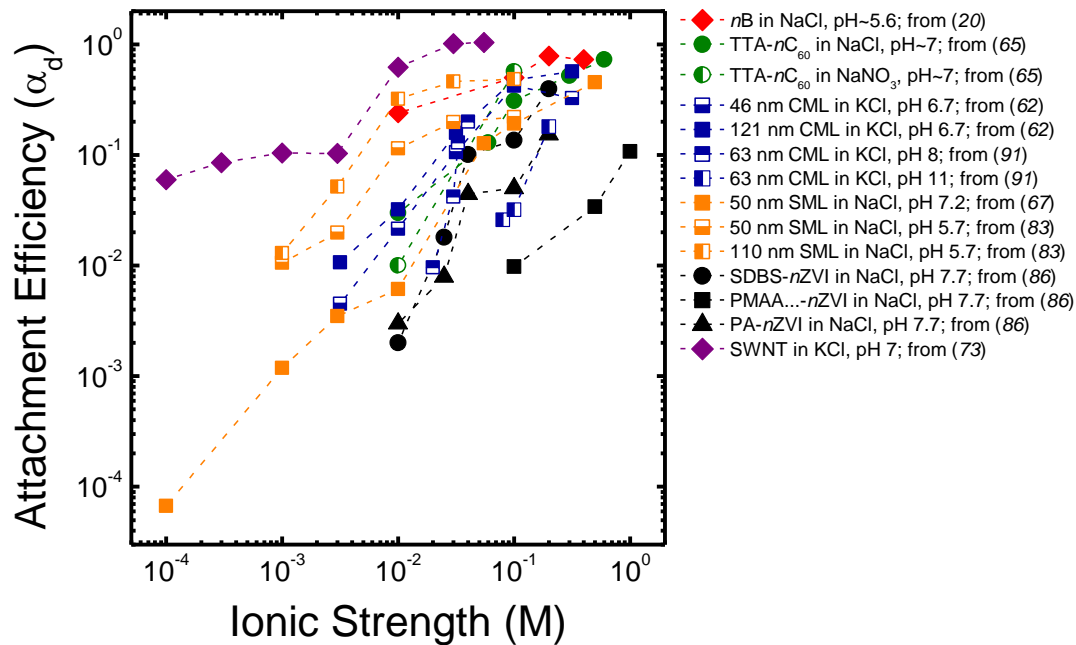


Figure 2. Representative deposition stability curves for selected engineered nanomaterials, including nB , nC_{60} , carboxyl-modified latex (CML), sulfate-modified latex (SML), $nZVI$, and SWNTs. Experimental data adapted from (20, 62, 65, 67, 73, 83, 86, 91).



BRIEF

A comprehensive overview of theoretical and experimental approaches pertaining to nanomaterial transport and aggregation in aquatic environments emphasizing the role of physicochemical interactions.