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- 1 Wood cellulose films regenerated from NaOH/urea aqueous solution and treated
- 2 by hot pressing for food packaging application
- 3
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### 19 Abstract

Cellulose films made from 'green' solvent provide the possibility to mitigate 20 21 environmental pollution caused by non-degradable plastic packaging. Herein, 22 regenerated cellulose films were prepared from five wood pulps in NaOH/urea aqueous 23 solution, dried either at ambient conditions or by hot pressing, and tested as 24 biodegradable packaging materials. The results revealed that different wood origins did not cause much difference in the structure of cellulose films. However, hot-pressing 25 26 could not only efficiently remove water from wet films, but also significantly improve 27 the tensile strength and water vapor barrier property of regenerated films. The RC-P-28 HP film had the tensile strength of 85.00±3.26 MPa, Young's modulus of 6.45±0.36 GPa, and water vapor permeability of  $3.59\pm0.14\times10^{-7}$  gm<sup>-1</sup>h<sup>-1</sup>Pa<sup>-1</sup>, and exhibited the 29 30 similar capacity as the commercial plastic wrap during the preservation of cherry 31 tomatoes for up to 16 days. Therefore, this study demonstrates a feasible strategy to 32 fabricate wood cellulose films for biodegradable food packaging.

33

34 Keywords: Wood pulps; cellulose films; regeneration; hot pressing; food packaging

### 36 1. Introduction

37 Food packaging waste accounts for approximately one-third of all household waste in 38 Canada (Diggle & Walker, 2020). Among them, plastic waste has low secondary market 39 value and high resistance to degradation and only 20% is collected for reuse and 40 recycling (Diggle et al., 2020; Huang & Wang, 2022). The accumulation of this non-41 degradable waste has severe impacts on marine and terrestrial ecosystems, resulting in 42 the urgent demand for eco-friendly food packaging materials. Cellulose is the most 43 abundant biopolymer and has been explored as a potential alternative to petroleum-44 based plastics owing to its availability, renewability, and biodegradability (Shi et al., 45 2022). Wood is the most important source of cellulose, and the type of wood (e.g. 46 hardwood and softwood) and processing conditions such as pulping and bleaching can 47 affect the structure of isolated cellulose (Tang et al., 2021). Wood cellulose has been 48 studied for applications in papermaking, textiles, biomedical, and high-performance 49 materials (Jia et al., 2018). Recently, the development of packaging materials from 50 wood cellulose nanofibrils (CNF) has been reported. For example, Missio et al. (2020) 51 fabricated an antioxidative film by combining CNF from Acacia mearnsii bark and 52 tannins. Tayeb et al. (2020) developed an oil barrier packaging material using CNF from 53 a bleached softwood kraft pulp, and Muthoka et al. (2021) infiltrated CNF and chitosan 54 into bleached fir veneer wood to form a transparent package.

55 Besides the utilization of CNF, natural cellulose fibers can also be easily converted into 56 different materials through dissolution and regeneration (Huang, Wang, Zhang, & Chen, 57 2016). Traditional solvents for cellulose dissolution, such as N-methylmorpholine-N-58 oxide (NMMO), LiCl/DMAc, and ionic liquids (ILs), have significant disadvantages 59 involving tedious handling processes, high energy consumption, and/or inefficient 60 recyclability (Huang et al., 2016). The NaOH/urea aqueous system is a "green" solvent 61 of cellulose that can disrupt the intra-/intermolecular hydrogen bonds of the 62 supramolecular structure within cellulose (Cai & Zhang, 2005). It has been reported 63 that the NaOH/urea system can be used to rapidly dissolve unbleached softwood kraft

64 pulp and spruce pulp at low temperatures after a mechanical or chemical pretreatment 65 (Shi et al., 2018). However, the structure and properties of regenerated cellulose (RC) films from various wood pulps have not yet been well studied. Moreover, drying 66 67 methods of cellulose films, such as air drying, freeze-drying, oven drying, and hot 68 pressing, can also affect the performance of the films. Among them, hot pressing is a 69 convenient way to dry cellulose films in a short time using elevated temperatures and 70 pressures (Rol et al., 2020). Qing et al. (2015) found that the hot-pressed cellulose 71 nanofibril (CNF) films showed improved mechanical properties compared to the 72 freeze-dried and air/oven-dried samples. Similar results were observed by Hasan et al. 73 (2021) that the CNF films treated by hot pressing exhibited decreased water vapor and 74 oxygen permeability due to better consolidation of layers in the film structures.

Therefore, to develop wood cellulose films as biodegradable food packaging materials, in this work, various hardwood (aspen, eucalyptus, and maple) and softwood (pine and spruce) pulps were dissolved in NaOH/urea aqueous solution, and the corresponding RC films were dried either in the air at 25 °C or by hot pressing. The structure and properties of RC films were characterized, and the RC film with the best mechanical and barrier properties was selected to preserve fresh cherry tomatoes.

# 81 2. Materials and methods

#### 82 **2.1. Materials**

The bleached kraft pulps of aspen, eucalyptus, maple, pine, and spruce were kindly provided by FPInnovations (QC, Canada). Sulfuric acid (95.0%-98.0%) was purchased from Sigma-Aldrich (Oakville, ON, Canada). Sodium hydroxide (>97.0%) and urea (>99.6%) were purchased from Fisher Scientific (Mississauga, ON, Canada). Distilled water was utilized throughout this study.

88

#### 89 2.2. Preparation of wood cellulose films

90 The wood pulp (2 g) was placed in 200 mL of H<sub>2</sub>SO<sub>4</sub> solution for 48 hours at 25 °C

91 with continuous stirring at 200 rpm to reduce the molecular weight of cellulose via 92 hydrolysis, where the concentrations of H<sub>2</sub>SO<sub>4</sub> solutions were 30 wt.% for aspen, pine 93 and spruce pulps, and 25 wt.% for eucalyptus and maple pulps. After acid hydrolysis, 94 the samples were thoroughly washed with water, dried in an oven at 100 °C for 16 hours, 95 and dissolved (4 wt.%) in the aqueous solution containing NaOH/urea/H<sub>2</sub>O in a 7:12:81 96 weight ratio. The solvent and wood pulps were pre-cooled to -20 °C and stirred at 2000 97 rpm for 8 minutes. The obtained solutions were centrifuged at 1000 rpm for 5 minutes 98 (25 °C) to degas and precipitate the insoluble fractions, and then cast on the glass plate 99 and coagulated in 5 wt.% H<sub>2</sub>SO<sub>4</sub> aqueous bath at 25 °C for 5 minutes to produce RC 100 films. In one treatment, the wet RC films prepared from aspen, eucalyptus, maple, pine, 101 and spruce were air dried at 25 °C and coded as RC-A-AD, RC-E-AD, RC-M-AD, RC-102 P-AD, RC-S-AD, respectively. In another aspect, the wet films were dried between two 103 stainless steel plates of a hot press machine (3895, Carver Inc., USA) at 90 °C and 0.4 104 MPa for 10 minutes, followed by hot pressing at 120 °C and 18 MPa for 10 minutes. 105 The hot-pressed RC films were labelled as RC-A-HP, RC-E-HP, RC-M-HP, RC-P-HP, 106 RC-S-HP, respectively.

### 107 **2.3. Characterization of wood cellulose films**

108 The recovery rate of cellulose after acid hydrolysis was calculated using a gravimetric

109 method by the Equation (1):

Recovery rate (%) = 
$$\frac{W_2}{W_1} \times 100\%$$
 (1)

110 Where 
$$W_1$$
 is the dry weight of wood pulps before acid hydrolysis, and  $W_2$  is the dry  
111 weight of wood pulps after acid hydrolysis.

Before viscosity-average molecular weight ( $M_v$ ) measurement, original wood pulps, acid hydrolyzed wood pulps, and hot-pressed RC films were stored at 25 °C and 50% RH for 4 days to ensure same water content. The intrinsic viscosity [ $\eta$ ] of each sample was conducted according to the TAPPI T230 standard test method. The degree of polymerization (DP) was determined by the Mark-Houwink-Sakurada equation, and 117 the  $M_{\nu}$  values were calculated by multiplying DP by the molar mass of anhydrous 118 glucose unit (162 g/mol).

$$DP^{0.9} = 1.65[\eta] \tag{2}$$

Before density measurement, RC films (5 cm × 5 cm) were conditioned at 25 °C and 50% RH for 4 days. The thickness of the films was determined with a micrometer (resolution of 0.001 mm, Mitutoyo 547-400S, Japan) at 10 random points. The density was calculated by the ratio of weight and volume, and the apparent porosity was calculated based on the densities of RC films ( $\rho_f$ ) and crystalline cellulose ( $\rho_c = 1.63$ g/cm<sup>3</sup>) as shown in Equation (3) (Aulin, Gällstedt, & Lindström, 2010):

$$Porosity (\%) = \frac{\rho_c - \rho_f}{\rho_c} \times 100\%$$
(3)

125 The FT-IR spectra of RC films were recorded on an Agilent Technologies Cary 630 FT-IR spectrometer (Agilent Technologies Inc., CA, USA) as the average of 64 scans with 126 a resolution of 2 cm<sup>-1</sup>. The crystalline profile of wood pulps and RC films was measured 127 128 using a high-resolution X-ray diffractometer (Empyrean, Malvern Panalytical Ltd, 129 Malvern, UK) with copper Kα radiation (1.54178 Å) in 2θ ranging from 4° to 40°. The 130 surface morphology of RC films was observed by a Hitachi TM1000 SEM (Hitachi Co. 131 Ltd., Tokyo, Japan) with an acceleration voltage of 4 kV. The samples were sputtercoated with a 4 nm layer of gold-palladium using a Leica EM ACE200 coater (ON, 132 133 Canada) prior to observation.

134 The tensile strength, elongation at break, and Young's modulus of RC films were tested 135 at 25 °C and 50% RH by using an ADMET MTEST Quattro eXpert 7600 single-column 136 testing system (MA, USA) with a load cell of 250 lb. and a crosshead speed of 5 mm/min. The water vapor permeability (WVP) of RC films was determined based on 137 the ASTM E96-92 standard (ASTM, 1995). A dried film was taped on the top of a glass 138 139 flask containing 3 g of anhydrous calcium chloride. The sealed glass flask was then 140 located in a desiccator with water to reach a relative humidity of 100%. The weight change of the flask was recorded periodically at 25 °C. The WVP (g m<sup>-1</sup> h<sup>-1</sup> Pa<sup>-1</sup>) of 141

142 films was calculated by the Equation (4):

$$WVP = \frac{\Delta m \times k}{A \times \Delta T \times \Delta P} \tag{4}$$

143 Where  $\Delta m$  is the weight change of the flask (g) during time  $\Delta T$  (h), k is the thickness 144 of each RC film (m), A is the exposed area of the film (7.85 × 10<sup>-5</sup> m<sup>2</sup>), and  $\Delta P$  is the 145 partial water vapor pressure difference between two sides of the film (Pa). The oxygen 146 transmission rate (OTR) of RC films was determined at 23 °C and 0% RH using the 147 Mocon Ox-Tran Model 2/22 (Mocon, Minneapolis, USA). The oxygen permeability 148 (OP) was calculated by the Equation (5):

$$OP = \frac{OTR \times \ell}{\Delta P'} \tag{5}$$

149 where *OTR* is oxygen transmission rate,  $\ell$  is the film thickness, and  $\Delta P'$  is the partial 150 pressure of oxygen (kPa).

151 **2.4. Study of shelf life** 

The evaluation of the preservation effect of cellulose films on fruits was based on the methods of Guo et al. (2020) with slight modifications. Fresh cherry tomatoes washed with deionized water were placed in glass jars and covered with polyvinyl chloride plastic wrap (Kirkland Signature Stretch-Tite Plastic Wrap - 11 7/8 x750 Feet) and RC-P-HP. The tomatoes without any package were set as the control. All samples were stored at 25 °C and 50% RH for a maximum of 3 weeks to monitor the appearance and weight loss.

## 159 **2.5. Statistical analysis**

Each measurement was performed in triplicate, and the experimental data were presented as the mean  $\pm$  standard deviation. Analysis of variance (ANOVA) was applied for the statistical analysis, followed by multiple comparison tests via Duncan's multiple-range test. All the analyses were carried out through SPSS statistical software (version 26, IBM SPSS Inc., New York, NY) with significant differences within samples at p < 0.05.

### 166 **3. Results and discussion**

As listed in Table 1, all the samples had a high recovery rate (~90%) after acid hydrolysis. The  $M_{\nu}$  values of original wood pulps ranged from  $2.87 \times 10^5$  to  $6.28 \times 10^5$ g/mol, which decreased to the range of  $1.53 \times 10^5$  to  $2.33 \times 10^5$  g/mol after acid hydrolysis. The molecular weight of hot-pressed RC films was relatively lower because a few insoluble fractions (~0.3%) were removed by centrifugation and the slight degradation happened during dissolution and regeneration process (Wang, Zhao & Deng, 2008).

Wood pulps	Recovery rates (%)	$M_{v}$ (g/mol)				
		Original wood pulps	After acid hydrolysis	Hot-pressed films		
Aspen	$89.53 \pm 0.35$	$6.28 \times 10^{5}$	$2.33 \times 10^{5}$	$1.70 \times 10^{5}$		
Eucalyptus	$92.25 \pm 1.11$	$4.41 \times 10^{5}$	$1.53 \times 10^{5}$	$1.15 \times 10^{5}$		
Maple	$90.01 \pm 1.73$	$2.87 \times 10^{5}$	$1.70 \times 10^5$	$9.23 \times 10^{4}$		
Pine	$91.85\pm2.01$	$5.26 \times 10^{5}$	$1.90 \times 10^5$	$1.46 \times 10^{5}$		
Spruce	$92.42 \pm 1.86$	$4.54 \times 10^5$	$1.85 \times 10^5$	$7.51 \times 10^4$		

174 Table 1. Recovery rate and molecular weight  $(M_v)$  of wood pulps and hot-pressed films.

175 The average thickness of RC films produced by air-drying was  $33 \pm 3 \mu m$ , while the 176 hot-pressed RC films were significantly thinner ( $27 \pm 1 \mu m$ ). As shown in Fig. 1, 177 different sources of wood pulps did not affect the density and porosity of RC films, but 178 the hot pressing treatment remarkably increased the density from approximately 0.95 g/cm<sup>3</sup> to 1.15 g/cm<sup>3</sup> and reduced the porosity from about 35% to 22.5%. Similar results 179 have been reported that RC films dried with applied pressure could form dense 180 structures (Shahi, Min, Sapkota, & Rangari, 2020). The decreased free space and 181 182 cavities in RC films could contribute to the improvement in mechanical strength and 183 gas barrier properties (Aulin et al., 2010; Wakabayashi, Fujisawa, Saito, & Isogai, 2020).



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Fig. 1. Density (A) and porosity (B) of RC films. Different letters on the tops of columns represented the significant difference (p < 0.05).

FT-IR spectra and XRD diffraction patterns of various wood pulps and RC films were 187 188 collected to investigate the effects of cellulose dissolution and regeneration in 189 NaOH/urea aqueous solution and different drying methods on cellulose structure. As 190 shown in Fig. 2 A-C, all samples displayed similar FT-IR spectra with no new peaks 191 after dissolution, regeneration and drying, which demonstrated no chemical 192 modifications happened during film production. However, changes in the intensity of 193 the peaks were observed. For instance, the intensities of absorption peaks at around 3360 and 3269 cm<sup>-1</sup> decreased after dissolution and regeneration, while the hot-pressed 194 195 films presented even lower intensities than the air-dried films. These two peaks were 196 attributed to the O-H stretching vibration of the hydroxyl groups, which indicated the 197 intra- and intermolecular hydrogen bonds in cellulose, respectively (Zhou & Wang, 198 2021). The hydrogen bonds were broken during the dissolution, and the rearrangement happened during the regeneration and drying process. The rapid coagulation and drying 199 200 process of RC films led to the disturbed intermolecular interaction and decreased 201 intensities at 3330 and 3269 cm<sup>-1</sup> (Lindman, Medronho, Alves, Costa, Edlund, & Norgren, 2017). Besides, the peak at 1427 cm<sup>-1</sup> was the absorption band of the 202 crystalline cellulose due to asymmetric -CH<sub>2</sub> bending vibration, while the peak at 898 203 204 cm<sup>-1</sup> was the -C-O-C- bridge stretching, representing the amorphous region and

205 cellulose II crystalline structure (Salim, Asik, & Sarjadi, 2021) The ratio of peak intensities at 1427 and 898 cm<sup>-1</sup> was defined as "crystallinity index", which was 206 decreased after dissolution and regeneration, indicating the decrease in crystallinity and 207 208 the transition from cellulose I to cellulose II structure (Salim et al., 2021; Zhou et al., 209 2021). As shown in Fig. 2 D-E, the wood pulps displayed similar diffraction peaks at about  $14.8^{\circ}$  (110),  $16.3^{\circ}$  (110),  $22.5^{\circ}$  (200), and  $34^{\circ}$  (040), which were typical cellulose 210 I structure (Zhou et al., 2021). After the dissolution and regeneration process, the RC 211 films showed cellulose II structure with broad diffraction peaks at 20.2° and 22.6°, 212 213 corresponding to (110) and (020) crystallographic planes, respectively (Razali et al., 214 2022). The crystallinity indices (CI) of RC films were significantly lower than those of 215 the wood pulps. It indicated a crystal transformation of cellulose I to cellulose II during 216 dissolution and regeneration, which was in accordance with the FT-IR results. The sources of wood pulps did not affect the diffraction patterns of RC films. 217



Fig. 2. Fourier transform infrared spectroscopy spectra of wood pulp cellulose (A),
air-dried RC films (B), and hot-pressed RC films (C). X-ray diffraction patterns and

221 crystallinity index of wood cellulose pulps (D) and RC films (E).

222 The morphology of RC films dried by different methods was observed by SEM. As 223 shown in Fig. 3 A, no obvious undissolved fibers were observed on the surface of RC 224 films, indicating a good solubility of hydrolyzed wood pulp cellulose in NaOH/urea aqueous solution. However, the air-dried RC films showed uneven and rough surfaces 225 226 and layered cross-sections (Fig. 3 B), which might be due to the inevitable non-uniform shrinkage during the air-drying process (Ketola et al., 2018). In contrast, the hot-pressed 227 228 RC films possessed smooth and uniform surfaces and dense internal structures. It was 229 because the hot pressing treatment could facilitate the stretch and rearrangement of 230 cellulose chains and effectively reduce the free space and cavities in the RC films 231 (Wang et al., 2013). Moreover, the air-dried RC films were not as transparent as the 232 hot-pressed ones (Fig. 3 C). It was due to the uneven structure and larger thickness of 233 air-dried RC films. The high transparency of RC films is beneficial for displaying the food products in packaging. 234



235

Fig. 3. SEM images of RC films: surface (A) and cross-section (B). Photos of RC films(C).

238 The mechanical properties of RC films are essential because food packaging materials 239 need to maintain the integrity and preserve the quality of packaged food (Ai et al., 2021). 240 As shown in Fig. 4 A and Fig. 4 C, the tensile strength and Young's modulus of RC 241 films produced from pine were significantly higher than those of other RC films. It might be due to the variation of molecular weight and CI of cellulose from different 242 sources (Aulin et al., 2010; De Silva & Byrne, 2017; Mokhena, Sadiku, Mochane, Ray, 243 244 John, & Mtibe, 2021; Yousefi, Faezipour, Hedjazi, Mousavi, Azusa, & Heidari, 2013). 245 For example, the higher  $M_{\nu}$  value of cellulose could enhance the intermolecular 246 entanglement, leading to an improved tensile strength of cellulose film (Jin et al., 2019); 247 however, the aggregation and entanglement of cellulose chains also restricted the 248 molecular orientation during dissolution and regeneration processes, and resulted in the 249 decreased tensile strength (Xie et al. 2021). At the same time, the high content of the 12

250 crystalline structure led to an enhanced tensile strength (Shi et al., 2021). As expected, 251 the hot-pressed RC films possessed notable enhancement in tensile strength and 252 modulus compared to the air-dried films. These different mechanical properties were 253 attributed to the density and porosity (Cazón, Velazquez, & Vázquez, 2019). It has been 254 demonstrated that pores and free volume affects the mechanical properties of the 255 material, since the less solid material per unit volume, the weaker the resistance to deformation (Cao et al., 2020; Su, Rao, He, & Wei, 2020). The RC-P-HP sample 256 exhibited the highest tensile strength of  $85.00 \pm 3.26$  MPa and Young's modulus of 6.45 257 258  $\pm$  0.36 GPa and was stronger than the RC films fabricated from bamboos in DMAc/LiCl 259 solvent (81.09 MPa) (Gao, Li, Zhang, Tang, & Chen, 2021), corncob residue in ionic 260 liquid (70.63 MPa) (Song, Chen, Chen, Xu, & Xu, 2021), bed sheets in NaOH/urea 261 solution (76.21 MPa) (Zhou et al., 2021), and cotton linter pulps in NaOH/urea solution (73.40 MPa) (Reddy, Varada Rajulu, Rhim, & Seo, 2018). 262



Fig. 4. Mechanical properties (A-E) and WVP (F) of RC films. Different letters on the tops of columns represented the significant difference (p < 0.05).

266 The WVP values of RC films dried by different methods are shown in Fig. 4 F. Despite the sources of wood pulps, the air-dried RC films displayed similar WVP values ranging 267 from 4.14  $\pm$  0.19 to 4.59  $\pm$  0.11  $\times$   $10^{-7}$  g m  $^{-1}$  h  $^{-1}$  Pa  $^{-1}$  , while the hot pressing treatment 268 significantly decreased the values to the range of  $3.43 \pm 0.36$  to  $3.89 \pm 0.15 \times 10^{-7}$  g m<sup>-1</sup> 269  $h^{-1}$  Pa<sup>-1</sup>. The hot-pressed films had reduced apparent porosity, which slowed down the 270 271 diffusion of water vapor. It is well known that the water vapor barrier property of cellulose films is not ideal because of their hydrophilic nature, and chemical 272 modifications are usually required (Li, Wang, Wang, Qin, & Wu, 2019). The 273 274 improvement in barrier properties through hot pressing treatment could avoid using 275 chemical reagents and eliminate possible contamination from chemical residues. It was 276 worth noting that the WVP values of most RC films in this work were lower than those of RC films manufactured from oil palm biomass  $(4.68 \times 10^{-7} \text{ g m}^{-1} \text{ h}^{-1} \text{ Pa}^{-1})$  (Amalini, 277 Haida, Imran, & Haafiz, 2019) and cotton linter pulp  $(8.21 \times 10^{-6} \text{ g m}^{-1} \text{ h}^{-1} \text{ Pa}^{-1})$ 278 279 (Reddy et al., 2018).

280 Packaging materials with suitable mechanical and barrier properties can protect food 281 products from physical damage, oxidation, loss of nutrients, and dehydration, and 282 thereby extend the shelf life (Pandey, Sharma, & Gundabala, 2022; Yilmaz, Demirhan, 283 & Ozbek, 2022). Based on the above-mentioned results, the RC-P-HP film with 284 relatively good tensile strength and water vapor barrier property was selected for the shelf-life study and comparison with commercial plastic wrap. As shown in Fig. 5 A, 285 286 the unpackaged cherry tomatoes became soft and exhibited obvious wrinkles on the 287 surface on day 10, and completely deteriorated with a putrid odor on day 16. However, 288 the tomatoes packaged with plastic wrap and RC-P-HP film well maintained their bright 289 red color and hardness on day 10, and only showed minor shrinkages without putridity 290 on day 16. The dehydration of fruits affects their shelf life and commercial value (Fich, 291 Fisher, Zamir, & Rose, 2020). The weight loss of unwrapped and packaged cherry tomatoes over 16 days was monitored and displayed in Fig. 5 B. The unwrapped 292 293 tomatoes lost about 21.72% of their original weight on day 16. This was lowered to 294 10.40% and 11.25% when commercial plastic wrap and RC-P-HP film were applied, 295 respectively. The weight loss of cherry tomatoes was mainly due to water loss from transpiration and respiration processes. The WVP value of RC-P-HP  $(3.56 \pm 0.14 \times 10^{-1})$ 296 <sup>7</sup> g m<sup>-1</sup> h<sup>-1</sup> Pa<sup>-1</sup>) was higher than the plastic wrap  $(2.37 \pm 0.17 \times 10^{-8} \text{ g m}^{-1} \text{ h}^{-1} \text{ Pa}^{-1})$ . 297 However, the OTR value of plastic wrap exceeded the detection limit ( $2000 \text{ cc/m}^2 \text{ day}$ ), 298 and its OP value was higher than 0.02 cc m<sup>-1</sup> day<sup>-1</sup> atm<sup>-1</sup> compared to  $3.01 \pm 0.49 \times 10^{-1}$ 299  $^{5}$  cc m<sup>-1</sup> day<sup>-1</sup> atm<sup>-1</sup> for RC-P-HP. It was reported that the composite film of gelatin and 300 carboxymethyl cellulose with a WVP value of  $5.47 \times 10^{-7}$  g m<sup>-1</sup> h<sup>-1</sup> Pa<sup>-1</sup> and OP of 1.32 301  $\times 10^{-4}$  cc m<sup>-1</sup> day<sup>-1</sup> atm<sup>-1</sup> led to 23.22% weight loss of packed cherry tomatoes after 14 302 303 days' storage (Samsi et al., 2019). Thus, RC-P-HP effectively prevented the weight loss of cherry tomatoes due to the significantly reduced OP and relatively low WVP values. 304



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Fig. 5. Appearance (A) and weight loss (B) of cherry tomatoes under differentpackaging conditions.

## 308 4. Conclusion

After acid hydrolysis, five wood pulps were successfully dissolved in NaOH/urea aqueous solution. The type of wood pulps showed no remarkable impact on the structure of RC films, and all films were transparent for displaying the packaged products. Furthermore, the hot pressing process resulted in the RC films with smoother surfaces and fewer cavities compared to the air-dried films, which contributed to the dramatically improved mechanical strength and water vapor barrier property. Among all the samples, the RC-P-HP film made from pine showed the best properties and could effectively prevent the weight loss and deterioration of the wrapped cherry tomatoes for up to 16 days. This performance was comparable to the commercial plastic wrap, and thus the hot-pressed RC films had the potential applications in biodegradable food packaging.

## 320 **Conflict of Interest**

321 The authors declare that they have no conflict of interest.

## 322 Acknowledgement

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